

Amherst Island Wind Energy  
Project  
Mainland Laydown Area Erosion  
and Sediment Control Plan and  
Stormwater Management Report



Prepared for:  
Windlectric Inc.  
c/o Algonquin Power Co.  
354 Davis Road, Suite 100  
Oakville, ON L6J 2X1

Prepared by:  
Stantec Consulting Ltd.  
100-300 Hagey Blvd  
Waterloo, ON N2H 6M7

July 24, 2017

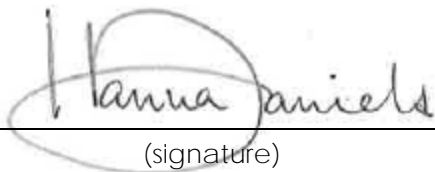
# Sign-off Sheet

This document entitled Amherst Island Wind Energy Project Mainland Laydown Area Erosion and Sediment Control Plan and Stormwater Management Report was prepared by Stantec Consulting Ltd. ("Stantec") for the account of Windlectric Inc. (the "Client"). Any reliance on this document by any third party is strictly prohibited. The material in it reflects Stantec's professional judgment in light of the scope, schedule and other limitations stated in the document and in the contract between Stantec and the Client. The opinions in the document are based on conditions and information existing at the time the document was published and do not take into account any subsequent changes. In preparing the document, Stantec did not verify information supplied to it by others. Any use which a third party makes of this document is the responsibility of such third party. Such third party agrees that Stantec shall not be responsible for costs or damages of any kind, if any, suffered by it or any other third party as a result of decisions made or actions taken based on this document.



Prepared by \_\_\_\_\_  
(signature)

Nick Emery, P.Eng.

  
\_\_\_\_\_  
(signature)

Reviewed by \_\_\_\_\_

Hanna Daniels, EIT

AMHERST ISLAND WIND ENERGY PROJECT  
MAINLAND LAYDOWN AREA EROSION AND SEDIMENT CONTROL PLAN AND STORMWATER  
MANAGEMENT REPORT

July 24, 2017

## Table of Contents

1.0	INTRODUCTION .....	1.2
1.1	STUDY APPROACH .....	1.2
1.2	BACKGROUND INFORMATION .....	1.3
2.0	ASSESSMENT OF HYDROLOGIC IMPACTS AND MITIGATION – OPERATIONAL PHASE (SWM) .....	2.1
2.1	EXISTING CONDITIONS.....	2.1
2.2	PROPOSED CONDITIONS.....	2.1
2.3	HYDROLOGIC MODELING .....	2.2
2.4	STORMWATER MANAGEMENT STRATEGY.....	2.2
2.4.1	Vegetated Filter Strip .....	2.3
2.4.2	Vegetated Swale .....	2.3
2.4.3	Dry Pond .....	2.3
2.4.4	Design Considerations .....	2.4
3.0	ASSESSMENT OF POTENTIAL HYDROLOGIC IMPACTS AND MITIGATION – DURING-CONSTRUCTION PHASE (ESC).....	3.1
3.1	DURING CONSTRUCTION DEWATERING.....	3.1
3.2	EROSION AND SEDIMENT CONTROL PLAN.....	3.1
3.3	EROSION AND SEDIMENTATION CONTROL MONITORING PLAN.....	3.3
3.4	LONG TERM EROSION AND SEDIMENT CONTROL.....	3.4
4.0	CONCLUSIONS AND RECOMMENDATIONS.....	4.1

## FIGURES

FIGURE 1 – MAINLAND LAYDOWN AREA PRE-DEVELOPMENT CATCHMENT PLAN

FIGURE 2 – MAINLAND LAYDOWN AREA POST-DEVELOPMENT CATCHMENT PLAN

## APPENDICES

APPENDIX A – EXISTING CONDITIONS HYDROLOGY

APPENDIX B – PROPOSED CONDITIONS HYDROLOGY

APPENDIX C – DESIGN CALCULATIONS

## DRAWINGS

DRAWING C104 – MAINLAND LAYDOWN AREA GRADING AND SEDIMENT AND  
EROSION CONTROL PLAN

DRAWING C303 – SITE DETAIL SHEET



July 24, 2017

## 1.0 INTRODUCTION

Stantec Consulting Ltd. (Stantec) was retained by Windlectric Inc. (the Proponent) to assess and review the need for erosion and sediment control (ESC) and stormwater management (SWM) measures associated with the proposed development of the Amherst Island Wind Energy Project (herein referred to as the "Project"). This report is intended to address the requirements for SWM measures as described in Section H of the project's Renewable Energy Approval (REA #7123-9W9NH2) and supplement the information included as part of the application for a REA.

The Project includes the construction of a temporary laydown area, referred to herein as the Mainland Laydown Area (MLA) for stockpiling wind project components and construction materials, and a SWM facility.

This ESC and SWM Report summarizes the assessment of potential hydrologic impacts associated with the construction phase (i.e., ESC) and operational phase (i.e., SWM) of the Project. Assessed potential hydrologic impacts include changes to the stormwater runoff quality and/or quantity discharged to the surface or sub-surface receiving systems. The objective of this report is to demonstrate that the Project design and proposed mitigation measures associated with the construction and operation phases of the Project, as described in the REA Application, detailed engineering design, and herein, are sufficient to minimize any potential impacts to environmental features within the Project area, and to provide details on the mitigation and control measures that will be implemented.

### 1.1 STUDY APPROACH

The study approach involves the following components:

- A qualitative assessment of existing hydrologic conditions of the Project area and receiving systems;
- A review of the proposed Project activities as described in the REA with an emphasis on assessing potential impacts associated with changes in hydrologic characteristics of the Project area;
- Complete final design of SWM measures to control site runoff in a manner consistent with Ministry of Environment and Climate Change (MOECC) and Ministry of Transportation (MTO) requirements; and
- Development of an erosion and sediment control (ESC) strategy outlining the anticipated approach to minimize impacts related to construction.

AMHERST ISLAND WIND ENERGY PROJECT  
MAINLAND LAYDOWN AREA EROSION AND SEDIMENT CONTROL PLAN AND STORMWATER  
MANAGEMENT REPORT

July 24, 2017

## 1.2 BACKGROUND INFORMATION

A variety of sources have been referenced during the preparation of this ESC and SWM Report, including project-specific documentation, such as the various reports submitted in support of the REA application, and general industry-standard design guidance documentation and/or literature references, as follows:

### General Guidance Documentation / Literature

- *Drainage Management Manual (Ministry of Transportation, Ontario, 1997)*
- *Highway Drainage Design Standards (Ministry of Transportation, Ontario, 2008)*
- *Low Impact Development Stormwater Management Planning and Design Guide, Credit Valley Conservation and Toronto and Region Conservation, 2011*
- *Erosion and Sediment Control Guideline for Urban Construction (ESC Guidelines), Greater Golden Horseshoe Conservation Authorities, Dec. 2006*
- *Stormwater Management Planning and Design Manual (SWMPD Manual), Ontario Ministry of the Environment, March 2003*
- *Guidelines for Evaluating Construction Activities on Water Resources, Ontario Ministry of the Environment, January 1995*

### Project-Specific Consultation / Documentation

- *Hydrogeological Investigation – Proposed Amherst Island Wind Farm, Stantec Consulting Ltd., January 2016*
- *Supplementary Geotechnical Investigation – Proposed Amherst Island Wind Farm, Stantec Consulting Ltd., September 2015*
- *Geophysical Investigation to Map bedrock in Amherst Island, Ontario, Geophysics GPR International Inc., June 2015*
- *Amherst Island Wind Energy Project: Water Assessment and Waterbody Report (WA/WR), Stantec Consulting Ltd., April 2013*
- *Amherst Island Wind Energy Project: Design and Operations Report (DOR), Stantec Consulting Ltd., December 2013*
- *Amherst Island Wind Energy Project: Construction Plan Report, Stantec Consulting Ltd., December 2013*



July 24, 2017

## 2.0 ASSESSMENT OF HYDROLOGIC IMPACTS AND MITIGATION – OPERATIONAL PHASE (SWM)

### 2.1 EXISTING CONDITIONS

The location of the proposed MLA is a former industrial property. As shown in Figure 1, surface runoff drains southerly to the north Bath Road roadside ditch, which conveys it to an existing open footing concrete box culvert. The culvert discharges directly to Lake Ontario.

The subject site topography generally slopes from north to south at an average grade of approximately 3%. The information presented in the Lennox and Addington Soil Survey suggests that the site soil is Farmington loam, which is typically located over shallow bedrock.

The existing drainage catchments are delineated on Figure 1, and are summarized as follows:

Catchment EXT1 – This external drainage area is a former industrial property. All buildings have been demolished. Any on-site storm sewers were likely abandoned and capped as part of the demolition works. Consequently, all runoff travels southward as shallow surface flow.

Catchment 101 – This portion of the site is comprised of grassed area and parking lots. The available site survey information shows that there are catch basins within the proposed project limits, but the alignment and outlet locations of the on-site storm sewers are unknown. However, based on the site location topography, any storm sewers in this area likely discharge near the upstream side of the Bath Road culvert.

### 2.2 PROPOSED CONDITIONS

The grassed portions of the Mainland Laydown Area will be stripped of topsoil, graded, proof rolled, and a granular layer will be applied. The MLA is a temporary construction feature and is scheduled to be rehabilitated to existing conditions following the completion of the construction of the Project. The MLA will drain by sheet flow to a dry SWM pond, located near the southeast site corner, to provide water quality and quantity treatment prior to discharging to the Bath Road ditch. A topsoil berm surrounding the gravel portion of the laydown area will divert external runoff around the disturbed area to the Bath Road ditch.

The proposed drainage catchments are delineated on Figure 2, and are summarized as follows:

Catchment EXT1 – This external drainage area is a former industrial property. All buildings have been demolished. Any on-site storm sewers were likely abandoned and capped as part of the demolition works. All runoff travels southward as shallow surface flow across the western portion of the MLA to the Bath Road ditch.

AMHERST ISLAND WIND ENERGY PROJECT  
MAINLAND LAYDOWN AREA EROSION AND SEDIMENT CONTROL PLAN AND STORMWATER  
MANAGEMENT REPORT

July 24, 2017

Catchment EXT2 – This external drainage area is a former industrial property. All buildings have been demolished. Any on-site storm sewers were likely abandoned and capped as part of the demolition works. All runoff travels southward as shallow surface flow and is diverted eastward by the MLA topsoil berms to the Bath Road ditch.

Catchment 201 – This area is comprised of existing parking lots and undisturbed grass. All runoff travels as sheet flow to the Bath Road ditch.

Catchment 202 – This area is comprised of existing parking lots. All runoff is diverted eastward by the proposed topsoil berms and travels as shallow concentrated flow to the Bath Road ditch.

Catchment 203 – This area will be stripped of topsoil, graded, and proof rolled and a gravel layer will be applied. All runoff is directed to a temporary dry SWM pond that, along with a grassed swale and vegetated filter strip, acts as a treatment train to provide all necessary stormwater treatment. Any existing catch basins in this area will be temporarily capped.

## 2.3 HYDROLOGIC MODELING

Hydrologic models were prepared to simulate drainage conditions for the subject development using the SWMHYMO (Stormwater Management Hydrologic Model) software package, which is an MTO accepted hydrologic modeling software. The models were used to estimate flows for the existing and proposed development conditions and to design SWM systems to reduce the proposed development peak flow rates at the Bath Road culvert to existing condition magnitudes. Flows were calculated using the 2, 5, 10 and 100-year SCS Type II storm distribution and the 25 mm, 4-hour Chicago storm event. Schematics of the SWMHYMO model and all input and output files are provided in Appendices A and B.

## 2.4 STORMWATER MANAGEMENT STRATEGY

Stormwater runoff from the proposed MLA is treated by a temporary dry stormwater management pond located near the southeast site corner (Drawing C104). A dry facility was selected due to the shallow local bedrock depths and because the proposed drainage area is less than 5 hectares, which is the minimum MOECC guideline to sustain a permanent pool in a wet facility.

Runoff from the proposed MLA is conveyed to the pond both as shallow sheet flow and as concentrated flow by a proposed grassed swale. The combination of vegetated filter strip, vegetated swale conveyance, and dry facility attenuation will provide water quality controls for the MLA, while the dry facility will provide the water quantity controls for the site.

Water quality benefits of the proposed vegetated filter strip, vegetated swale, and vegetated dry pond facility are achieved by the runoff / vegetation interaction which reduces the velocity of runoff, as compared to a piped system, thereby promoting the sedimentation of particulate



July 24, 2017

matter. The vegetation also provides nutrient uptake benefits to help reduce biological pollutants such as nitrogen and phosphorous.

#### 2.4.1 Vegetated Filter Strip

The vegetated filter strip provides pretreatment to the MLA runoff upstream of the vegetated swale and dry SWM pond. The vegetated filter strip is comprised of a 2 m wide swath of undisturbed grass. While the guidance presented in the *Low Impact Development (LID) Stormwater Management Planning and Design Guide (LID Design Guide)* (Credit Valley Conservation (CVC), 2010) recommends a minimum width of 5 m, the guide also notes that narrower filter strips can be used when they are employed as pretreatment devices for other water quality best management practices. A wider filter strip is not feasible since it would encroach into the proposed MLA, reducing the area available to stockpile material.

#### 2.4.2 Vegetated Swale

The vegetated swale is sized to convey the 4-hour, 25-mm storm event at a velocity of 0.5 m/s at a depth of 150 mm. *The Low Impact Development (LID) Stormwater Management Planning and Design Guide (LID Design Guide)* (Credit Valley Conservation (CVC), 2010) and the *Stormwater Management Planning and Design Manual* (Ministry of Environment and Climate Change (MOECC), 2003), suggest that a design depth of 100 mm be used. Upon further investigation of the criteria, it was confirmed that the maximum flow depth of 100 mm is based on the assumption that it is 2/3 the height of the vegetation, which was limited to 150 mm. This is true for turf grass type vegetation, however the seed bank mix vegetation for the site swale is proposed to be a naturalization mix that reaches heights over 1 m. Since the design flow depth is less than 2/3 of the vegetation height, the proposed vegetated swale will filter the MLA runoff and reduce the peak flow velocities. The proposed vegetated swale will provide approximately 76% total suspended solids (TSS) removal, per the LID Design Guide (CVC, 2010).

#### 2.4.3 Dry Pond

The dry, extended detention SWM facility has been designed per the guidance of the SWMPD Manual (MOE, 2003) to provide the MOE Basic treatment level, or 60% TSS removal efficiency, and includes 482 m<sup>3</sup> of extended detention storage to be drawn-down over approximately 27 hours, satisfying the recommended draw-down time of 24-48 hours.

The combination of vegetated filter strip, vegetated swale, and dry extended detention SWM facility, will provide an Enhanced level of water quality control (80% long term average suspended solids removal), as required by the MOECC.

The facility will be drained by a single 100 mm diameter PVC outlet that discharges to a level spreader on the south side of the proposed pond. Similar to existing conditions, the pond discharges travel as shallow surface flow from the level spreader to the Bath Road roadside



AMHERST ISLAND WIND ENERGY PROJECT  
 MAINLAND LAYDOWN AREA EROSION AND SEDIMENT CONTROL PLAN AND STORMWATER  
 MANAGEMENT REPORT

July 24, 2017

ditch. Stage-storage discharge characteristics for the pond were calculated using spreadsheet analysis and incorporated into the hydrologic model presented in Appendix B. Tables highlighting the details regarding the parameters and results are presented below.

Table 1 – SWM Facility Design Characteristics

Parameter	SWM Characteristic
Total Contributing Area	1.72 ha
Total Percent Impervious	100%
Pond Elevations (Bottom/Top)	78.05 m / 79.35 m
Water Quality Control	
TSS Removal Efficiency Required	80%
Grassed Swale / Dry Facility	76% / 60%
Extended Detention Volume Required / Provided	482 m <sup>3</sup> / 482 m <sup>3</sup>
Extended Detention Drawdown Time	27 hours
Outlet Details	
Outlet Pipe Elevation / Diameter	78.05 m / 100 mm
Overflow Weir Invert Elevation / Length	79.05 m / 5 m

Table 2 – Stormwater Management Facility Operating Characteristics

Storm Event	25 mm	2-year	5-year	10-year	100-year
Existing Flows to Bath Road Culvert (m <sup>3</sup> /s)	0.81	1.47	2.04	2.43	3.68
Proposed Flows to Bath Road Culvert (m <sup>3</sup> /s)	0.81	1.43	1.97	2.33	3.47
Proposed Flows to SWM Facility (m <sup>3</sup> /s)	0.09	0.19	0.28	0.34	0.53
Proposed Flows from SWM Facility (m <sup>3</sup> /s)	0.01	0.01	0.02	0.02	0.02
Maximum Storage Used (m <sup>3</sup> )	110	300	460	580	980
Maximum Ponding Elevation (m)	78.25	78.46	78.61	78.71	79.02
Maximum Ponding Depth (m)	0.20	0.41	0.56	0.66	0.97
Drawdown Time (hrs)	5	15	26	35	70

As shown in Table 2, water quantity control targets have been met as the post-development peak flow rates are less than the target discharges established using existing conditions modeling.

#### 2.4.4 Design Considerations

As the dry pond facility is proposed to be constructed in summer 2017, additional measures have been included in the design of the MLA to minimize the potential for sediment to migrate



AMHERST ISLAND WIND ENERGY PROJECT  
MAINLAND LAYDOWN AREA EROSION AND SEDIMENT CONTROL PLAN AND STORMWATER  
MANAGEMENT REPORT

July 24, 2017

offsite, prior to site vegetation becoming fully established. The perimeter berms around the MLA are covered by straw matting and seeded, the vegetated swale upstream of the dry pond is covered by Anti-Wash Geojute to minimize erosion potential of designed features.

The outlet of the dry pond facility will be protected by light duty silt fencing. Light duty silt fencing was chosen for ease of installation and maintenance, as it can be manipulated without the assistance of machinery due to limited access to the outlet structure.

Due to the temporary nature of the MLA and to maximize the amount of working area, the dry pond facility has been sized to contain the 10-year rainfall event. Under larger storm events, shallow ponding will occur within the limits of the graveled area on the site. The 100-year ponding limit will be identified on site. Ponding depths on the graveled area of the site will not exceed 0.09 meters, which still allows for vehicle passage.

July 24, 2017

### 3.0 ASSESSMENT OF POTENTIAL HYDROLOGIC IMPACTS AND MITIGATION – DURING-CONSTRUCTION PHASE (ESC)

An assessment of the erosion potential of the construction area was completed following the methodology outlined in the Environmental Guide for Erosion and Sediment Control During Construction of Highway Projects (MTO, 2015). The erosion potential is based on an assessment of three primary factors, namely slope gradient, slope length and soil texture (erodibility), with the resultant designation of either “low”, “moderate”, or “high” erosion potential. The relative level of erosion potential dictates, to some extent, the comprehensiveness of the resultant ESC system design, monitoring, and maintenance program.

The existing and proposed (post-construction) condition gradients on the Project site can be classified as low (0 – 10% - Overland flow paths), with predominantly long slopes (greater than 70 m). Site soils are comprised primarily of silt clay tills and clays, which are considered to represent a medium erodibility potential (Table 5.1, Environmental Guide). Therefore, based on this classification, the site has a “moderate” erosion potential.

#### 3.1 DURING CONSTRUCTION DEWATERING

Since no significant excavation is proposed within the MLA, the proposed construction activities are not expected to intercept the local water table. Pumping rates are not anticipated to exceed 50,000 litres per day or the requirements of an Environmental Activity Sector Registration application approval. However, if groundwater is encountered during excavation, it should be removed using a conventional sump drainage system and pumped into a holding tank situated onsite. Groundwater within the holding tank should be tested for the contaminants of concern, manifested and trucked offsite to a disposal facility, in accordance with the guidance presented in the Soil/Groundwater Management Program and Health & Safety Plan – North Parcel (Stantec, 2017).

Detailed pumping records will be kept on site to demonstrate that maximum pumping rates are not exceeded.

#### 3.2 EROSION AND SEDIMENT CONTROL PLAN

The various construction activities required to construct the MLA include topsoil removal, minor grading activities, and general construction traffic. If left unmitigated, these activities will result in impacts ranging from disturbance of at-surface soils and exposure of the native sub-soils to potential erosion and sediment transport to offsite locations.

AMHERST ISLAND WIND ENERGY PROJECT  
MAINLAND LAYDOWN AREA EROSION AND SEDIMENT CONTROL PLAN AND STORMWATER  
MANAGEMENT REPORT

July 24, 2017

Erosion control will be achieved primarily through the excavation-and-backfill methods of construction and by limiting the duration of exposure of disturbed soils inherent in the construction process. For example, laydown area construction includes the removal of topsoil and sub-soils as necessary to achieve a competent base, followed by the placement of granular material back to proposed grade elevations (or marginally above); hence, the work areas are generally protected from erosion and sediment transport since they are lower than the surrounding ground surface. Further, at any given location, these works will be completed in short order, providing little opportunity for sub-soils to be disturbed and entrained in storm runoff.

In addition to limiting the potential for erosion, sediment control measures will be implemented prior to any grading or servicing works commencing as shown on the accompanying plan (Drawing C104), and include, but not necessarily be limited to, the following items:

- Sediment and erosion control measures should be implemented prior to construction and maintained during the construction phase to prevent entry of sediment into the water:
  - Erect silt fence (per OPSD 219.110) on the downstream sides of disturbed areas within 30 m of the buffers to environmental features and around entirety of temporarily stockpiled soils;
  - Temporarily stockpiled excavated native materials and imported materials with a  $D_{50}$  less than 4.75 mm (typical  $D_{50}$  of Granular A) will be covered with rolled erosion control products when the material is expected to be left in place in excess of 10 days, while imported materials with a  $D_{50}$  of 4.75 mm or greater can remain uncovered. Granular A and B (Type II) gradation requirements allow up to 55% percent passing a 4.75 mm sieve (#4 sieve), and may be stockpiled without covering with rolled erosion control products. Uncovered stockpiles will be surrounded with a double layer of light duty silt fence (1 m separation between layers) to provide a secondary layer of protection from sediment migration;
  - Topsoil stockpiles expected to be left in place in excess of 30 days may be stabilized with vegetation, i.e. Hydroseeding as referenced in the GGHA ESC Guidelines (GGHCA, 2006) instead of a rolled erosion control product;
  - In the event of inclement weather or unfavourable terrain for construction, construction best practices, such as temporary rig-mats may be used to prevent disruption of surface soils and vegetative cover by construction vehicles and equipment. As these measures are within the constructible areas of the project, it is not anticipated that offsite flows will increase from proposed conditions;
  - Topsoil stockpiles should be sufficiently distant from watercourses to preclude sediment inputs due to erosion of stored soil materials;
  - Topsoil berms are to be stabilized with straw matting;
  - Grassed swales and stormwater management vegetated swales are to be stabilized with Antiwash Geojute or approved equivalent;



July 24, 2017

- Additional erosion and sediment controls may be required due to unforeseen circumstances, changing site conditions or if the proposed controls do not achieve their anticipated result. In these circumstances, additional controls may be installed consistent with GGHCA ESC Guidelines and MOECC SWMPD Manual. The locations and application of the controls will be approved by a qualified erosion and sediment control inspector prior to their installation; and
- If the sediment and erosion control measures are not functioning properly and there is immediate risk of sediment discharges to the downstream environment, no further work should occur until the sediment and/or erosion problem is addressed.
- All materials and equipment used for the purpose of site preparation and Project construction should be operated and stored in a manner that prevents any deleterious substance (e.g., petroleum products, silt, etc.) from entering nearby watercourses:
  - Any stockpiled materials should be stored and stabilized away from watercourses;
  - Refuelling and maintenance of construction equipment should occur in designated areas, a minimum of 100 m from a water body;
  - As appropriate, spills should be reported to the MOECC Spills Action Centre;
  - Any part of equipment entering water should be free of fluid leaks and externally cleaned/degreased to prevent any deleterious substance from entering the water;
  - Only clean material, free of fine particulate matter should be placed in the water: and
  - A 100 mm PVC end cap will be stored on-site to plug the upstream end of the SWM facility outlet pipe in the event of a spill.
- Revegetate all disturbed areas where construction is not expected for 30 days with a minimum 50 mm of topsoil and hydro-seeding or other stabilizing vegetation / erosion protection measures (per OPSS 804). If, given seasonal restriction or other revegetation limiting factors, the disturbed area should be stabilized against erosion impacts by non-vegetated means such as erosion control blankets.

The ESC measures shall be maintained in good repair during the entire construction period, and removed as contributing drainage areas are restored and stabilized. ESC measures shall not be removed until a qualified inspector determines that the measures are no longer required and the risk of surface water and environmental impacts from construction activities are negligible. In addition, the condition of erosion control works, their overall performance, and any repairs, replacement, or modifications to the installed item shall be noted in logbooks to be kept on-site.

### 3.3 EROSION AND SEDIMENTATION CONTROL MONITORING PLAN

To ensure the effectiveness of the various erosion and sediment control measures, a routine program should be implemented which includes the inspection of the erosion and sediment controls daily and after each significant rainfall event (10 mm), and immediate repair of any



AMHERST ISLAND WIND ENERGY PROJECT  
MAINLAND LAYDOWN AREA EROSION AND SEDIMENT CONTROL PLAN AND STORMWATER  
MANAGEMENT REPORT

July 24, 2017

deficiencies. The program will be compliant with REA condition H7. Non-urgent repairs (i.e., no immediate risk of sediment discharges to the downstream environment) will be completed within 48 hours of identifying the deficiency, or prior to the next anticipated rainfall event, whichever is less. This program will consist of the following activities:

- Visual inspection of the ESC measures to ensure discharged flows are generally free of sediment and turbidity;
- Inspection of vegetation protection and silt fencing to ensure that they are maintained in good repair;
- Removal of construction debris that may accumulate; and
- Implementation of remedial measures including erosion stabilization, repair of damaged fencing and any other remediation, where required.

If the monitoring program outlined above indicates a persistent problem, then the following steps should be undertaken to determine appropriate mitigative measures (if step 1 does not resolve the issue, proceed to step 2):

1. Analysis of the monitoring information and field visits as required, determine the cause of the problem, and develop a mitigation plan to address the issue in consultation with a certified ESC inspector.
  - a. Implement additional mitigation measures and monitor the results.
2. Convene a meeting with the appropriate review agencies to discuss the problem.
  - a. Develop a consensus on a proposed plan of action to resolve the problem in consultation with agency staff.
  - b. Implement additional mitigation measures and monitor the results

### 3.4 LONG TERM EROSION AND SEDIMENT CONTROL

Upon restoration of the MLA with native topsoil, replanting with a grass seed mix will be undertaken. Approximately, one year after construction a survey will be undertaken to ensure that long-term erosion control measures have been effective. Seeded or replanted areas will be inspected to ensure that revegetation measures were successful and reseeding or replanting will occur where necessary.

If erosion control measures are found to be less than fully effective during this survey, reseeding or replanting of problem areas will take place. Should there be residual effects noted during post-construction monitoring, advice on contingency measures will be sought out and applied.

July 24, 2017

## 4.0 CONCLUSIONS AND RECOMMENDATIONS

Based on the preceding design report the following conclusions can be drawn:

- Water quality and quantity control for the MLA is provided using a vegetated filter strip, grassed swale, and dry pond facility.
- The proposed SWM measures act as a treatment train to provide the necessary water quality control.

Based on the findings of this report, the following recommendations are provided:

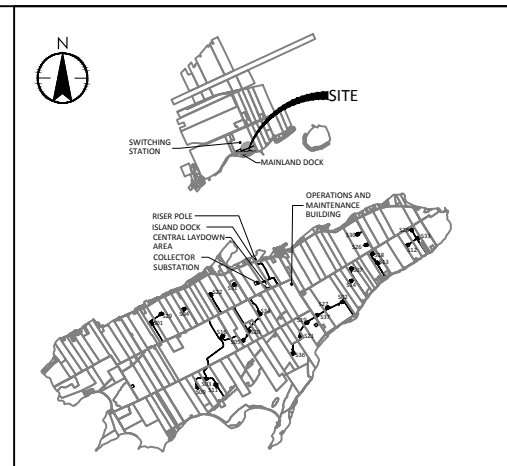
- The proposed SWM and ESC measures be implemented for the subject site.
- The Monitoring and Maintenance Program be undertaken to ensure that the proposed measures function appropriately.

## FIGURES



V:\01614\active\133560100\design\drawing\civil\sheet\_files\SWM\133560100C-FIG-PR-Mainland\_Laydown\_Area.dwg  
2017/07/13 4:36 PM By: Robb, Brad

ORIGINAL SHEET - ANSI B



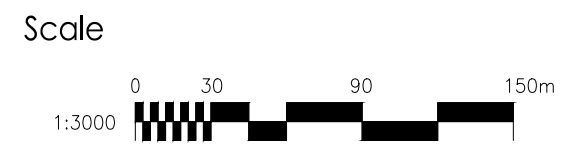
**KEY PLAN**  
N.T.S

April, 2017  
160960595

300 Hagey Blvd. Suite 100  
Waterloo, ON, N2L 0A4  
Tel. 519.579.4410  
www.stantec.com

**Legend**

- AREA NUMBER
- CONTRIBUTING AREA (ha)
- OVERLAND FLOW ROUTE
- DRAINAGE BOUNDARY



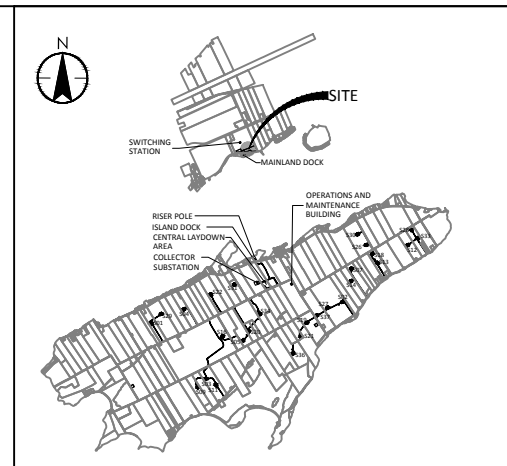
Client/Project  
ALGONQUIN POWER CO.  
AMHERST ISLAND WIND ENERGY PROJECT

Figure No.  
**FIGURE 1**

Title  
**MAINLAND LAYDOWN AREA  
PRE-DEVELOPMENT CATCHMENT PLAN**

V:\01614\active\133560100\design\drawing\civil\sheet\_files\SWM\133560100C-FIG-POST-Mainland\_Laydown\_Area.dwg  
 2017/07/13 4:42 PM By: Robb, Brad

ORIGINAL SHEET - ANSI B



**KEY PLAN**  
N.T.S

April, 2017  
160960595

**Stantec**  
 300 Hagey Blvd. Suite 100  
 Waterloo, ON, N2L 0A4  
 Tel. 519.579.4410  
 www.stantec.com

**Legend**

- AREA NUMBER
- CONTRIBUTING AREA (ha)
- OVERLAND FLOW ROUTE
- DRAINAGE BOUNDARY

**Scale**

1:3000

Client/Project  
 ALGONQUIN POWER CO.  
 AMHERST ISLAND WIND ENERGY PROJECT

Figure No.  
**FIGURE 2**

Title  
**MAINLAND LAYDOWN AREA  
 POST-DEVELOPMENT CATCHMENT PLAN**

APPENDIX A  
EXISTING CONDITIONS HYDROLOGY

Subject: CN Calculation - Existing  
 Project: Amherst Island Wind Energy Project - Mainland Laydown Area  
 Project No.: 1609-60595  
 Client: Windlectric  
 Date: July 5, 2017

TABLE OF CURVE NUMBERS (CN's)								
Land Use	Hydrologic Soil Type							Source
	A	AB	B	BC	C	CD	D	
Meadow "Good"	30	44	58	65	71	75	78	MTO
Woodlot "Fair"	36	48	60	67	73	76	79	MTO
Lawns "Good"	39	50	61	68	74	77	80	USDA
Pasture/Range	58	62	65	71	76	79	81	MTO
Crop	66	70	74	78	82	84	86	MTO
Gravel	76	81	85	87	89	90	91	Chin
Bare Soil (Fallow)	77	82	86	89	91	93	94	MTO
Impervious	98	98	98	98	98	98	98	MTO

MTO - Ministry of Transportation Ontario Drainage Manual (1997), Design Chart 1.09-Soil/Land Use Curve Numbers  
 USDA - United States Department of Agriculture (2004), National Engineering Handbook, Part 630 Hydrology, Chapter 9 Hydrologic Soil Cover Complexes

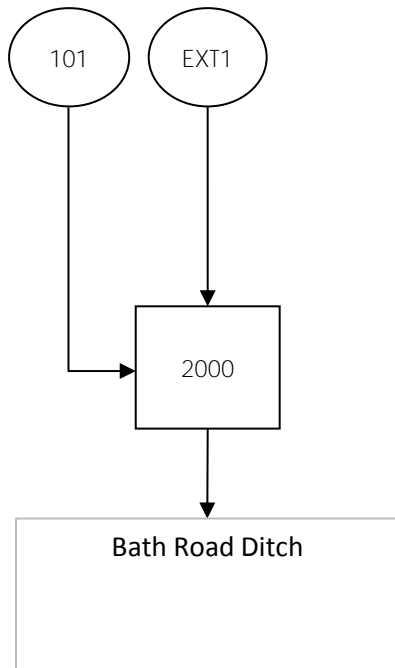
HYDROLOGIC SOIL TYPE (%) - Existing Conditions								
Catchment	Hydrologic Soil Type							TOTAL
	A	AB	B	BC	C	CD	D	
EXT1					100			100
101					100			100
								0
								0
								0
								0

LAND USE (%) - Existing Conditions									
Catchment	Meadow	Woodlot	Lawns	Pasture Range	Crop	Bare Soil	Gravel	Impervious	Total
EXT1			5					95	100
101			66					34	100

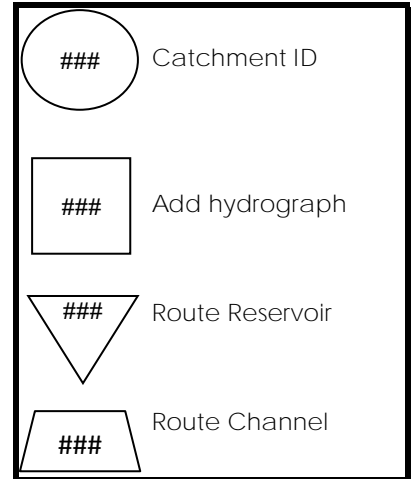
CURVE NUMBER (CN) - Existing Conditions										
Catchment	Meadow	Woodlot	Lawns	Pasture Range	Crop	Bare Soil	Gravel	Impervious	Weighted CN w/ imp area	Weighted CN w/o imp area
EXT1			4					93	97	74
101			49					33	82	74

Notes:  
 AMC II assumed  
 Hydrological Soil Groups taken from MTO Drainage Manual

**Subject:** Pre-Development SWMHYMO Schematic  
**Project:** Amherst Island Wind Energy Project - Mainland Laydown Area  
**Project No.:** 1609-60595  
**Client:** Windlectric  
**Date:** July 5, 2017



Legend



AMHERST ISLAND - MLA

PRE-DEVELOPMENT CONDITIONS SWMHYMO OUTPUT

```

=====
SSSSS W W M M H H Y Y M M OOO          999 999 =====
S      W W W MM MM H H Y Y MM MM O O    9 9 9 9
SSSSS W W W M M M HHHHH Y M M M O O ## 9 9 9 9 Ver 4.05
S      W W M M H H Y M M O O          9999 9999 Sept 2011
SSSSS W W M M H H Y M M OOO          9 9 9 9 =====
                                           9 9 9 9 # 4730904

StormWater Management Hydrologic Model      999 999 =====

*****
***** SWMHYMO Ver/4.05 *****
***** A single event and continuous hydrologic simulation model *****
***** based on the principles of HYMO and its successors *****
***** OTHYMO-83 and OTHYMO-89. *****
*****
***** Distributed by: J.F. Sabourin and Associates Inc. *****
***** Ottawa, Ontario: (613) 836-3884 *****
***** Gatineau, Quebec: (819) 243-6858 *****
***** E-Mail: swmhymo@jfsa.Com *****
*****
+++++++ Licensed user: Stantec Consulting Ltd. (Kitchener) ++++++
+++++++ Kitchener SERIAL#:4730904 ++++++
+++++++

*****
***** +++++ PROGRAM ARRAY DIMENSIONS +++++ *****
***** Maximum value for ID numbers : 10 *****
***** Max. number of rainfall points: 105408 *****
***** Max. number of flow points : 105408 *****
*****

***** D E T A I L E D O U T P U T *****
*****
* DATE: 2017-07-05 TIME: 10:27:02 RUN COUNTER: 000617 *
* Input filename: Z:\Temp\Amherst\0595EX1.dat *
* Output filename: Z:\Temp\Amherst\0595EX1.out *
* Summary filename: Z:\Temp\Amherst\0595EX1.sum *
* User comments: *
* 1: _____ *
* 2: _____ *
* 3: _____ *
*****

-----
001:0001-----
-
*# Project Name: [Amherst Island MLA] Project Number: [1609-60595]
*# Date : 07-05-2017
*# Modeller : [NE]
*# Company : Stantec Consulting Ltd. (London)
*# License # : 4730904
*#
*# EXISTING CONDITIONS
*# 25 mm Water Quality Event
*# 2, 5, 10, 100-year 24-hour SCS Design Storm
*#
*#
-----

```

```

| START | Project dir.: Z:\Temp\Amherst\
|-----| Rainfall dir.: Z:\Temp\Amherst\
TZERO = .00 hrs on 0
METOUT= 2 (output = METRIC)
NRUN = 001
NSTORM= 1
# 1=25mm.4hr
-----
001:0002-----
|-----|
| READ STORM | Filename: 25 mm, 4hr Chicago Storm - Kitchener IDF
| Ptotal= 25.00 mm | Comments: 25 mm, 4hr Chicago Storm - Kitchener IDF
-----
TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
.08 1.465 | 1.08 4.024 | 2.08 5.764 | 3.08 2.074
.17 1.540 | 1.17 4.814 | 2.17 4.969 | 3.17 1.977
.25 1.625 | 1.25 6.025 | 2.25 4.374 | 3.25 1.889
.33 1.720 | 1.33 8.114 | 2.33 3.913 | 3.33 1.810
.42 1.829 | 1.42 12.526 | 2.42 3.545 | 3.42 1.737
.50 1.955 | 1.50 27.198 | 2.50 3.245 | 3.50 1.671
.58 2.101 | 1.58 74.855 | 2.58 2.994 | 3.58 1.610
.67 2.274 | 1.67 31.410 | 2.67 2.782 | 3.67 1.553
.75 2.482 | 1.75 16.819 | 2.75 2.601 | 3.75 1.501
.83 2.736 | 1.83 11.357 | 2.83 2.443 | 3.83 1.453
.92 3.055 | 1.92 8.563 | 2.92 2.305 | 3.92 1.408
1.00 3.468 | 2.00 6.882 | 3.00 2.183 | 4.00 1.366
-----
001:0003-----
-
*# External Drainage Area - Former Invista Site
*#-----
| DESIGN NASHYD | Area (ha)= 9.90 Curve Number (CN)=97.00
| 01:EXT1 DT= 2.00 | Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
|-----| U.H. Tp(hrs)= .180
Unit Hyd Qpeak (cms)= 2.101
PEAK FLOW (cms)= .702 (i)
TIME TO PEAK (hrs)= 1.750
RUNOFF VOLUME (mm)= 17.613
TOTAL RAINFALL (mm)= 25.000
RUNOFF COEFFICIENT = .705
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
-----
001:0004-----
-
*# Area of Interest - lawns and parking areas
*#-----
| DESIGN NASHYD | Area (ha)= 5.34 Curve Number (CN)=82.00
| 02:101 DT= 2.00 | Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
|-----| U.H. Tp(hrs)= .220
Unit Hyd Qpeak (cms)= .927
PEAK FLOW (cms)= .117 (i)

```

AMHERST ISLAND - MLA

PRE-DEVELOPMENT CONDITIONS SWMHYMO OUTPUT

TIME TO PEAK (hrs)= 1.833  
 RUNOFF VOLUME (mm)= 6.968  
 TOTAL RAINFALL (mm)= 25.000  
 RUNOFF COEFFICIENT = .279

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 001:0005-----  
 -

\*#\*\*\*\*\*  
 \*# Total Flow to Bath Road Culvert  
 \*#\*\*\*\*\*

ADD HYD ( 2000)   ID: NHYD	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	DWF (cms)
ID1 01:EXT1	9.90	.702	1.75	17.61	.000
+ID2 02:101	5.34	.117	1.83	6.97	.000
=====					
SUM 03: 2000	15.24	.810	1.75	13.88	.000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----  
 001:0006-----  
 -

\*\* END OF RUN : 1

\*\*\*\*\*

-----  
 | START | Project dir.: Z:\Temp\Amherst\  
 |-----| Rainfall dir.: Z:\Temp\Amherst\  
 TZERO = .00 hrs on 0  
 METOUT= 2 (output = METRIC)  
 NRUN = 002  
 NSTORM= 1  
 # 1-AI2SCS.24H  
 -----

-----  
 002:0002-----  
 -

\*#\*\*\*\*\*  
 \*# Project Name: [Amherst Island MLA] Project Number: [1609-60595]  
 \*# Date : 07-05-2017  
 \*# Modeller : [NE]  
 \*# Company : Stantec Consulting Ltd. (London)  
 \*# License # : 4730904  
 \*#\*\*\*\*\*

\*#  
 \*# EXISTING CONDITIONS  
 \*# 25 mm Water Quality Event  
 \*# 2, 5, 10, 100-year 24-hour SCS Design Storm  
 \*#  
 \*#\*\*\*\*\*

-----  
 002:0002-----  
 -

| READ STORM | Filename: Amherst Island MTO IDF (44 9' 15"N, 76 4  
 | Ptotal= 54.10 mm | Comments: Amherst Island MTO IDF (44 9' 15"N, 76 4

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.25	.595	6.25	1.082	12.25	7.790	18.25	.974
.50	.595	6.50	1.082	12.50	7.790	18.50	.974
.75	.595	6.75	1.082	12.75	4.003	18.75	.974
1.00	.595	7.00	1.082	13.00	4.003	19.00	.974
1.25	.595	7.25	1.082	13.25	.757	19.25	.974
1.50	.595	7.50	1.082	13.50	.757	19.50	.974
1.75	.595	7.75	1.082	13.75	4.436	19.75	.974
2.00	.595	8.00	1.082	14.00	4.436	20.00	.974
2.25	.703	8.25	1.461	14.25	1.623	20.25	.649
2.50	.703	8.50	1.461	14.50	1.623	20.50	.649
2.75	.703	8.75	1.461	14.75	1.623	20.75	.649
3.00	.703	9.00	1.461	15.00	1.623	21.00	.649
3.25	.703	9.25	1.731	15.25	1.623	21.25	.649
3.50	.703	9.50	1.731	15.50	1.623	21.50	.649
3.75	.703	9.75	1.948	15.75	1.623	21.75	.649
4.00	.703	10.00	1.948	16.00	1.623	22.00	.649
4.25	.866	10.25	2.489	16.25	.974	22.25	.649
4.50	.866	10.50	2.489	16.50	.974	22.50	.649
4.75	.866	10.75	3.354	16.75	.974	22.75	.649
5.00	.866	11.00	3.354	17.00	.974	23.00	.649
5.25	.866	11.25	5.194	17.25	.974	23.25	.649
5.50	.866	11.50	5.194	17.50	.974	23.50	.649
5.75	.866	11.75	22.506	17.75	.974	23.75	.649
6.00	.866	12.00	59.726	18.00	.974	24.00	.649

-----  
 002:0003-----  
 -

\*#\*\*\*\*\*  
 \*# External Drainage Area - Former Invista Site  
 \*#\*\*\*\*\*

DESIGN NASHYD	Area (ha)	Curve Number (CN)
01:EXT1 DT= 2.00	9.90	97.00
	Ia (mm)= 1.500	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .180	

Unit Hyd Qpeak (cms)= 2.101  
 PEAK FLOW (cms)= 1.162 (i)  
 TIME TO PEAK (hrs)= 12.072  
 RUNOFF VOLUME (mm)= 45.765  
 TOTAL RAINFALL (mm)= 54.100  
 RUNOFF COEFFICIENT = .846

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 002:0004-----  
 -

\*#\*\*\*\*\*  
 \*# Area of Interest - lawns and parking areas  
 \*#\*\*\*\*\*

DESIGN NASHYD	Area (ha)	Curve Number (CN)
02:101 DT= 2.00	5.34	82.00
	Ia (mm)= 1.500	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .220	

Unit Hyd Qpeak (cms)= .927  
 PEAK FLOW (cms)= .314 (i)

AMHERST ISLAND - MLA

TIME TO PEAK (hrs)= 12.108  
 RUNOFF VOLUME (mm)= 25.534  
 TOTAL RAINFALL (mm)= 54.100  
 RUNOFF COEFFICIENT = .472

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

002:0005-----

```

*#*****
*# Total Flow to Bath Road Culvert
*#*****
  
```

ADD HYD (	2000)	ID: NHYD	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	DWF (cms)
ID1	01:EXT1		9.90	1.162	12.07	45.76	.000
+ID2	02:101		5.34	.314	12.11	25.53	.000
SUM 03:			2000	15.24	1.472	12.07	38.68 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

002:0006-----

002:0002-----

\*\* END OF RUN : 4

```

| START | Project dir.: Z:\Temp\Amherst\
|-----| Rainfall dir.: Z:\Temp\Amherst\
  TZERO = .00 hrs on 0
  METOUT= 2 (output = METRIC)
  NRUN = 005
  NSTORM= 1
  # 1-AI5SCS.24H
  
```

005:0002-----

```

*# Project Name: [Amherst Island MLA] Project Number: [1609-60595]
*# Date : 07-05-2017
*# Modeller : [NE]
*# Company : Stantec Consulting Ltd. (London)
*# License # : 4730904
*#
*# EXISTING CONDITIONS
*# 25 mm Water Quality Event
*# 2, 5, 10, 100-year 24-hour SCS Design Storm
*#
*#
  
```

PRE-DEVELOPMENT CONDITIONS SWMHYMO OUTPUT

005:0002-----

```

| READ STORM | Filename: Amherst Island MTO IDF (44 9' 15"N, 76 4
| Ptotal= 71.40 mm | Comments: Amherst Island MTO IDF (44 9' 15"N, 76 4
  
```

TIME (hrs)	RAIN (mm/hr)	TIME (hrs)	RAIN (mm/hr)	TIME (hrs)	RAIN (mm/hr)	TIME (hrs)	RAIN (mm/hr)
.25	.785	6.25	1.428	12.25	10.282	18.25	1.285
.50	.785	6.50	1.428	12.50	10.282	18.50	1.285
.75	.785	6.75	1.428	12.75	5.284	18.75	1.285
1.00	.785	7.00	1.428	13.00	5.284	19.00	1.285
1.25	.785	7.25	1.428	13.25	3.713	19.25	1.285
1.50	.785	7.50	1.428	13.50	3.998	19.50	1.285
1.75	.785	7.75	1.428	13.75	2.999	19.75	1.285
2.00	.785	8.00	1.428	14.00	2.999	20.00	1.285
2.25	.928	8.25	1.928	14.25	2.142	20.25	.857
2.50	.928	8.50	1.928	14.50	2.142	20.50	.857
2.75	.928	8.75	1.928	14.75	2.142	20.75	.857
3.00	.928	9.00	1.928	15.00	2.142	21.00	.857
3.25	.928	9.25	2.285	15.25	2.142	21.25	.857
3.50	.928	9.50	2.285	15.50	2.142	21.50	.857
3.75	.928	9.75	2.570	15.75	2.142	21.75	.857
4.00	.928	10.00	2.570	16.00	2.142	22.00	.857
4.25	1.142	10.25	3.284	16.25	1.285	22.25	.857
4.50	1.142	10.50	3.284	16.50	1.285	22.50	.857
4.75	1.142	10.75	4.427	16.75	1.285	22.75	.857
5.00	1.142	11.00	4.427	17.00	1.285	23.00	.857
5.25	1.142	11.25	6.854	17.25	1.285	23.25	.857
5.50	1.142	11.50	6.854	17.50	1.285	23.50	.857
5.75	1.142	11.75	29.702	17.75	1.285	23.75	.857
6.00	1.142	12.00	78.826	18.00	1.285	24.00	.857

005:0003-----

```

*# External Drainage Area - Former Invista Site
*#
  
```

DESIGN NASHYD	Area (ha)	Curve Number (CN)
01:EXT1 DT= 2.00	9.90	97.00
	Ia (mm)= 1.500	# of Linear Res.(N)= 3.00
	U.H. Tp(hrs)= .180	

```

Unit Hyd Qpeak (cms)= 2.101
PEAK FLOW (cms)= 1.567 (i)
TIME TO PEAK (hrs)= 12.072
RUNOFF VOLUME (mm)= 62.836
TOTAL RAINFALL (mm)= 71.398
RUNOFF COEFFICIENT = .880
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
  
```

005:0004-----

```

*# Area of Interest - lawns and parking areas
*#
  
```

DESIGN NASHYD	Area (ha)	Curve Number (CN)
02:101 DT= 2.00	5.34	82.00
	Ia (mm)= 1.500	# of Linear Res.(N)= 3.00



AMHERST ISLAND - MLA

PRE-DEVELOPMENT CONDITIONS SWMHYMO OUTPUT

```

----- U.H. Tp(hrs)= .220
Unit Hyd Qpeak (cms)= .927
PEAK FLOW (cms)= .481 (i)
TIME TO PEAK (hrs)= 12.108
RUNOFF VOLUME (mm)= 38.882
TOTAL RAINFALL (mm)= 71.398
RUNOFF COEFFICIENT = .545
    
```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
005:0005-----
*#*****
*# Total Flow to Bath Road Culvert
*#*****
| ADD HYD ( 2000) | ID: NHYD      AREA   QPEAK  TPEAK  R.V.   DWF
-----
                    (ha)   (cms)  (hrs)  (mm)   (cms)
ID1 01:EXT1      9.90   1.567  12.07  62.84  .000
+ID2 02:101      5.34   .481   12.11  38.88  .000
=====
SUM 03:          2000   15.24   2.044  12.07  54.44  .000
    
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```

-----
005:0006-----
-----
005:0002-----
-----
005:0002-----
** END OF RUN : 9
    
```

```

-----
| START | Project dir.: Z:\Temp\Amherst\
----- Rainfall dir.: Z:\Temp\Amherst\
TZERO = .00 hrs on 0
METOUT= 2 (output = METRIC)
NRUN = 010
NSTORM= 1
# 1=AI10SCS.24H
    
```

```

-----
010:0002-----
*#*****
*# Project Name: [Amherst Island MLA] Project Number: [1609-60595]
*# Date : 07-05-2017
*# Modeller : [NE]
*# Company : Stantec Consulting Ltd. (London)
*# License # : 4730904
    
```

```

*#*****
*#
*# EXISTING CONDITIONS
*# 25 mm Water Quality Event
*# 2, 5, 10, 100-year 24-hour SCS Design Storm
*#
*#*****
*#
    
```

```

-----
010:0002-----
-----
| READ STORM | Filename: Amherst Island MTO IDF (44 9' 15"N, 76 4
| Ptotal= 83.00 mm | Comments: Amherst Island MTO IDF (44 9' 15"N, 76 4
    
```

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.25	.913	6.25	1.660	12.25	11.952	18.25	1.494
.50	.913	6.50	1.660	12.50	11.952	18.50	1.494
.75	.913	6.75	1.660	12.75	6.142	18.75	1.494
1.00	.913	7.00	1.660	13.00	6.142	19.00	1.494
1.25	.913	7.25	1.660	13.25	1.162	19.25	1.494
1.50	.913	7.50	1.660	13.50	1.162	19.50	1.494
1.75	.913	7.75	1.660	13.75	6.806	19.75	1.494
2.00	.913	8.00	1.660	14.00	6.806	20.00	1.494
2.25	1.079	8.25	2.241	14.25	2.490	20.25	.996
2.50	1.079	8.50	2.241	14.50	2.490	20.50	.996
2.75	1.079	8.75	2.241	14.75	2.490	20.75	.996
3.00	1.079	9.00	2.241	15.00	2.490	21.00	.996
3.25	1.079	9.25	2.656	15.25	2.490	21.25	.996
3.50	1.079	9.50	2.656	15.50	2.490	21.50	.996
3.75	1.079	9.75	2.988	15.75	2.490	21.75	.996
4.00	1.079	10.00	2.988	16.00	2.490	22.00	.996
4.25	1.328	10.25	3.818	16.25	1.494	22.25	.996
4.50	1.328	10.50	3.818	16.50	1.494	22.50	.996
4.75	1.328	10.75	5.146	16.75	1.494	22.75	.996
5.00	1.328	11.00	5.146	17.00	1.494	23.00	.996
5.25	1.328	11.25	7.968	17.25	1.494	23.25	.996
5.50	1.328	11.50	7.968	17.50	1.494	23.50	.996
5.75	1.328	11.75	34.528	17.75	1.494	23.75	.996
6.00	1.328	12.00	91.632	18.00	1.494	24.00	.996

```

-----
010:0003-----
*#*****
*# External Drainage Area - Former Invista Site
*#*****
| DESIGN NASHYD | Area (ha)= 9.90 Curve Number (CN)=97.00
| 01:EXT1 DT= 2.00 | Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
----- U.H. Tp(hrs)= .180
    
```

```

Unit Hyd Qpeak (cms)= 2.101
PEAK FLOW (cms)= 1.838 (i)
TIME TO PEAK (hrs)= 12.072
RUNOFF VOLUME (mm)= 74.335
TOTAL RAINFALL (mm)= 83.000
RUNOFF COEFFICIENT = .896
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
    
```

AMHERST ISLAND - MLA

PRE-DEVELOPMENT CONDITIONS SWMHYMO OUTPUT

```
010:0004-----
-
*#*****
*# Area of Interest - lawns and parking areas
*#*****
| DESIGN NASHYD | Area (ha)= 5.34 Curve Number (CN)=82.00
| 02:101 DT= 2.00 | Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
|-----| U.H. Tp(hrs)= .220

Unit Hyd Qpeak (cms)= .927

PEAK FLOW (cms)= .600 (i)
TIME TO PEAK (hrs)= 12.108
RUNOFF VOLUME (mm)= 48.393
TOTAL RAINFALL (mm)= 83.000
RUNOFF COEFFICIENT = .583

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
```

```
010:0005-----
*#*****
*# Total Flow to Bath Road Culvert
*#*****
| ADD HYD ( 2000) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
|-----| (ha) (cms) (hrs) (mm) (cms)
| ID1 01:EXT1 | 9.90 1.838 12.07 74.34 .000
| +ID2 02:101 | 5.34 .600 12.11 48.39 .000
|-----|
| SUM 03: 2000 | 15.24 2.433 12.07 65.25 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.
```

```
010:0006-----
-
010:0002-----
-
010:0002-----
-
010:0002-----
-
010:0002-----
-
010:0002-----
-
** END OF RUN : 99
```

```
-----
| START | Project dir.: Z:\Temp\Amherst\
|-----| Rainfall dir.: Z:\Temp\Amherst\
TZERO = .00 hrs on 0
METOUT= 2 (output = METRIC)
NRUN = 100
```

```
NSTORM= 1
# 1=AI100SCS.24H
-----
100:0002-----
*#*****
*# Project Name: [Amherst Island MLA] Project Number: [1609-60595]
*# Date : 07-05-2017
*# Modeller : [NE]
*# Company : Stantec Consulting Ltd. (London)
*# License # : 4730904
*#*****
*#
*# EXISTING CONDITIONS
*# 25 mm Water Quality Event
*# 2, 5, 10, 100-year 24-hour SCS Design Storm
*#*****
*#
```

```
100:0002-----
-
| READ STORM | Filename: Amherst Island MTO IDF (44 9' 15"N, 76 4
| Ptotal= 119.80 mm | Comments: Amherst Island MTO IDF (44 9' 15"N, 76 4
|-----|
| TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
| hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
| .25 1.318 | 6.25 2.396 | 12.25 17.251 | 18.25 2.156
| .50 1.318 | 6.50 2.396 | 12.50 17.251 | 18.50 2.156
| .75 1.318 | 6.75 2.396 | 12.75 8.865 | 18.75 2.156
| 1.00 1.318 | 7.00 2.396 | 13.00 8.865 | 19.00 2.156
| 1.25 1.318 | 7.25 2.396 | 13.25 1.677 | 19.25 2.156
| 1.50 1.318 | 7.50 2.396 | 13.50 1.677 | 19.50 2.156
| 1.75 1.318 | 7.75 2.396 | 13.75 9.824 | 19.75 2.156
| 2.00 1.318 | 8.00 2.396 | 14.00 9.824 | 20.00 2.156
| 2.25 1.557 | 8.25 3.235 | 14.25 3.594 | 20.25 1.438
| 2.50 1.557 | 8.50 3.235 | 14.50 3.594 | 20.50 1.438
| 2.75 1.557 | 8.75 3.235 | 14.75 3.594 | 20.75 1.438
| 3.00 1.557 | 9.00 3.235 | 15.00 3.594 | 21.00 1.438
| 3.25 1.557 | 9.25 3.834 | 15.25 3.594 | 21.25 1.438
| 3.50 1.557 | 9.50 3.834 | 15.50 3.594 | 21.50 1.438
| 3.75 1.557 | 9.75 4.313 | 15.75 3.594 | 21.75 1.438
| 4.00 1.557 | 10.00 4.313 | 16.00 3.594 | 22.00 1.438
| 4.25 1.917 | 10.25 5.511 | 16.25 2.156 | 22.25 1.438
| 4.50 1.917 | 10.50 5.511 | 16.50 2.156 | 22.50 1.438
| 4.75 1.917 | 10.75 7.428 | 16.75 2.156 | 22.75 1.438
| 5.00 1.917 | 11.00 7.428 | 17.00 2.156 | 23.00 1.438
| 5.25 1.917 | 11.25 11.501 | 17.25 2.156 | 23.25 1.438
| 5.50 1.917 | 11.50 11.501 | 17.50 2.156 | 23.50 1.438
| 5.75 1.917 | 11.75 49.837 | 17.75 2.156 | 23.75 1.438
| 6.00 1.917 | 12.00 132.259 | 18.00 2.156 | 24.00 1.438
```

```
100:0003-----
-
*#*****
*# External Drainage Area - Former Invista Site
*#*****
| DESIGN NASHYD | Area (ha)= 9.90 Curve Number (CN)=97.00
| 01:EXT1 DT= 2.00 | Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
|-----| U.H. Tp(hrs)= .180
```

AMHERST ISLAND - MLA

PRE-DEVELOPMENT CONDITIONS SWMHYMO OUTPUT

Unit Hyd Qpeak (cms)= 2.101  
 PEAK FLOW (cms)= 2.690 (i)  
 TIME TO PEAK (hrs)= 12.037  
 RUNOFF VOLUME (mm)= 110.935  
 TOTAL RAINFALL (mm)= 119.801  
 RUNOFF COEFFICIENT = .926

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 100:0004-----  
 -

\*#\*\*\*\*\*  
 \*# Area of Interest - lawns and parking areas  
 \*#\*\*\*\*\*  
 -----  
 | DESIGN NASHYD | Area (ha)= 5.34 Curve Number (CN)=82.00  
 | 02:101 DT= 2.00 | Ia (mm)= 1.500 # of Linear Res.(N)= 3.00  
 -----  
 | U.H. Tp(hrs)= .220

Unit Hyd Qpeak (cms)= .927  
 PEAK FLOW (cms)= .998 (i)  
 TIME TO PEAK (hrs)= 12.108  
 RUNOFF VOLUME (mm)= 80.406  
 TOTAL RAINFALL (mm)= 119.801  
 RUNOFF COEFFICIENT = .671

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
 100:0005-----  
 -

\*#\*\*\*\*\*  
 \*# Total Flow to Bath Road Culvert  
 \*#\*\*\*\*\*  
 -----  
 | ADD HYD ( 2000) | ID: NHYD AREA QPEAK TPEAK R.V. DWF  
 (ha) (cms) (hrs) (mm) (cms)  
 -----  
 | ID1 01:EXT1 9.90 2.690 12.04 110.93 .000  
 +ID2 02:101 5.34 .998 12.11 80.41 .000  
 -----  
 | SUM 03: 2000 15.24 3.683 12.07 100.24 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----  
 100:0006-----  
 -

-----  
 100:0002-----  
 -

-----  
 100:0002-----  
 -

-----  
 100:0002-----  
 -

100:0002-----  
 -  
 FINISH  
 -----  
 \*  
 \*\*\*\*\*  
 \*  
 WARNINGS / ERRORS / NOTES  
 -----  
 Simulation ended on 2017-07-05 at 10:27:04  
 =====  
 =

APPENDIX B  
PROPOSED CONDITIONS HYDROLOGY

Subject: CN Calculation - Proposed  
 Project: Amherst Island Wind Energy Project - Mainland Laydown Area  
 Project No.: 1609-60595  
 Client: Windlectric  
 Date: July 5, 2017

TABLE OF CURVE NUMBERS (CN's)								Source
Land Use	Hydrologic Soil Type							
	A	AB	B	BC	C	CD	D	
Meadow "Good"	30	44	58	65	71	75	78	MTO
Woodlot "Fair"	36	48	60	67	73	76	79	MTO
Lawns "Good"	39	50	61	68	74	77	80	USDA
Pasture/Range	58	62	65	71	76	79	81	MTO
Crop	66	70	74	78	82	84	86	MTO
Gravel	76	81	85	87	89	90	91	Chin
Bare Soil (Fallow)	77	82	86	89	91	93	94	MTO
Impervious	98	98	98	98	98	98	98	MTO

MTO - Ministry of Transportation Ontario Drainage Manual (1997), Design Chart 1.09-Soil/Land Use Curve Numbers  
 USDA - United States Department of Agriculture (2004), National Engineering Handbook, Part 630 Hydrology, Chapter 9 Hydrologic Soil Cover Complexes

HYDROLOGIC SOIL TYPE (%) - Existing Conditions								
Catchment	Hydrologic Soil Type							TOTAL
	A	AB	B	BC	C	CD	D	
EXT1					100			100
EXT2					100			100
201					100			100
202					100			100
203					100			100

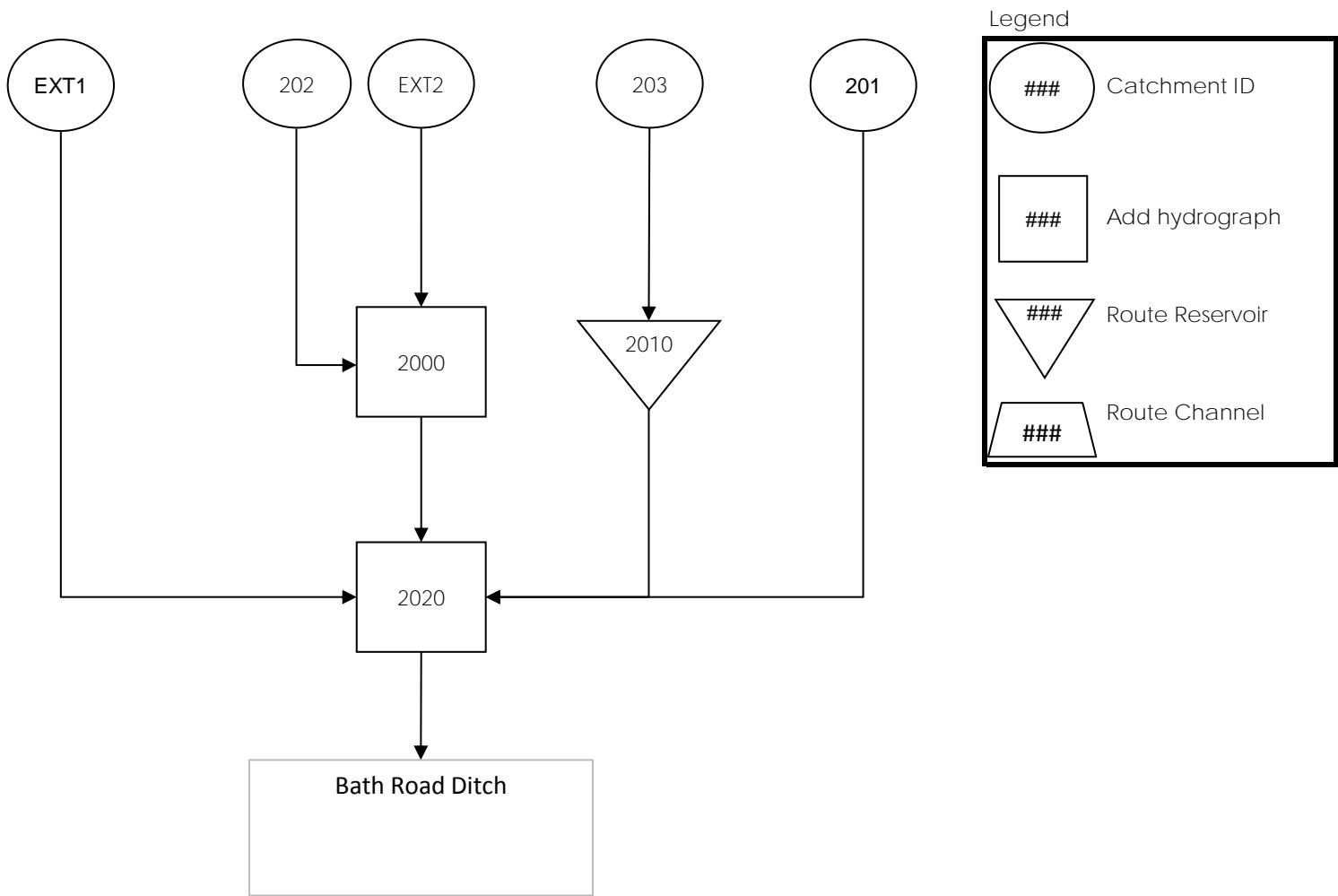
LAND USE (%) - Existing Conditions									
Catchment	Meadow	Woodlot	Lawns	Pasture Range	Crop	Bare Soil	Gravel	Impervious	Total
EXT1			5					95	100
EXT2			5					95	100
201			60					40	100
202			5					95	100
203							100		100

CURVE NUMBER (CN) - Existing Conditions										
Catchment	Meadow	Woodlot	Lawns	Pasture Range	Crop	Bare Soil	Gravel	Impervious	Weighted CN w/ imp area	Weighted CN w/o imp area
EXT1			4					93	97	74
EXT2			4					93	97	74
201			44					39	84	74
202			4					93	97	79
203							89		89	89

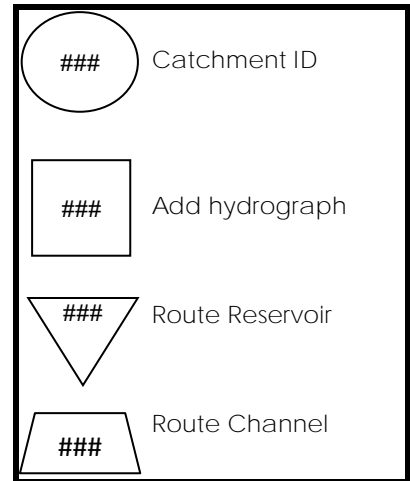
Notes:

AMC II assumed  
 Hydrological Soil Groups taken from MTO Drainage Manual

**Subject:** Post-Development SWMHYMO Schematic  
**Project:** Amherst Island Wind Energy Project - Mainland Laydown Area  
**Project No.:** 1609-60595  
**Client:** Windlectric  
**Date:** July 5, 2017



Legend



```

=====
SSSSS W W M M H H Y Y M M OOO          999 999 =====
S      W W W MM MM H H Y Y MM MM O O      9 9 9 9
SSSSS W W W M M M HHHHH Y M M M O O ##    9 9 9 9 Ver 4.05
S      W W M M H H Y M M O O              9999 9999 Sept 2011
SSSSS W W M M H H Y M M OOO              9 9
StormWater Management HYDrologic Model      9 9 9 9 # 4730904
                                           999 999 =====

*****
***** SWMHYMO Ver/4.05 *****
***** A single event and continuous hydrologic simulation model *****
***** based on the principles of HYMO and its successors *****
***** OTHYMO-83 and OTHYMO-89. *****
***** Distributed by: J.F. Sabourin and Associates Inc. *****
***** Ottawa, Ontario: (613) 836-3884 *****
***** Gatineau, Quebec: (819) 243-6858 *****
***** E-Mail: swmhymo@jfsa.Com *****
*****
+++++++ Licensed user: Stantec Consulting Ltd. (Kitchener) ++++++
+++++++ Kitchener SERIAL#:4730904 ++++++
*****
***** +++++ PROGRAM ARRAY DIMENSIONS +++++ *****
***** Maximum value for ID numbers : 10 *****
***** Max. number of rainfall points: 105408 *****
***** Max. number of flow points : 105408 *****
*****
***** D E T A I L E D   O U T P U T *****
*****
* DATE: 2017-07-10 TIME: 14:18:31 RUN COUNTER: 000629 *
* Input filename: Z:\Temp\Amherst\0595PR5.dat *
* Output filename: Z:\Temp\Amherst\0595PR5.out *
* Summary filename: Z:\Temp\Amherst\0595PR5.sum *
* User comments: *
* 1: _____ *
* 2: _____ *
* 3: _____ *
*****
-----
001:0001-----
-
*# Project Name: [Amherst Island MLA] Project Number: [1609-60595]
*# Date : 07-05-2017
*# Modeller : [NE]
*# Company : Stantec Consulting Ltd. (London)
*# License # : 4730904
*#
*# PROPOSED CONDITIONS
*# 25 mm Water Quality Event
*# 2, 5, 10, 100-year 24-hour SCS Design Storm
*#
*****
-----

```

```

| START | Project dir.: Z:\Temp\Amherst\
-----| Rainfall dir.: Z:\Temp\Amherst\
TZERO = .00 hrs on 0
METOUT= 2 (output = METRIC)
NRUN = 001
NSTORM= 1
# 1=25mm.4hr
-----
001:0002-----
| READ STORM | Filename: 25 mm, 4hr Chicago Storm - Kitchener IDF
| Ptotal= 25.00 mm | Comments: 25 mm, 4hr Chicago Storm - Kitchener IDF
-----
TIME RAIN | TIME RAIN | TIME RAIN | TIME RAIN
hrs mm/hr | hrs mm/hr | hrs mm/hr | hrs mm/hr
.08 1.465 | 1.08 4.024 | 2.08 5.764 | 3.08 2.074
.17 1.540 | 1.17 4.814 | 2.17 4.969 | 3.17 1.977
.25 1.625 | 1.25 6.025 | 2.25 4.374 | 3.25 1.889
.33 1.720 | 1.33 8.114 | 2.33 3.913 | 3.33 1.810
.42 1.829 | 1.42 12.526 | 2.42 3.545 | 3.42 1.737
.50 1.955 | 1.50 27.198 | 2.50 3.245 | 3.50 1.671
.58 2.101 | 1.58 74.855 | 2.58 2.994 | 3.58 1.610
.67 2.274 | 1.67 31.410 | 2.67 2.782 | 3.67 1.553
.75 2.482 | 1.75 16.819 | 2.75 2.601 | 3.75 1.501
.83 2.736 | 1.83 11.357 | 2.83 2.443 | 3.83 1.453
.92 3.055 | 1.92 8.563 | 2.92 2.305 | 3.92 1.408
1.00 3.468 | 2.00 6.882 | 3.00 2.183 | 4.00 1.366
-----
001:0003-----
*# External Drainage Area - Former Invista Site
*#
| DESIGN NASHYD | Area (ha)= 5.02 Curve Number (CN)=97.00
| 01:EXT1 DT= 2.00 | Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
-----| U.H. Tp(hrs)= .190
Unit Hyd Qpeak (cms)= 1.009
PEAK FLOW (cms)= .344 (i)
TIME TO PEAK (hrs)= 1.750
RUNOFF VOLUME (mm)= 17.613
TOTAL RAINFALL (mm)= 25.000
RUNOFF COEFFICIENT = .704
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.
-----
001:0004-----
| DESIGN NASHYD | Area (ha)= 4.89 Curve Number (CN)=97.00
| 02:EXT2 DT= 2.00 | Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
-----| U.H. Tp(hrs)= .190
Unit Hyd Qpeak (cms)= .983
PEAK FLOW (cms)= .335 (i)
TIME TO PEAK (hrs)= 1.750
RUNOFF VOLUME (mm)= 17.613
TOTAL RAINFALL (mm)= 25.000

```

AMHERST ISLAND – MLA

POST-DEVELOPMENT CONDITIONS SWMHYMO OUTPUT

RUNOFF COEFFICIENT = .704

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0005-----

\*# Area of Interest - lawns and parking areas

DESIGN NASHYD	Area (ha)=	3.12	Curve Number (CN)=	84.00
03:201 DT= 2.00	Ia (mm)=	1.500	# of Linear Res.(N)=	3.00
	U.H. Tp(hrs)=	.190		

Unit Hyd Qpeak (cms) = .627

PEAK FLOW (cms) = .083 (i)  
 TIME TO PEAK (hrs) = 1.792  
 RUNOFF VOLUME (mm) = 7.683  
 TOTAL RAINFALL (mm) = 25.000  
 RUNOFF COEFFICIENT = .307

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0006-----

\*# Area of Interest - parking area

DESIGN NASHYD	Area (ha)=	.59	Curve Number (CN)=	97.00
04:202 DT= 2.00	Ia (mm)=	1.500	# of Linear Res.(N)=	3.00
	U.H. Tp(hrs)=	.100		

Unit Hyd Qpeak (cms) = .225

PEAK FLOW (cms) = .058 (i)  
 TIME TO PEAK (hrs) = 1.667  
 RUNOFF VOLUME (mm) = 17.613  
 TOTAL RAINFALL (mm) = 25.000  
 RUNOFF COEFFICIENT = .705

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0007-----

\*# Flow Diverted Around Laydown Area

ADD HYD ( 2000)	ID: NHYD	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	DWF (cms)
ID1 02:EXT2		4.89	.335	1.75	17.61	.000
+ID2 04:202		.59	.058	1.67	17.61	.000
SUM 05:	2000	5.48	.380	1.75	17.61	.000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

001:0008-----

\*# Laydown Area

DESIGN NASHYD	Area (ha)=	1.72	Curve Number (CN)=	89.00
07:203 DT= 2.00	Ia (mm)=	1.500	# of Linear Res.(N)=	3.00
	U.H. Tp(hrs)=	.100		

Unit Hyd Qpeak (cms) = .657

PEAK FLOW (cms) = .087 (i)  
 TIME TO PEAK (hrs) = 1.667  
 RUNOFF VOLUME (mm) = 10.061  
 TOTAL RAINFALL (mm) = 25.000  
 RUNOFF COEFFICIENT = .402

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

001:0009-----

ROUTE RESERVOIR Requested routing time step = 2.0 min.

===== OUTFLOW STORAGE TABLE =====			
OUTFLOW (cms)	STORAGE (ha.m.)	OUTFLOW (cms)	STORAGE (ha.m.)
.000	.0000E+00	.017	.6200E-01
.005	.4000E-02	.018	.7500E-01
.008	.1100E-01	.019	.8800E-01
.010	.2000E-01	.020	.1020E+00
.012	.2900E-01	.303	.1190E+00
.014	.4000E-01	.852	.1390E+00
.015	.5100E-01	.000	.0000E+00

ROUTING RESULTS	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)
INFLOW >07: (203 )	1.72	.087	1.667	10.061
OUTFLOW <04: (002010)	1.72	.008	2.833	10.061

PEAK FLOW REDUCTION [Qout/Qin](%) = 9.250  
 TIME SHIFT OF PEAK FLOW (min) = 70.00  
 MAXIMUM STORAGE USED (ha.m.) = .1129E-01

001:0010-----

\*# Total Flow to Bath Road Culvert

ADD HYD ( 2020)	ID: NHYD	AREA (ha)	QPEAK (cms)	TPEAK (hrs)	R.V. (mm)	DWF (cms)
ID1 01:EXT1		5.02	.344	1.75	17.61	.000
+ID2 03:201		3.12	.083	1.79	7.68	.000
+ID3 04:	2010	1.72	.008	2.83	10.06	.000
+ID4 05:	2000	5.48	.380	1.75	17.61	.000
SUM 06:	2020	15.34	.810	1.75	14.75	.000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.



AMHERST ISLAND – MLA

POST-DEVELOPMENT CONDITIONS SWMHYMO OUTPUT

```
-----
-
001:0011-----
-
** END OF RUN : 1
```

5.00	.866	11.00	3.354	17.00	.974	23.00	.649
5.25	.866	11.25	5.194	17.25	.974	23.25	.649
5.50	.866	11.50	5.194	17.50	.974	23.50	.649
5.75	.866	11.75	22.506	17.75	.974	23.75	.649
6.00	.866	12.00	59.726	18.00	.974	24.00	.649

\*\*\*\*\*

```
-----
| START | Project dir.: Z:\Temp\Amherst\
-----|----- Rainfall dir.: Z:\Temp\Amherst\
TZERO = .00 hrs on 0
METOUT= 2 (output = METRIC)
NRUN = 002
NSTORM= 1
# 1=AI2SCS.24H
```

```
-----
002:0003-----
-
*#*****
*# External Drainage Area - Former Invista Site
*#*****
```

DESIGN NASHYD	Area (ha)=	5.02	Curve Number (CN)=	97.00
01:EXT1 DT= 2.00	Ia (mm)=	1.500	# of Linear Res.(N)=	3.00
	U.H. Tp(hrs)=	.190		

```
Unit Hyd Qpeak (cms)= 1.009

PEAK FLOW (cms)= .575 (i)
TIME TO PEAK (hrs)= 12.072
RUNOFF VOLUME (mm)= 45.765
TOTAL RAINFALL (mm)= 54.100
RUNOFF COEFFICIENT = .846
```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
-----
002:0002-----
-
*#*****
*# Project Name: [Amherst Island MLA] Project Number: [1609-60595]
*# Date : 07-05-2017
*# Modeller : [NE]
*# Company : Stantec Consulting Ltd. (London)
*# License # : 4730904
*#*****
*#
*# PROPOSED CONDITIONS
*# 25 mm Water Quality Event
*# 2, 5, 10, 100-year 24-hour SCS Design Storm
*#
*#*****
*#
```

```
-----
002:0004-----
-
*#*****
*# Area of Interest - lawns and parking areas
*#*****
```

DESIGN NASHYD	Area (ha)=	4.89	Curve Number (CN)=	97.00
02:EXT2 DT= 2.00	Ia (mm)=	1.500	# of Linear Res.(N)=	3.00
	U.H. Tp(hrs)=	.190		

```
Unit Hyd Qpeak (cms)= .983

PEAK FLOW (cms)= .560 (i)
TIME TO PEAK (hrs)= 12.072
RUNOFF VOLUME (mm)= 45.765
TOTAL RAINFALL (mm)= 54.100
RUNOFF COEFFICIENT = .846
```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
-----
002:0002-----
-
*#*****
*# READ STORM | Filename: Amherst Island MTO IDF (44 9' 15"N, 76 4
*# Ptotal= 54.10 mm | Comments: Amherst Island MTO IDF (44 9' 15"N, 76 4
*#*****
```

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.25	.595	6.25	1.082	12.25	7.790	18.25	.974
.50	.595	6.50	1.082	12.50	7.790	18.50	.974
.75	.595	6.75	1.082	12.75	4.003	18.75	.974
1.00	.595	7.00	1.082	13.00	4.003	19.00	.974
1.25	.595	7.25	1.082	13.25	.757	19.25	.974
1.50	.595	7.50	1.082	13.50	.757	19.50	.974
1.75	.595	7.75	1.082	13.75	4.436	19.75	.974
2.00	.595	8.00	1.082	14.00	4.436	20.00	.974
2.25	.703	8.25	1.461	14.25	1.623	20.25	.649
2.50	.703	8.50	1.461	14.50	1.623	20.50	.649
2.75	.703	8.75	1.461	14.75	1.623	20.75	.649
3.00	.703	9.00	1.461	15.00	1.623	21.00	.649
3.25	.703	9.25	1.731	15.25	1.623	21.25	.649
3.50	.703	9.50	1.731	15.50	1.623	21.50	.649
3.75	.703	9.75	1.948	15.75	1.623	21.75	.649
4.00	.703	10.00	1.948	16.00	1.623	22.00	.649
4.25	.866	10.25	2.489	16.25	.974	22.25	.649
4.50	.866	10.50	2.489	16.50	.974	22.50	.649
4.75	.866	10.75	3.354	16.75	.974	22.75	.649

```
-----
002:0005-----
-
*#*****
*# Area of Interest - lawns and parking areas
*#*****
```

DESIGN NASHYD	Area (ha)=	3.12	Curve Number (CN)=	84.00
03:201 DT= 2.00	Ia (mm)=	1.500	# of Linear Res.(N)=	3.00
	U.H. Tp(hrs)=	.190		

```
Unit Hyd Qpeak (cms)= .627

PEAK FLOW (cms)= .216 (i)
TIME TO PEAK (hrs)= 12.072
RUNOFF VOLUME (mm)= 27.399
TOTAL RAINFALL (mm)= 54.100
RUNOFF COEFFICIENT = .506
```

AMHERST ISLAND – MLA

POST-DEVELOPMENT CONDITIONS SWMHYMO OUTPUT

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
-----
002:0006-----
*#*****
*# Area of Interest - parking area
*#*****
| DESIGN NASHYD | Area (ha)= .59 Curve Number (CN)=97.00
| 04:202 DT= 2.00 | Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
-----
U.H. Tp(hrs)= .100
```

```
Unit Hyd Qpeak (cms)= .225
PEAK FLOW (cms)= .087 (i)
TIME TO PEAK (hrs)= 12.001
RUNOFF VOLUME (mm)= 45.765
TOTAL RAINFALL (mm)= 54.100
RUNOFF COEFFICIENT = .846
```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
-----
002:0007-----
*#*****
*# Flow Diverted Around Laydown Area
*#*****
| ADD HYD ( 2000) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
-----
ID1 02:EXT2 4.89 .560 12.07 45.76 .000
+ID2 04:202 .59 .087 12.00 45.76 .000
=====
SUM 05: 2000 5.48 .636 12.04 45.76 .000
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```
-----
002:0008-----
*#*****
*# Laydown Area
*#*****
| DESIGN NASHYD | Area (ha)= 1.72 Curve Number (CN)=89.00
| 07:203 DT= 2.00 | Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
-----
U.H. Tp(hrs)= .100
```

```
Unit Hyd Qpeak (cms)= .657
PEAK FLOW (cms)= .190 (i)
TIME TO PEAK (hrs)= 12.001
RUNOFF VOLUME (mm)= 32.940
TOTAL RAINFALL (mm)= 54.100
RUNOFF COEFFICIENT = .609
```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
-----
002:0009-----
```

```
-----
| ROUTE RESERVOIR | Requested routing time step = 2.0 min.
| IN>07:(203 ) |
| OUT<04:(002010) |
-----
===== OUTFLOW STORAGE TABLE =====
OUTFLOW STORAGE OUTFLOW STORAGE
(cms) (ha.m.) (cms) (ha.m.)
.000 .0000E+00 .017 .6200E-01
.005 .4000E-02 .018 .7500E-01
.008 .1100E-01 .019 .8800E-01
.010 .2000E-01 .020 .1020E+00
.012 .2900E-01 .303 .1190E+00
.014 .4000E-01 .852 .1390E+00
.015 .5100E-01 .000 .0000E+00
```

```
ROUTING RESULTS AREA QPEAK TPEAK R.V.
(ha) (cms) (hrs) (mm)
INFLOW >07: (203 ) 1.72 .190 12.001 32.940
OUTFLOW<04: (002010) 1.72 .012 13.072 32.940
```

```
PEAK FLOW REDUCTION [Qout/Qin](%)= 6.403
TIME SHIFT OF PEAK FLOW (min)= 64.29
MAXIMUM STORAGE USED (ha.m.)=.2995E-01
```

```
-----
002:0010-----
*#*****
*# Total Flow to Bath Road Culvert
*#*****
| ADD HYD ( 2020) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
-----
ID1 01:EXT1 5.02 .575 12.07 45.76 .000
+ID2 03:201 3.12 .216 12.07 27.40 .000
+ID3 04: 2010 1.72 .012 13.07 32.94 .000
+ID4 05: 2000 5.48 .636 12.04 45.76 .000
=====
SUM 06: 2020 15.34 1.431 12.07 40.59 .000
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```
-----
002:0011-----
-----
002:0002-----
** END OF RUN : 4
*****
```

```
-----
| START | Project dir.: Z:\Temp\Amherst\
| | Rainfall dir.: Z:\Temp\Amherst\
-----
TZERO = .00 hrs on 0
METOUT= 2 (output = METRIC)
NRUN = 005
NSTORM= 1
# 1=AI5SCS.24H
```

AMHERST ISLAND – MLA

POST-DEVELOPMENT CONDITIONS SWMHYMO OUTPUT

```

-----
005:0002-----
-
*#*****
*# Project Name: [Amherst Island MLA] Project Number: [1609-60595]
*# Date       : 07-05-2017
*# Modeller   : [NE]
*# Company    : Stantec Consulting Ltd. (London)
*# License #  : 4730904
*#*****
*#
*# PROPOSED CONDITIONS
*# 25 mm Water Quality Event
*# 2, 5, 10, 100-year 24-hour SCS Design Storm
*#
*#*****
*#

```

```

-----
005:0002-----
-
| READ STORM |          Filename: Amherst Island MTO IDF (44 9' 15"N, 76 4
| Ptotal= 71.40 mm |          Comments: Amherst Island MTO IDF (44 9' 15"N, 76 4

```

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.25	.785	6.25	1.428	12.25	10.282	18.25	1.285
.50	.785	6.50	1.428	12.50	10.282	18.50	1.285
.75	.785	6.75	1.428	12.75	5.284	18.75	1.285
1.00	.785	7.00	1.428	13.00	5.284	19.00	1.285
1.25	.785	7.25	1.428	13.25	3.713	19.25	1.285
1.50	.785	7.50	1.428	13.50	3.998	19.50	1.285
1.75	.785	7.75	1.428	13.75	2.999	19.75	1.285
2.00	.785	8.00	1.428	14.00	2.999	20.00	1.285
2.25	.928	8.25	1.928	14.25	2.142	20.25	.857
2.50	.928	8.50	1.928	14.50	2.142	20.50	.857
2.75	.928	8.75	1.928	14.75	2.142	20.75	.857
3.00	.928	9.00	1.928	15.00	2.142	21.00	.857
3.25	.928	9.25	2.285	15.25	2.142	21.25	.857
3.50	.928	9.50	2.285	15.50	2.142	21.50	.857
3.75	.928	9.75	2.570	15.75	2.142	21.75	.857
4.00	.928	10.00	2.570	16.00	2.142	22.00	.857
4.25	1.142	10.25	3.284	16.25	1.285	22.25	.857
4.50	1.142	10.50	3.284	16.50	1.285	22.50	.857
4.75	1.142	10.75	4.427	16.75	1.285	22.75	.857
5.00	1.142	11.00	4.427	17.00	1.285	23.00	.857
5.25	1.142	11.25	6.854	17.25	1.285	23.25	.857
5.50	1.142	11.50	6.854	17.50	1.285	23.50	.857
5.75	1.142	11.75	29.702	17.75	1.285	23.75	.857
6.00	1.142	12.00	78.826	18.00	1.285	24.00	.857

```

-----
005:0003-----
-
*#*****
*# External Drainage Area - Former Invista Site
*#*****
*#
| DESIGN NASHYD | Area (ha)= 5.02 Curve Number (CN)=97.00
| 01:EXT1 DT= 2.00 | Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
-----
U.H. Tp(hrs)= .190

```

Unit Hyd Qpeak (cms)= 1.009

```

PEAK FLOW (cms)= .777 (i)
TIME TO PEAK (hrs)= 12.072
RUNOFF VOLUME (mm)= 62.836
TOTAL RAINFALL (mm)= 71.398
RUNOFF COEFFICIENT = .880

```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
005:0004-----
-
| DESIGN NASHYD | Area (ha)= 4.89 Curve Number (CN)=97.00
| 02:EXT2 DT= 2.00 | Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
-----
U.H. Tp(hrs)= .190

```

Unit Hyd Qpeak (cms)= .983

```

PEAK FLOW (cms)= .756 (i)
TIME TO PEAK (hrs)= 12.072
RUNOFF VOLUME (mm)= 62.836
TOTAL RAINFALL (mm)= 71.398
RUNOFF COEFFICIENT = .880

```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
005:0005-----
-
*#*****
*# Area of Interest - lawns and parking areas
*#*****
| DESIGN NASHYD | Area (ha)= 3.12 Curve Number (CN)=84.00
| 03:201 DT= 2.00 | Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
-----
U.H. Tp(hrs)= .190

```

Unit Hyd Qpeak (cms)= .627

```

PEAK FLOW (cms)= .327 (i)
TIME TO PEAK (hrs)= 12.072
RUNOFF VOLUME (mm)= 41.307
TOTAL RAINFALL (mm)= 71.398
RUNOFF COEFFICIENT = .579

```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

-----
005:0006-----
-
*#*****
*# Area of Interest - parking area
*#*****
| DESIGN NASHYD | Area (ha)= .59 Curve Number (CN)=97.00
| 04:202 DT= 2.00 | Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
-----
U.H. Tp(hrs)= .100

```

Unit Hyd Qpeak (cms)= .225

```

PEAK FLOW (cms)= .117 (i)
TIME TO PEAK (hrs)= 12.001
RUNOFF VOLUME (mm)= 62.836
TOTAL RAINFALL (mm)= 71.398

```

AMHERST ISLAND – MLA

POST-DEVELOPMENT CONDITIONS SWMHYMO OUTPUT

RUNOFF COEFFICIENT = .880

TIME SHIFT OF PEAK FLOW (min)= 96.43  
 MAXIMUM STORAGE USED (ha.m.)=.4625E-01

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
-----
005:0007-----
*#*****
*# Flow Diverted Around Laydown Area
*#*****
| ADD HYD ( 2000) | ID: NHYD      AREA   QPEAK  TPEAK  R.V.   DWF
|-----|-----|-----|-----|-----|-----|
|              | ID1 02:EXT2 | 4.89   .756   12.07  62.84  .000
|              | +ID2 04:202 | .59    .117   12.00  62.84  .000
|              |-----|-----|-----|-----|
|              | SUM 05:     | 2000   5.48   .859   12.04  62.84  .000
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```
-----
005:0008-----
*#*****
*# Laydown Area
*#*****
| DESIGN NASHYD | Area (ha)= 1.72 Curve Number (CN)=89.00
| 07:203 DT= 2.00 | Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
|-----|-----|-----|-----|
|              | U.H. Tp(hrs)= .100

Unit Hyd Qpeak (cms)= .657

PEAK FLOW (cms)= .277 (i)
TIME TO PEAK (hrs)= 12.001
RUNOFF VOLUME (mm)= 48.234
TOTAL RAINFALL (mm)= 71.398
RUNOFF COEFFICIENT = .676
```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```
-----
005:0009-----
| ROUTE RESERVOIR | Requested routing time step = 2.0 min.
| IN>07:(203 ) |
| OUT<04:(002010) |
|-----|-----|
|=====  

| OUTFLOW STORAGE | OUTFLOW STORAGE |
| (cms) (ha.m.) | (cms) (ha.m.) |
|-----|-----|
| .000 .0000E+00 | .017 .6200E-01 |
| .005 .4000E-02 | .018 .7500E-01 |
| .008 .1100E-01 | .019 .8800E-01 |
| .010 .2000E-01 | .020 .1020E+00 |
| .012 .2900E-01 | .303 .1190E+00 |
| .014 .4000E-01 | .852 .1390E+00 |
| .015 .5100E-01 | .000 .0000E+00 |
|-----|-----|

ROUTING RESULTS      AREA   QPEAK  TPEAK  R.V.
-----|-----|-----|-----|
INFLOW >07: (203 )  1.72   .277   12.001  48.234
OUTFLOW<04: (002010) 1.72   .015   13.608  48.234

PEAK FLOW REDUCTION [Qout/Qin](%)= 5.268
```

```
-----
005:0010-----
*#*****
*# Total Flow to Bath Road Culvert
*#*****
| ADD HYD ( 2020) | ID: NHYD      AREA   QPEAK  TPEAK  R.V.   DWF
|-----|-----|-----|-----|-----|-----|
|              | ID1 01:EXT1 | 5.02   .777   12.07  62.84  .000
|              | +ID2 03:201 | 3.12   .327   12.07  41.31  .000
|              | +ID3 04:     | 1.72   .015   13.61  48.23  .000
|              | +ID4 05:     | 2000   5.48   .859   12.04  62.84  .000
|              |-----|-----|-----|-----|
|              | SUM 06:     | 2020   15.34  1.966   12.07  56.82  .000
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

```
-----
005:0011-----
-----
005:0002-----
-----
005:0002-----
** END OF RUN : 9
```

```
-----
| START | Project dir.: Z:\Temp\Amherst\
|-----| Rainfall dir.: Z:\Temp\Amherst\
TZERO = .00 hrs on 0
METOUT= 2 (output = METRIC)
NRUN = 010
NSTORM= 1
# 1=AI10SCS.24H
-----
010:0002-----
*#*****
*# Project Name: [Amherst Island MLA] Project Number: [1609-60595]
*# Date : 07-05-2017
*# Modeller : [NE]
*# Company : Stantec Consulting Ltd. (London)
*# License # : 4730904
*#*****
*# PROPOSED CONDITIONS
*# 25 mm Water Quality Event
*# 2, 5, 10, 100-year 24-hour SCS Design Storm
*#*****
```

AMHERST ISLAND – MLA

POST-DEVELOPMENT CONDITIONS SWMHYMO OUTPUT

```

*#
-----
010:0002-----
-----
| READ STORM |      Filename: Amherst Island MTO IDF (44 9' 15"N, 76 4
| Ptotal= 83.00 mm |      Comments: Amherst Island MTO IDF (44 9' 15"N, 76 4
-----
      TIME    RAIN    TIME    RAIN    TIME    RAIN    TIME    RAIN
      hrs    mm/hr   hrs    mm/hr   hrs    mm/hr   hrs    mm/hr
.25    .913    6.25  1.660  12.25  11.952  18.25  1.494
.50    .913    6.50  1.660  12.50  11.952  18.50  1.494
.75    .913    6.75  1.660  12.75  6.142   18.75  1.494
1.00   .913    7.00  1.660  13.00  6.142   19.00  1.494
1.25   .913    7.25  1.660  13.25  1.162   19.25  1.494
1.50   .913    7.50  1.660  13.50  1.162   19.50  1.494
1.75   .913    7.75  1.660  13.75  6.806   19.75  1.494
2.00   .913    8.00  1.660  14.00  6.806   20.00  1.494
2.25  1.079    8.25  2.241  14.25  2.490   20.25  .996
2.50  1.079    8.50  2.241  14.50  2.490   20.50  .996
2.75  1.079    8.75  2.241  14.75  2.490   20.75  .996
3.00  1.079    9.00  2.241  15.00  2.490   21.00  .996
3.25  1.079    9.25  2.656  15.25  2.490   21.25  .996
3.50  1.079    9.50  2.656  15.50  2.490   21.50  .996
3.75  1.079    9.75  2.988  15.75  2.490   21.75  .996
4.00  1.079   10.00  2.988  16.00  2.490   22.00  .996
4.25  1.328   10.25  3.818  16.25  1.494   22.25  .996
4.50  1.328   10.50  3.818  16.50  1.494   22.50  .996
4.75  1.328   10.75  5.146  16.75  1.494   22.75  .996
5.00  1.328   11.00  5.146  17.00  1.494   23.00  .996
5.25  1.328   11.25  7.968  17.25  1.494   23.25  .996
5.50  1.328   11.50  7.968  17.50  1.494   23.50  .996
5.75  1.328   11.75 34.528  17.75  1.494   23.75  .996
6.00  1.328   12.00 91.632  18.00  1.494   24.00  .996

```

```

-----
010:0003-----
-----
*# External Drainage Area - Former Invista Site
*#
-----
| DESIGN NASHYD | Area (ha)= 5.02 Curve Number (CN)=97.00
| 01:EXT1 DT= 2.00 | Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
| U.H. Tp(hrs)= .190
-----
Unit Hyd Qpeak (cms)= 1.009
PEAK FLOW (cms)= .911 (i)
TIME TO PEAK (hrs)= 12.072
RUNOFF VOLUME (mm)= 74.335
TOTAL RAINFALL (mm)= 83.000
RUNOFF COEFFICIENT = .896
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

```

-----
010:0004-----
-----
| DESIGN NASHYD | Area (ha)= 4.89 Curve Number (CN)=97.00
| 02:EXT2 DT= 2.00 | Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
| U.H. Tp(hrs)= .190

```

```

Unit Hyd Qpeak (cms)= .983
PEAK FLOW (cms)= .887 (i)
TIME TO PEAK (hrs)= 12.072
RUNOFF VOLUME (mm)= 74.335
TOTAL RAINFALL (mm)= 83.000
RUNOFF COEFFICIENT = .896
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

```

-----
010:0005-----
-----
*# Area of Interest - lawns and parking areas
*#
-----
| DESIGN NASHYD | Area (ha)= 3.12 Curve Number (CN)=84.00
| 03:201 DT= 2.00 | Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
| U.H. Tp(hrs)= .190
-----
Unit Hyd Qpeak (cms)= .627
PEAK FLOW (cms)= .405 (i)
TIME TO PEAK (hrs)= 12.072
RUNOFF VOLUME (mm)= 51.141
TOTAL RAINFALL (mm)= 83.000
RUNOFF COEFFICIENT = .616
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

```

-----
010:0006-----
-----
*# Area of Interest - parking area
*#
-----
| DESIGN NASHYD | Area (ha)= .59 Curve Number (CN)=97.00
| 04:202 DT= 2.00 | Ia (mm)= 1.500 # of Linear Res.(N)= 3.00
| U.H. Tp(hrs)= .100
-----
Unit Hyd Qpeak (cms)= .225
PEAK FLOW (cms)= .137 (i)
TIME TO PEAK (hrs)= 12.001
RUNOFF VOLUME (mm)= 74.335
TOTAL RAINFALL (mm)= 83.000
RUNOFF COEFFICIENT = .896
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

```

```

-----
010:0007-----
-----
*# Flow Diverted Around Laydown Area
*#
-----
| ADD HYD ( 2000) | ID: NHYD AREA QPEAK TPEAK R.V. DWF
| (ha) (cms) (hrs) (mm) (cms)
ID1 02:EXT2 4.89 .887 12.07 74.34 .000
+ID2 04:202 .59 .137 12.00 74.34 .000
=====

```

AMHERST ISLAND – MLA

POST-DEVELOPMENT CONDITIONS SWMHYMO OUTPUT

SUM 05: 2000 5.48 1.007 12.04 74.34 .000

=====

SUM 06: 2020 15.34 2.327 12.07 67.88 .000

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----

010:0008-----

-----

\*#\*\*\*\*\*

\*# Laydown Area

\*#\*\*\*\*\*

DESIGN NASHYD	Area (ha)=	1.72	Curve Number (CN)=	89.00
07:203 DT= 2.00	Ia (mm)=	1.500	# of Linear Res.(N)=	3.00
	U.H. Tp(hrs)=	.100		

Unit Hyd Qpeak (cms)= .657

PEAK FLOW (cms)= .336 (i)

TIME TO PEAK (hrs)= 12.001

RUNOFF VOLUME (mm)= 58.837

TOTAL RAINFALL (mm)= 83.000

RUNOFF COEFFICIENT = .709

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----

010:0009-----

ROUTE RESERVOIR	Requested routing time step = 2.0 min.
IN>07:(203 )	
OUT<04:(002010)	

=====		OUTFLOW STORAGE TABLE		=====	
OUTFLOW	STORAGE	OUTFLOW	STORAGE		
(cms)	(ha.m.)	(cms)	(ha.m.)		
.000	.0000E+00	.017	.6200E-01		
.005	.4000E-02	.018	.7500E-01		
.008	.1100E-01	.019	.8800E-01		
.010	.2000E-01	.020	.1020E+00		
.012	.2900E-01	.303	.1190E+00		
.014	.4000E-01	.852	.1390E+00		
.015	.5100E-01	.000	.0000E+00		

ROUTING RESULTS	AREA	QPEAK	TPEAK	R.V.
	(ha)	(cms)	(hrs)	(mm)
INFLOW >07: (203 )	1.72	.336	12.001	58.837
OUTFLOW<04: (002010)	1.72	.016	14.180	58.837

PEAK FLOW REDUCTION [Qout/Qin](%)= 4.827

TIME SHIFT OF PEAK FLOW (min)= 130.71

MAXIMUM STORAGE USED (ha.m.)=.5760E-01

-----

010:0010-----

\*#\*\*\*\*\*

\*# Total Flow to Bath Road Culvert

\*#\*\*\*\*\*

ADD HYD ( 2020)	ID: NHYD	AREA	QPEAK	TPEAK	R.V.	DWF
		(ha)	(cms)	(hrs)	(mm)	(cms)
ID1 01:EXT1		5.02	.911	12.07	74.34	.000
+ID2 03:201		3.12	.405	12.07	51.14	.000
+ID3 04:	2010	1.72	.016	14.18	58.84	.000
+ID4 05:	2000	5.48	1.007	12.04	74.34	.000

-----

010:0011-----

-----

010:0002-----

-----

010:0002-----

-----

010:0002-----

\*\* END OF RUN : 99

\*\*\*\*\*

START	Project dir.: Z:\Temp\Amherst\
	Rainfall dir.: Z:\Temp\Amherst\
TZERO =	.00 hrs on 0
METOUT=	2 (output = METRIC)
NRUN =	100
NSTORM=	1
	# 1=AI100SCS.24H

-----

100:0002-----

\*#\*\*\*\*\*

\*# Project Name: [Amherst Island MLA] Project Number: [1609-60595]

\*# Date : 07-05-2017

\*# Modeller : [NE]

\*# Company : Stantec Consulting Ltd. (London)

\*# License # : 4730904

\*#\*\*\*\*\*

\*#

\*# PROPOSED CONDITIONS

\*# 25 mm Water Quality Event

\*# 2, 5, 10, 100-year 24-hour SCS Design Storm

\*#

\*#\*\*\*\*\*

\*#

-----

100:0002-----

READ STORM	Filename: Amherst Island MTO IDF (44 9' 15"N, 76 4
Ptotal= 119.80 mm	Comments: Amherst Island MTO IDF (44 9' 15"N, 76 4

TIME	RAIN	TIME	RAIN	TIME	RAIN	TIME	RAIN
hrs	mm/hr	hrs	mm/hr	hrs	mm/hr	hrs	mm/hr
.25	1.318	6.25	2.396	12.25	17.251	18.25	2.156
.50	1.318	6.50	2.396	12.50	17.251	18.50	2.156

AMHERST ISLAND – MLA

POST-DEVELOPMENT CONDITIONS SWMHYMO OUTPUT

.75	1.318	6.75	2.396	12.75	8.865	18.75	2.156
1.00	1.318	7.00	2.396	13.00	8.865	19.00	2.156
1.25	1.318	7.25	2.396	13.25	1.677	19.25	2.156
1.50	1.318	7.50	2.396	13.50	1.677	19.50	2.156
1.75	1.318	7.75	2.396	13.75	9.824	19.75	2.156
2.00	1.318	8.00	2.396	14.00	9.824	20.00	2.156
2.25	1.557	8.25	3.235	14.25	3.594	20.25	1.438
2.50	1.557	8.50	3.235	14.50	3.594	20.50	1.438
2.75	1.557	8.75	3.235	14.75	3.594	20.75	1.438
3.00	1.557	9.00	3.235	15.00	3.594	21.00	1.438
3.25	1.557	9.25	3.834	15.25	3.594	21.25	1.438
3.50	1.557	9.50	3.834	15.50	3.594	21.50	1.438
3.75	1.557	9.75	4.313	15.75	3.594	21.75	1.438
4.00	1.557	10.00	4.313	16.00	3.594	22.00	1.438
4.25	1.917	10.25	5.511	16.25	2.156	22.25	1.438
4.50	1.917	10.50	5.511	16.50	2.156	22.50	1.438
4.75	1.917	10.75	7.428	16.75	2.156	22.75	1.438
5.00	1.917	11.00	7.428	17.00	2.156	23.00	1.438
5.25	1.917	11.25	11.501	17.25	2.156	23.25	1.438
5.50	1.917	11.50	11.501	17.50	2.156	23.50	1.438
5.75	1.917	11.75	49.837	17.75	2.156	23.75	1.438
6.00	1.917	12.00	132.259	18.00	2.156	24.00	1.438

-----  
100:0003-----  
-----  
\*#\*\*\*\*\*  
\*# External Drainage Area - Former Invista Site  
\*#\*\*\*\*\*  
-----  
| DESIGN NASHYD | Area (ha)= 5.02 Curve Number (CN)=97.00  
| 01:EXT1 DT= 2.00 | Ia (mm)= 1.500 # of Linear Res.(N)= 3.00  
-----  
U.H. Tp(hrs)= .190
Unit Hyd Qpeak (cms)= 1.009  
  
PEAK FLOW (cms)= 1.333 (i)  
TIME TO PEAK (hrs)= 12.072  
RUNOFF VOLUME (mm)= 110.935  
TOTAL RAINFALL (mm)= 119.801  
RUNOFF COEFFICIENT = .926  
  
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
100:0004-----  
-----  
| DESIGN NASHYD | Area (ha)= 4.89 Curve Number (CN)=97.00  
| 02:EXT2 DT= 2.00 | Ia (mm)= 1.500 # of Linear Res.(N)= 3.00  
-----  
U.H. Tp(hrs)= .190
Unit Hyd Qpeak (cms)= .983  
  
PEAK FLOW (cms)= 1.299 (i)  
TIME TO PEAK (hrs)= 12.072  
RUNOFF VOLUME (mm)= 110.935  
TOTAL RAINFALL (mm)= 119.801  
RUNOFF COEFFICIENT = .926  
  
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
100:0005-----  
-----  
\*#\*\*\*\*\*  
\*# Area of Interest - lawns and parking areas  
\*#\*\*\*\*\*  
-----  
| DESIGN NASHYD | Area (ha)= 3.12 Curve Number (CN)=84.00  
| 03:201 DT= 2.00 | Ia (mm)= 1.500 # of Linear Res.(N)= 3.00  
-----  
U.H. Tp(hrs)= .190
Unit Hyd Qpeak (cms)= .627  
  
PEAK FLOW (cms)= .664 (i)  
TIME TO PEAK (hrs)= 12.072  
RUNOFF VOLUME (mm)= 83.963  
TOTAL RAINFALL (mm)= 119.801  
RUNOFF COEFFICIENT = .701  
  
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
100:0006-----  
-----  
\*#\*\*\*\*\*  
\*# Area of Interest - parking area  
\*#\*\*\*\*\*  
-----  
| DESIGN NASHYD | Area (ha)= .59 Curve Number (CN)=97.00  
| 04:202 DT= 2.00 | Ia (mm)= 1.500 # of Linear Res.(N)= 3.00  
-----  
U.H. Tp(hrs)= .100
Unit Hyd Qpeak (cms)= .225  
  
PEAK FLOW (cms)= .201 (i)  
TIME TO PEAK (hrs)= 12.001  
RUNOFF VOLUME (mm)= 110.935  
TOTAL RAINFALL (mm)= 119.801  
RUNOFF COEFFICIENT = .926  
  
(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
100:0007-----  
-----  
\*#\*\*\*\*\*  
\*# Flow Diverted Around Laydown Area  
\*#\*\*\*\*\*  
-----  
| ADD HYD ( 2000) | ID: NHYD AREA QPEAK TPEAK R.V. DWF  
-----  
| (ha) (cms) (hrs) (mm) (cms)  
ID1 02:EXT2 4.89 1.299 12.07 110.93 .000  
+ID2 04:202 .59 .201 12.00 110.93 .000  
-----  
SUM 05: 2000 5.48 1.475 12.04 110.93 .000  
  
NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----  
100:0008-----  
-----  
\*#\*\*\*\*\*  
\*# Laydown Area  
\*#\*\*\*\*\*  
-----

```

DESIGN NASHYD      | Area   (ha)=   1.72   Curve Number   (CN)=89.00
07:203   DT= 2.00 | Ia     (mm)=   1.500   # of Linear Res.(N)= 3.00
                | U.H. Tp(hrs)=   .100
    
```

```

Unit Hyd Qpeak   (cms)=   .657

PEAK FLOW        (cms)=   .525 (i)
TIME TO PEAK     (hrs)=   12.001
RUNOFF VOLUME    (mm)=   93.492
TOTAL RAINFALL   (mm)=  119.801
RUNOFF COEFFICIENT =   .780
    
```

(i) PEAK FLOW DOES NOT INCLUDE BASEFLOW IF ANY.

-----  
100:0009-----  
-

```

ROUTE RESERVOIR   | Requested routing time step = 2.0 min.
IN>07:(203 )      |
OUT<04:(002010)  |
-----
===== OUTFLOW STORAGE TABLE =====
OUTFLOW STORAGE | OUTFLOW STORAGE
(cms) (ha.m.)   | (cms) (ha.m.)
.000 .0000E+00 | .017 .6200E-01
.005 .4000E-02 | .018 .7500E-01
.008 .1100E-01 | .019 .8800E-01
.010 .2000E-01 | .020 .1020E+00
.012 .2900E-01 | .303 .1190E+00
.014 .4000E-01 | .852 .1390E+00
.015 .5100E-01 | .000 .0000E+00
    
```

```

ROUTING RESULTS      AREA   QPEAK   TPEAK   R.V.
-----
INFLOW >07: (203 )  (ha)   (cms)   (hrs)   (mm)
OUTFLOW<04: (002010) 1.72   .525   12.001  93.492
    
```

```

PEAK FLOW REDUCTION [Qout/Qin](%)= 3.755
TIME SHIFT OF PEAK FLOW (min)= 132.86
MAXIMUM STORAGE USED (ha.m.)=.9786E-01
    
```

-----  
100:0010-----  
-

```

*#####
*# Total Flow to Bath Road Culvert
*#####
    
```

```

ADD HYD ( 2020) | ID: NHYD   AREA   QPEAK   TPEAK   R.V.   DWF
                | (ha)   (cms)   (hrs)   (mm)   (cms)
+ID1 01:EXT1     |      5.02  1.333  12.07  110.93  .000
+ID2 03:201      |      3.12  .664   12.07  83.96   .000
+ID3 04: 2010    |      1.72  .020   14.22  93.49   .000
+ID4 05: 2000    |      5.48  1.475  12.04  110.93  .000
=====
SUM 06: 2020     |     15.34  3.473  12.07  103.49  .000
    
```

NOTE: PEAK FLOWS DO NOT INCLUDE BASEFLOWS IF ANY.

-----  
100:0011-----  
-

100:0002-----  
-  
-----

100:0002-----  
-  
-----

100:0002-----  
-  
-----

100:0002-----  
-  
FINISH  
-----

-----  
\*\*\*\*\*  
\*  
\*\*\*\*\*

WARNINGS / ERRORS / NOTES

Simulation ended on 2017-07-10 at 14:18:34

-----  
=



APPENDIX C  
DESIGN CALCULATIONS

Subject: SWMHYMO Parameters  
 Project: Amherst Island Wind Energy Project - Mainland Laydown Area  
 Project No.: 1609-60595  
 Client: Windlectric  
 Date: July 10, 2017

**Pre-development Conditions**

Area Description	Catchment Number	SWMHYMO Command	Area (ha)	CN	TIMP	XIMP	Slope (%)	Length (m)	Tc (hrs)	Tp (hrs)
External Drainage Area - Former Invista Site	EXT1	DESIGN NASHYD	9.90	97	-	-	0.4	330	0.30	0.18
Parking Lot, Driveways, Lawn	101	DESIGN NASHYD	5.43	82	-	-	2.9	190	0.37	0.22
<b>Total</b>			15.33							

**Pre-development Conditions**

Area Description	Catchment Number	SWMHYMO Command	Area (ha)	CN	TIMP	XIMP	Slope (%)	Length (m)	Tc (hrs)	Tp (hrs)
External Drainage Area - Former Invista Site	EXT1	DESIGN NASHYD	5.02	97	-	-	0.4	330	0.32	0.19
External Drainage Area - Former Invista Site	EXT2	DESIGN NASHYD	4.89	97	-	-	0.4	330	0.32	0.19
Parking Lot, Driveways, Lawn	201	DESIGN NASHYD	3.12	84	-	-	2.9	140	0.32	0.19
Parking Lot	202	DESIGN NASHYD	0.59	97	-	-	2.9	30	0.02	0.01
Gravel Laydown Area	203	DESIGN NASHYD	1.72	89	-	-	2.9	80	0.06	0.03
<b>Total</b>			15.34							

**Notes:**

TIMP ..... Total percent impervious

XIMP ..... Percent impervious directly connected

Time of Concentration calculated using the Airport Method .....  $T_c = [ 3.26 (1.1-C) L^{0.5} ] / S^{0.33}$   
 Where: C = Runoff Coefficient = 0.4 for undeveloped areas  
 L = Length of Overland Flow (m)  
 S = Slope (%)

Time of Concentration calculated using the Bransby-Williams Method .....  $T_c = 0.057 L / [S_w^{0.2} \times A^{0.1}]$   
 Where: L = Length of Overland Flow (m)  
 S<sub>w</sub> = Watershed Slope (%)  
 A = Watershed Area (ha)

Time to Peak .....  $T_p = 0.6T_c$

Minimum T<sub>p</sub> = 0.1 hours used for all hydrologic calculations.

## Amherst Island Wind Energy Project - Mainland Staging Area - 1609-60595

### Stormwater Quality Volumetric Requirements

Facility	Drainage Area (ha) <sup>2</sup>	Total % Imp.	Level	Water Quality Unit Volume Requirements <sup>1</sup>	
				Total Unit Volume (m <sup>3</sup> /ha)	Total MOE Volume (m <sup>3</sup> /ha)
Dry Pond	1.72	100	Basic	280	482

<sup>1</sup> Water quality unit volume requirements based on Table 3.2, Stormwater Management Planning & Design Manual (MOE 2003), Protection Level "Basic"

<sup>2</sup> Drainage Area for Quality control represents total storm drainage area to SWM Facility and includes the area of the SWM facility itself

Amherst Island Wind Energy Project - Mainland Staging Area - 1609-60595  
 Stormwater Management Facility Design Calculations

Rating Curve			Estimated Detention Time (hrs)	Volume Estimation			Elevation (m)	Outlet Structure Controls					
Elevation (m)	Discharge (m³/s)	Active Storage (m³)		Elevation (m)	Volume (m³)	Depth (m)		Quality Outlet # 1 (m³/s)	Quantity Outlet #2 (m³/s)	Overflow Weir (m³/s)	Parameters		
78.05				78.05			78.05				Quality Outlet		
78.15	0.005	36	4.3	78.15	36	0.1	78.15	0.005			Outlet #1 Elev (m)	Orifice Coeff.	
78.25	0.008	110	9.1	78.25	110	0.2	78.25	0.008			78.05	0.60	
78.35	0.010	196	15.0	78.35	196	0.3	78.35	0.010			Outlet #1-Midpoint (mm)	Perimeter (m)	
78.45	0.012	293	22.1	78.45	293	0.4	78.45	0.012			78.10	0.31	
78.55	0.014	397	30.5	78.55	397	0.5	78.55	0.014			Outlet Diameter (mm)	Area (m²)	
78.65	0.015	507	40.1	78.65	507	0.6	78.65	0.015			100	0.008	
78.75	0.017	623	50.8	78.75	623	0.7	78.75	0.017			Weir Coeff. (semi-circular)	Orientation	
78.85	0.018	746	62.6	78.85	746	0.8	78.85	0.018			1.62	Vertical	
78.95	0.019	876	75.7	78.95	876	0.9	78.95	0.019			Quantity Outlet		
79.05	0.020	1,023	90.0	79.05	1,023	1.0	79.05	0.020			Outlet #2 Elev (m)	Orifice Coeff.	
79.15	0.303	1,194	92.1	79.15	1,194	1.1	79.15	0.021			Outlet #2-Midpoint (mm)	Perimeter (m)	
79.25	0.852	1,390	92.8	79.25	1,390	1.2	79.25	0.022			Outlet Diameter (mm)	Area (m²)	
										0.281		Weir Coeff. (semi-circular)	Orientation
										0.830		1.62	Vertical
Overflow Weir													
						Spillway Invert (m)	Top of Berm (m)						
						79.05	79.35						
						Spillway Length @ Invert (m)	Max. Flow Depth (m)						
						5	0.30						
						Left Side Slope	Right Side Slope						
						3	3						
						Weir Coefficient (Rectangle)	Topwidth						
						1.7	6.8						
						Weir Coefficient (Triangle)							
						1.3							

Drawdown Time Calculations Greater than 0.1 m above the permanent pool

$$T = [v_2 - v_1] / [(Q_2 + Q_1) / 2] / 3600$$

where

T = drawdown time in hours

v<sub>2</sub> = starting pond volume

v<sub>1</sub> = ending pond volume

Q<sub>2</sub> = starting flow

Q<sub>1</sub> = ending flow

From 0.0 to 0.1 m above the permanent pool

$$T = [v_2 - v_1] / [Q_2] / 3600$$

where

T = drawdown time in hours

v<sub>2</sub> = starting pond volume

v<sub>1</sub> = ending pond volume

Q<sub>2</sub> = starting flow

Broad Crested Weir Equation:

$$Q = C_{wb} * L * H^{1.5} + C_{wt} * S * H^{2.5}$$

where

L = bottom width of spillway

H = head above weir invert

S = side slopes (ratio of H:V)

C<sub>wt</sub> = broad-crested triangular weir coefficient

C<sub>wb</sub> = broad-crested rectangular weir coefficient

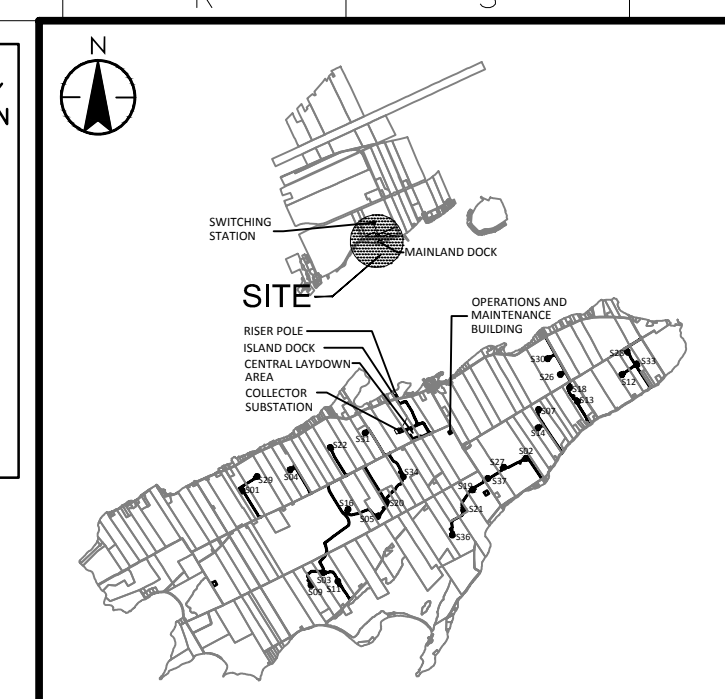
Subject: Grassed Swale  
 Project: Amherst Island Wind Energy Project - Mainland Laydown Area  
 Project No.: 1609-60595  
 Client: Windlectric  
 Date: July 5, 2017

Target Discharge (cms): 0.27  
 Bottom Width (m): 1  
 Side Slope (H:V): 3  
 Bottom Slope (m/m): 0.005  
 Hydraulic Roughness: 0.04

Depth (m)	Area (m <sup>2</sup> )	Perimeter (m)	Velocity (m/s)	Flow (cms)
0.00	0.000	0.00	0.00	0.00
0.01	0.010	1.06	0.08	0.00
0.02	0.021	1.13	0.13	0.00
0.03	0.033	1.19	0.16	0.01
0.04	0.045	1.25	0.19	0.01
0.05	0.058	1.32	0.22	0.01
0.06	0.071	1.38	0.24	0.02
0.07	0.085	1.44	0.27	0.02
0.08	0.099	1.51	0.29	0.03
0.09	0.114	1.57	0.31	0.04
0.10	0.130	1.63	0.33	0.04
0.11	0.146	1.70	0.35	0.05
0.12	0.163	1.76	0.36	0.06
0.13	0.181	1.82	0.38	0.07
0.14	0.199	1.89	0.39	0.08
0.15	0.218	1.95	0.41	0.09
0.16	0.237	2.01	0.42	0.10
0.17	0.257	2.08	0.44	0.11
0.18	0.277	2.14	0.45	0.13
0.19	0.298	2.20	0.47	0.14
0.20	0.320	2.26	0.48	0.15
0.21	0.342	2.33	0.49	0.17
0.22	0.365	2.39	0.51	0.18
0.23	0.389	2.45	0.52	0.20
0.24	0.413	2.52	0.53	0.22
0.25	0.438	2.58	0.54	0.24
0.26	0.463	2.64	0.55	0.26
0.27	0.489	2.71	0.56	0.28
0.28	0.515	2.77	0.58	0.30
0.29	0.542	2.83	0.59	0.32
0.30	0.570	2.90	0.60	0.34

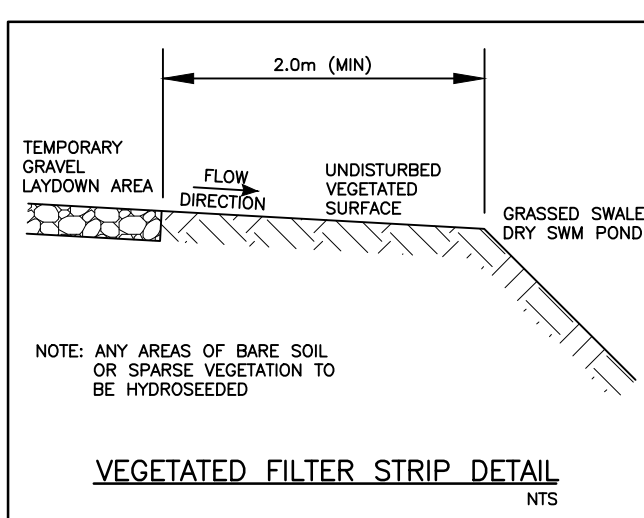
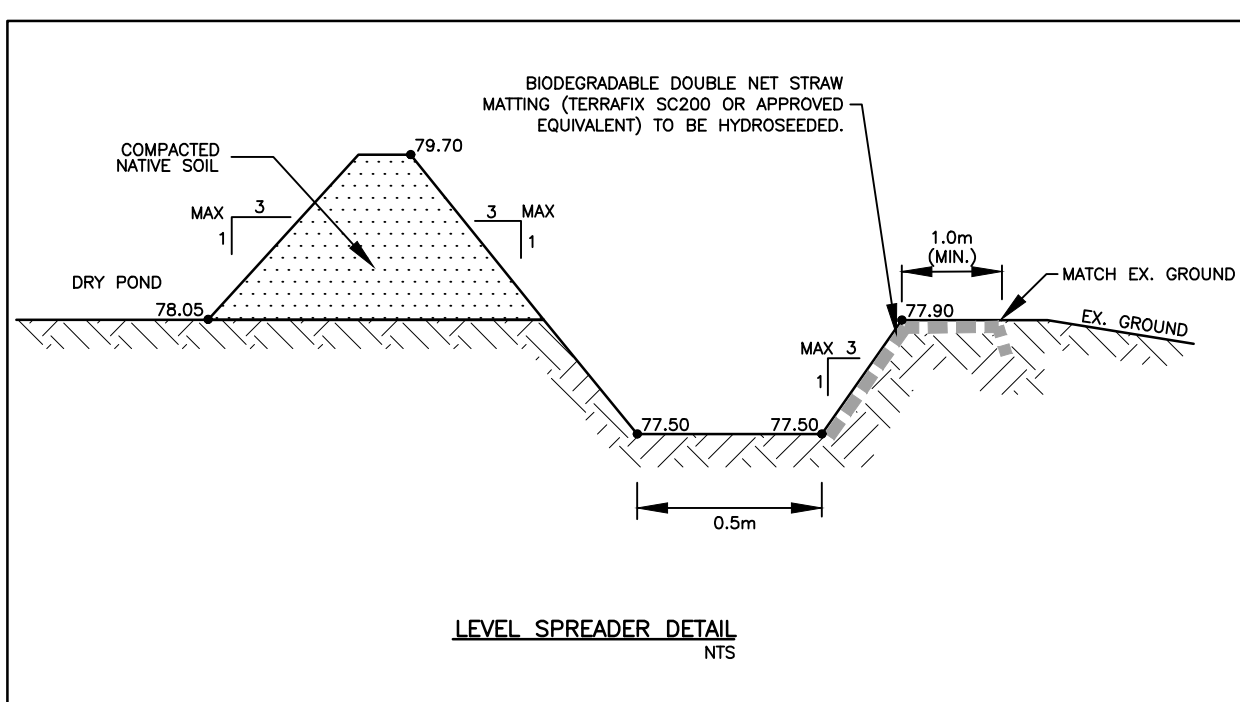
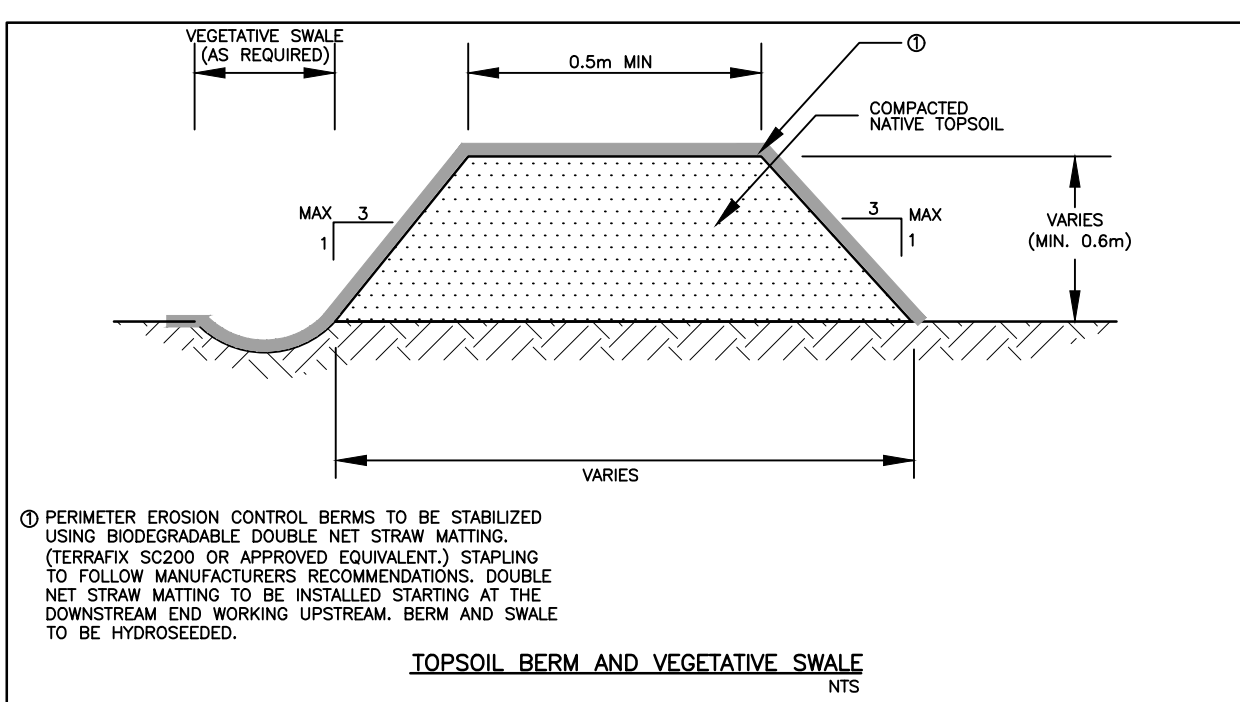
Notes

1. TOPOGRAPHIC SURVEY COMPLETED BY McINTOSH PERRY CONSULTING ENGINEERS DATED 2015 (UTM ZONE 18 NAD83 (GRS) 1987.0). GEOTECHNICAL INFORMATION PROVIDED BY STANTEC MEMO, DATED JUNE 2015.
2. THIS DRAWING TO BE READ IN CONJUNCTION WITH ALL OTHER DRAWINGS IN THIS SET PREPARED BY STANTEC CONSULTING LTD.
3. THE CONTRACTOR MUST CHECK AND VERIFY DIMENSIONS; OBTAIN ALL UTILITY LOCATES AND OBTAIN ALL REQUIRED PERMITS/LICENSES AND VERIFY ELEVATIONS OF EXISTING SERVICES BEFORE PROCEEDING WITH ANY WORK.
4. ALL CONSTRUCTION WORK SHALL BE CARRIED OUT IN ACCORDANCE WITH THE REQUIREMENTS OF THE OCCUPATIONAL HEALTH AND SAFETY ACT AND REGULATIONS FOR CONSTRUCTION PROJECTS (LATEST EDITION).
5. THE CONTRACTOR IS TO BE RESPONSIBLE FOR ALL DRAINAGE AND MEASURES TO CONTROL WATER. THE SITE IS TO BE FINE GRADED/ LEVELLED LEAVING THE SITE IN A NEAT APPEARANCE SUCH THAT POSITIVE DRAINAGE IS ACHIEVED.
6. CONTRACTOR MUST COMPLY WITH INVISTA CPU REQUIREMENTS.
7. ALL DISTURBED AREAS WITHIN THE PROPOSED WORKS ARE TO BE RE-VEGETATED USING NATIVE TOPSOIL AND SEED AS PER REAL MIX AND APPLICATION RATE/METHOD TO BE APPROVED PRIOR TO IMPLEMENTATION.
8. CLEARING AND GRUBBING AND REMOVALS TO BE COMPLETED IN ACCORDANCE WITH OPSS 201; TEMPORARY EROSION CONTROL TO BE COMPLETED IN ACCORDANCE WITH OPSS 805.
9. GRADING TO BE COMPLETED IN ACCORDANCE WITH OPSS 206.
10. GRANULAR MATERIAL TO BE USED IN ACCORDANCE WITH OPSS 1010.
11. ALL CULVERTS TO BE CONSTRUCTED IN ACCORDANCE WITH OPSS 421 AND AS PER OPSS 802.010.



KEY PLAN

N.T.S.

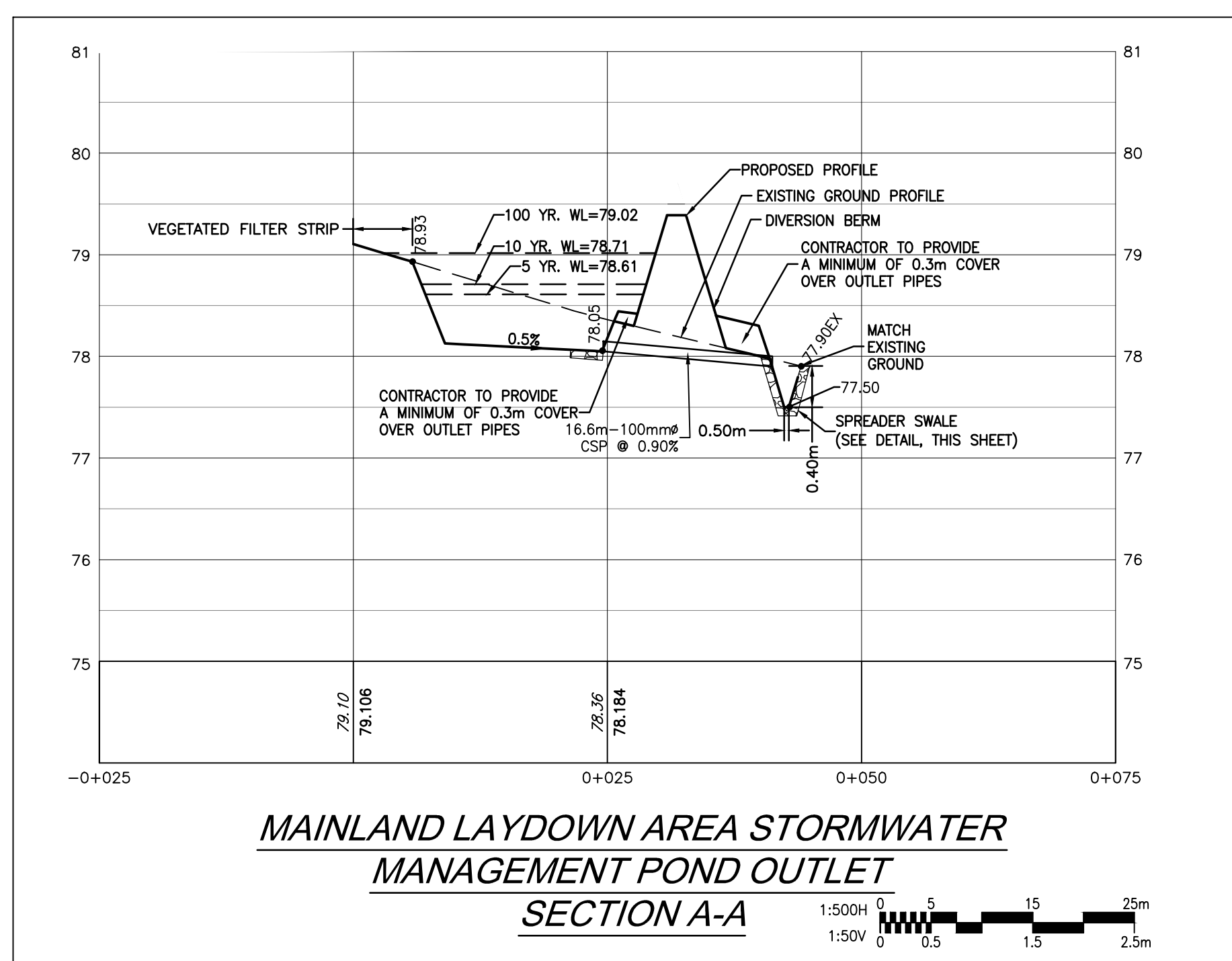


OSC SEED MIX #8215 - CREEK BANK SEED MIXTURE

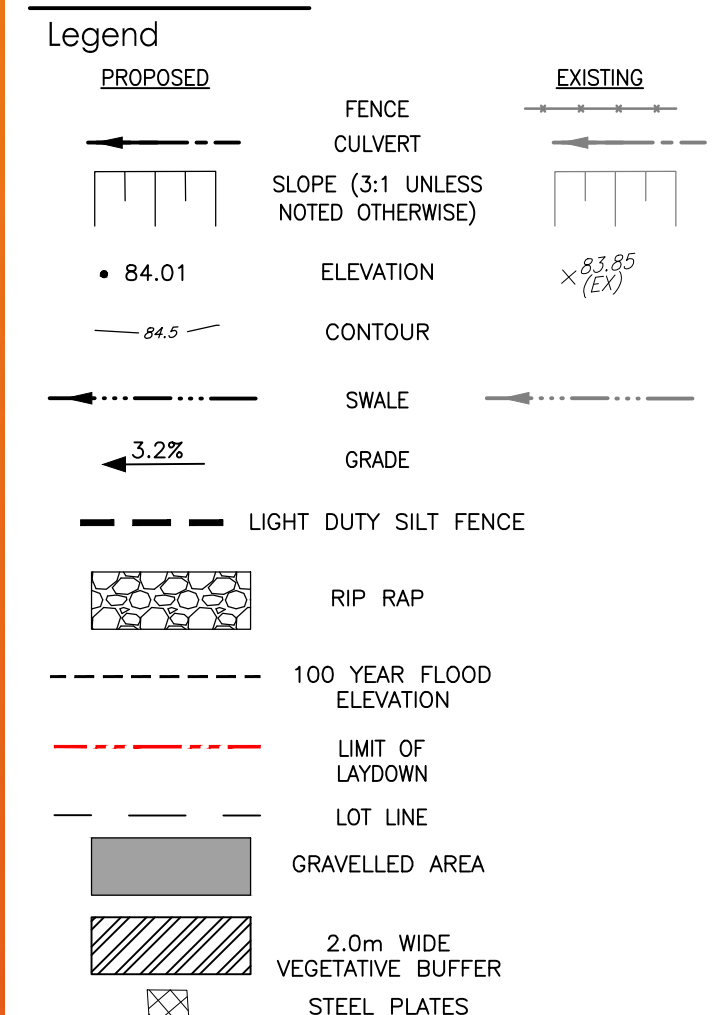
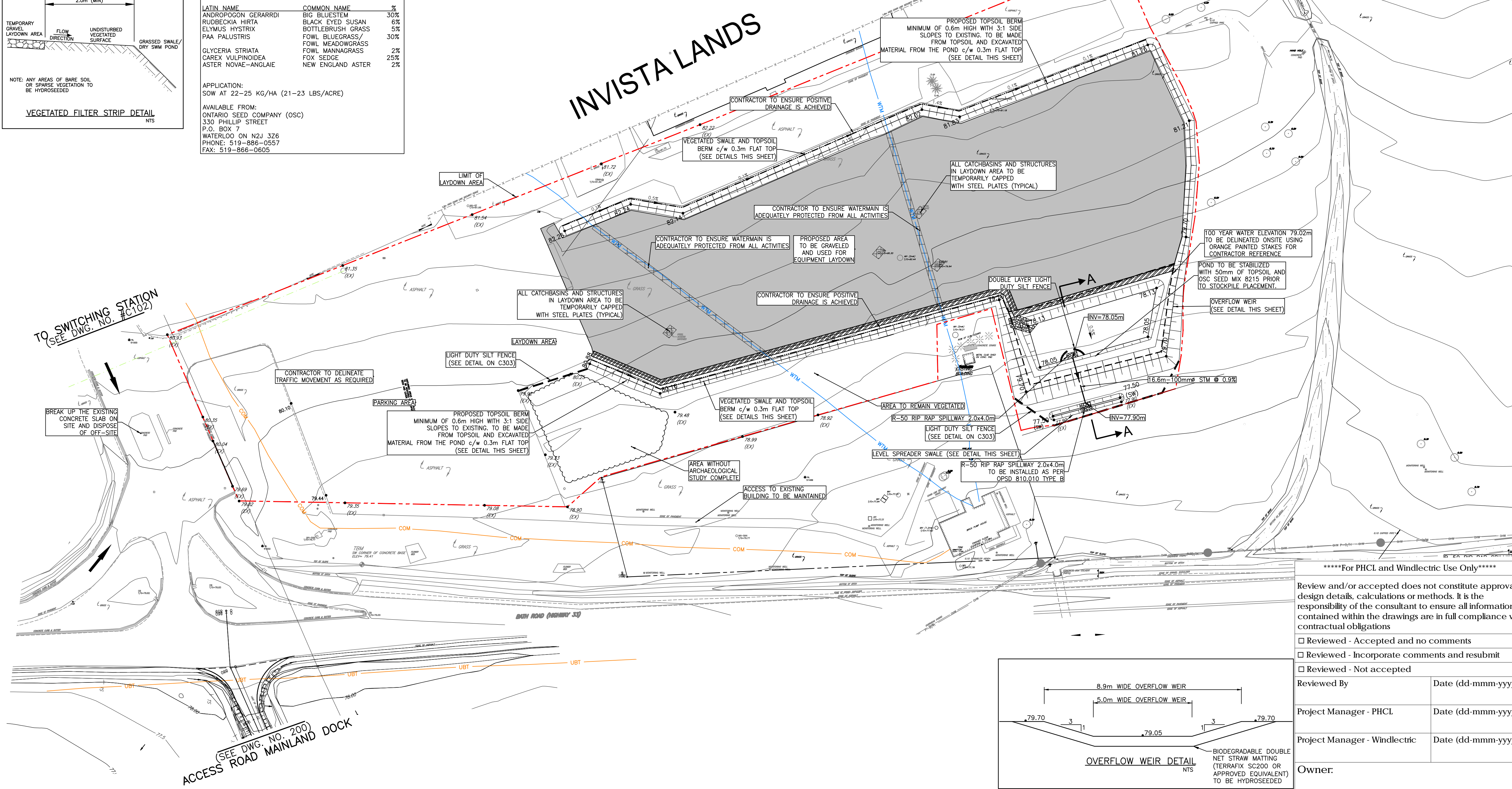
LATIN NAME	COMMON NAME	%
ANDROPOGON GERARDI	BIG BLUESTEM	30%
RUBRICKIA HIRTA	BLACK EYED SUSAN	6%
ELYMUS HYSTRIX	BOTTLEBRUSH GRASS	6%
PAA PALUSTRIS	FOWL BLUEGRASS	30%
GLYCERIA STRIATA	FOWL MEADOWGRASS	2%
CAREX VULPINOIDEA	FOWL SEDGE	25%
ASTER NOVAE-ANGLAIE	NEW ENGLAND ASTER	2%

APPLICATION:  
SOW AT 22-25 KG/HA (21-23 LBS/ACRE)

AVAILABLE FROM:  
ONTARIO SEED COMPANY (OSC)  
330 PHILLIP STREET  
P.O. BOX 7  
WATERLOO ON N2J 3Z6  
PHONE: 519-886-0557  
FAX: 519-866-0605



- NOTES:
1. ALL CONSTRUCTION ACTIVITIES ARE TO ADHERE TO THE SOIL/GROUNDWATER MANAGEMENT PROGRAM AND HEALTH & SAFETY PLAN, PREPARED BY STANTEC CONSULTING LTD. THESE PLANS ARE TO BE USED AS A REFERENCE TO FINAL CONSTRUCTION REQUIREMENTS, HOWEVER THE SOIL/GROUNDWATER MANAGEMENT PROGRAM AND HEALTH & SAFETY PLAN IS TO BE REVIEWED PRIOR TO BREAKING GROUND AND TO BE USED AS A REFERENCE FOR CONSTRUCTION ACTIVITIES AND PHASING.
  2. THIS DRAWING IS TO BE READ IN CONJUNCTION WITH DRAWING C303 FOR ADDITIONAL DETAILS AND NOTES
  3. THIS DRAWING IS TO BE READ IN CONJUNCTION WITH THE AMHERST ISLAND WIND ENERGY PROJECT MAINLAND LAYDOWN AREA EROSION AND SEDIMENT CONTROL PLAN AND STORMWATER MANAGEMENT REPORT
  4. ONE 100mm<sup>2</sup> END CAP TO BE ON SITE AT ALL TIMES TO BE AVAILABLE FOR EMERGENCY SPILL CONTAINMENT.
  5. LIGHT DUTY SILT FENCE TO BE INSTALLED AROUND PERIMETER OF ALL TEMPORARY STOCKPILED SOILS (AS REQUIRED)
  6. ALL RIPRAP SPILLWAYS TO BE MIN. 450mm THICK



Revision	By	Appd.	Y.M.M.D.D
F. ISSUED FOR MOECC APPROVAL	DMS	DKS	17.07.10
E. CIRCA LIMIT OVERLAY	DMS	DKS	17.04.27
D. PRELIMINARY - FOR CLIENT REVIEW	DMS	DKS	17.04.26
C. ISSUED FOR TENDER	JBM	DKS	17.02.10
B. UPDATED LAYDOWN CONFIGURATION	SJM	DKS	16.09.20
A. FOR CLIENT REVIEW	KDB	DKS	16.01.22

File Name	DS	DKS	DS	16.01.20
13356100-CG.dwg	Dm.	Chkd.	Dign.	Y.M.M.D.D

Permit-Seal

Client/Project  
**PENNECON HEAVY CIVIL**  
 AMHERST ISLAND WIND PROJECT  
 75MW WIND FARM  
 Amherst Island, Loyalist Township, Ontario

Title  
**MAINLAND LAYDOWN AREA  
 GRADING AND SEDIMENT AND EROSION  
 CONTROL PLAN**

Project No.	Scale	
13356100	1:750	
Drawing No.	Sheet	Revision
C104	1 of 1	F

\*\*\*\*\*For PHCL and Windlectric Use Only\*\*\*\*\*

Review and/or accepted does not constitute approval of design details, calculations or methods. It is the responsibility of the consultant to ensure all information contained within the drawings are in full compliance with contractual obligations

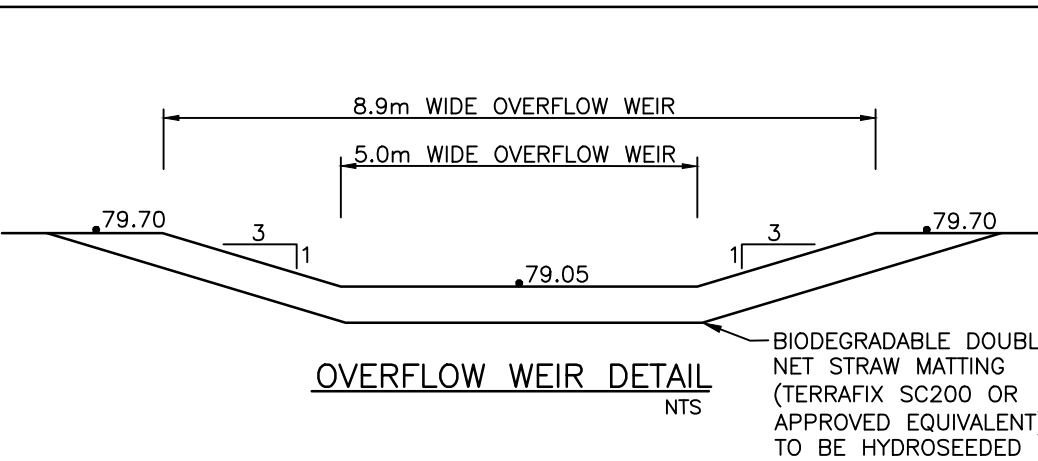
- Reviewed - Accepted and no comments
- Reviewed - Incorporate comments and resubmit
- Reviewed - Not accepted

Reviewed By \_\_\_\_\_ Date (dd-mmm-yyyy)

Project Manager - PHCL \_\_\_\_\_ Date (dd-mmm-yyyy)

Project Manager - Windlectric \_\_\_\_\_ Date (dd-mmm-yyyy)

Owner: \_\_\_\_\_



V:\0161\active\13356100\design\drawing\mainland\13356100-CG.dwg  
2017/07/14 10:03 AM By: Robb, Brad

Notes

- TOPOGRAPHIC SURVEY COMPLETED BY McINTOSH PERRY CONSULTING ENGINEERS DATED 2015 (UTM ZONE 18 NAD83 (GSD/1987)), GEOTECHNICAL INFORMATION PROVIDED BY STANTEC MEMO, DATED JUNE 2015.
- THIS DRAWING TO BE READ IN CONJUNCTION WITH ALL OTHER DRAWINGS IN THIS SET PREPARED BY STANTEC CONSULTING LTD.
- THE CONTRACTOR MUST VERIFY DIMENSIONS, OBTAIN ALL UTILITY LOCATES AND OBTAIN ALL REQUIRED PERMITS/LICENSES AND VERIFY ELEVATIONS OF EXISTING SERVICES BEFORE PROCEEDING WITH ANY WORK.
- ALL CONSTRUCTION WORK SHALL BE CARRIED OUT IN ACCORDANCE WITH THE REQUIREMENTS OF THE OCCUPATIONAL HEALTH AND SAFETY ACT AND REGULATIONS FOR CONSTRUCTION PROJECTS (LATEST EDITION).
- ENCROACHMENT ON NON-PARTICIPATING PROPERTIES IS STRICTLY PROHIBITED. THE CONTRACTOR AND/OR THEIR REPRESENTATIVES ARE TO BE AWARE OF ALL PARTICIPATING LAND OWNERS ON THE PROJECT AND THE PROJECTS CONSTRUCTIBLE LIMITS. ALL CONSTRUCTION ACTIVITY BEYOND THE CONSTRUCTIBLE LIMITS IS STRICTLY PROHIBITED.
- THE CONTRACTOR IS RESPONSIBLE FOR RESTORATION OF ALL DAMAGED AND/OR DISTURBED PROPERTY WITHIN THE MUNICIPAL RIGHT-OF-WAY TO THE CURRENT MUNICIPAL STANDARDS AND SHALL CONFORM TO ROAD USE AGREEMENT.
- THE CONTRACTOR IS TO BE RESPONSIBLE FOR ALL DRAINAGE AND MEASURES TO CONTROL STORM WATER. THE SITE IS TO BE FINE GRADED/LEVELLED LEAVING THE SITE IN A NEAT APPEARANCE SUCH THAT POSITIVE DRAINAGE IS ACHIEVED.
- CONSTRUCTION TURNING RADIUS LIMITS IDENTIFY AREAS WHERE ADDITIONAL ROAD WIDTH IS REQUIRED TO ALLOW FOR ADEQUATE CLEARANCE FOR CONSTRUCTION VEHICLES.
- ALL DISTURBED AREAS ARE TO BE RE-VEGETATED USING NATIVE TOPSOIL AND SEED AS PER REA APPROVAL. MIX AND APPLICATION RATE/METHOD TO BE APPROVED PRIOR TO IMPLEMENTATION.
- CLEARING AND GRUBBING AND REMOVALS TO BE COMPLETED IN ACCORDANCE WITH OPSD 201. TEMPORARY EROSION CONTROL TO BE COMPLETED IN ACCORDANCE WITH OPSD 805.
- GRADING TO BE COMPLETED IN ACCORDANCE WITH OPSD 206.
- GRANULAR MATERIAL TO BE USED IN ACCORDANCE WITH OPSD 1010.
- ALL CULVERTS TO BE CONSTRUCTED IN ACCORDANCE WITH OPSD 421 AND AS PER OPSD 802.010.

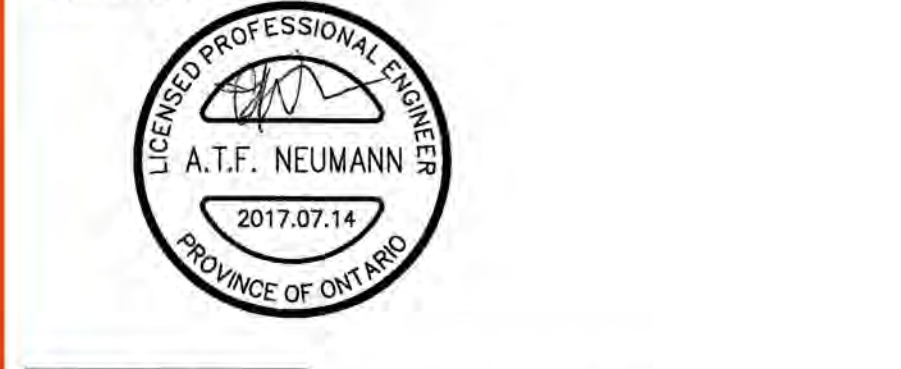
Legend

Revision	By	Appd.	YY.MM.DD
2	DMS	TN	17.07.14
1	DMS	DKS	17.04.13
0	JBM	DKS	17.01.20

Revision By Appd. YY.MM.DD

File Name	DS	DKS	DS	16.12.12
File Name: 133560100C-07.dwg	Dwn.	Chkd.	Dgn.	YY.MM.DD

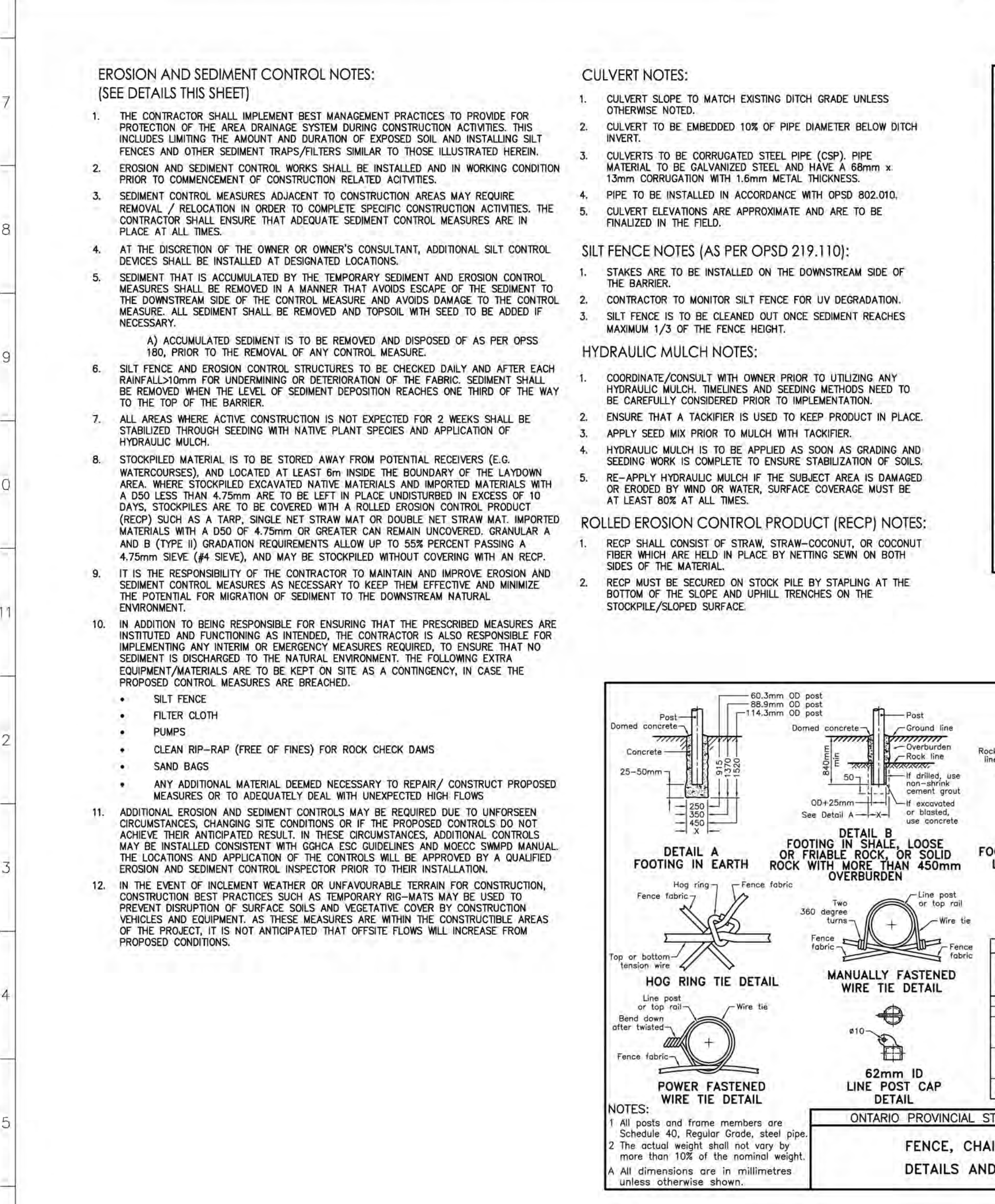
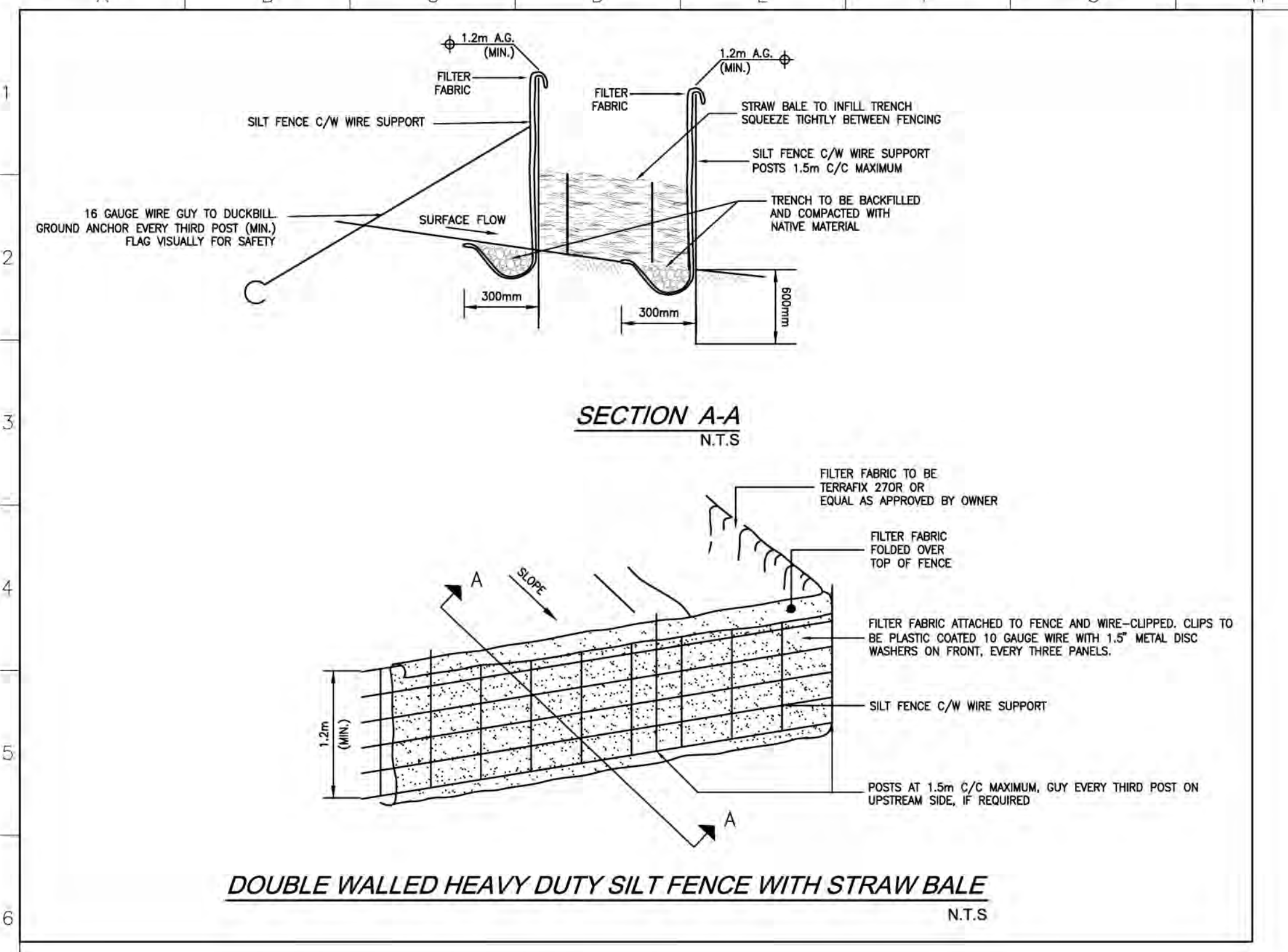
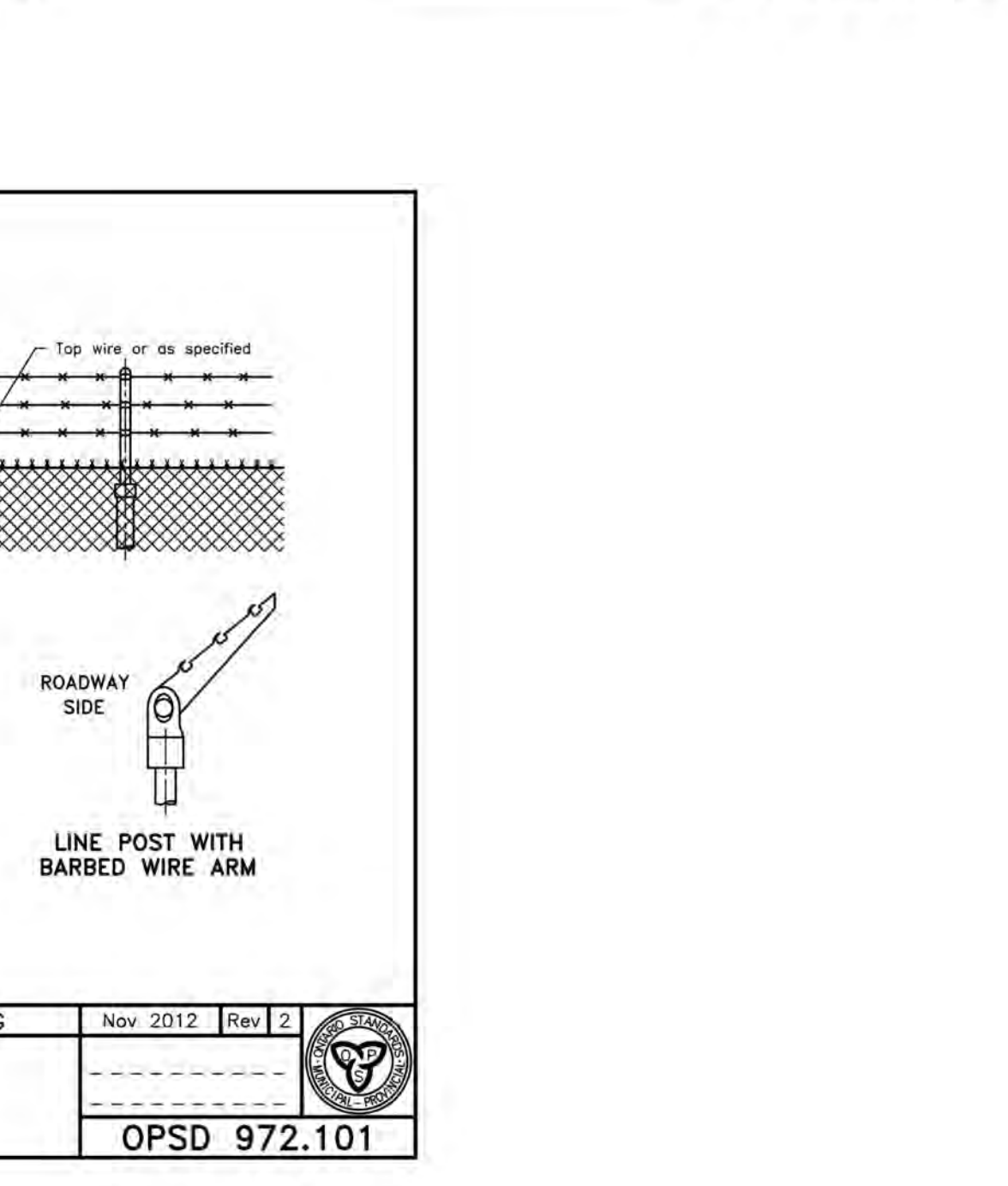
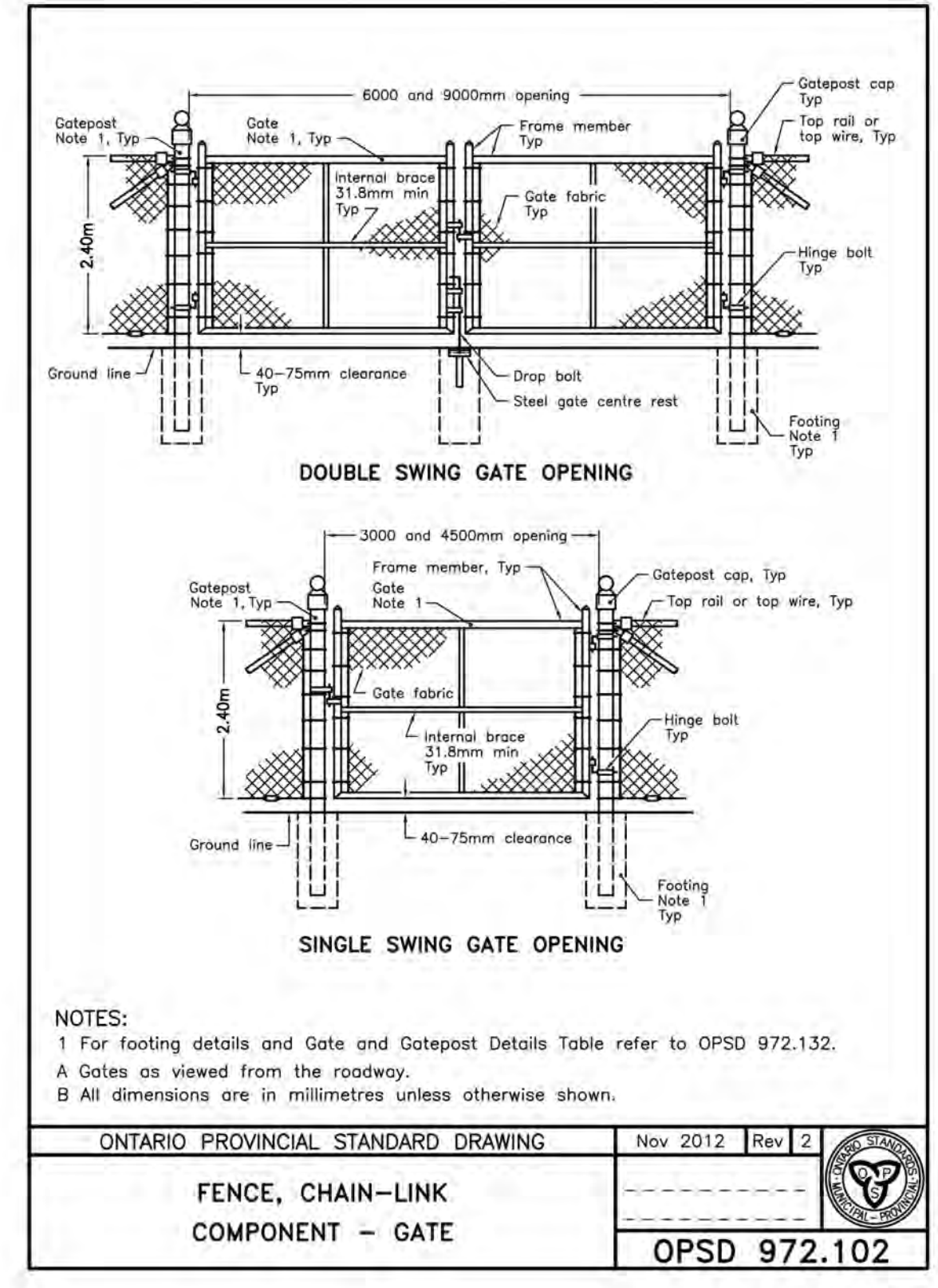
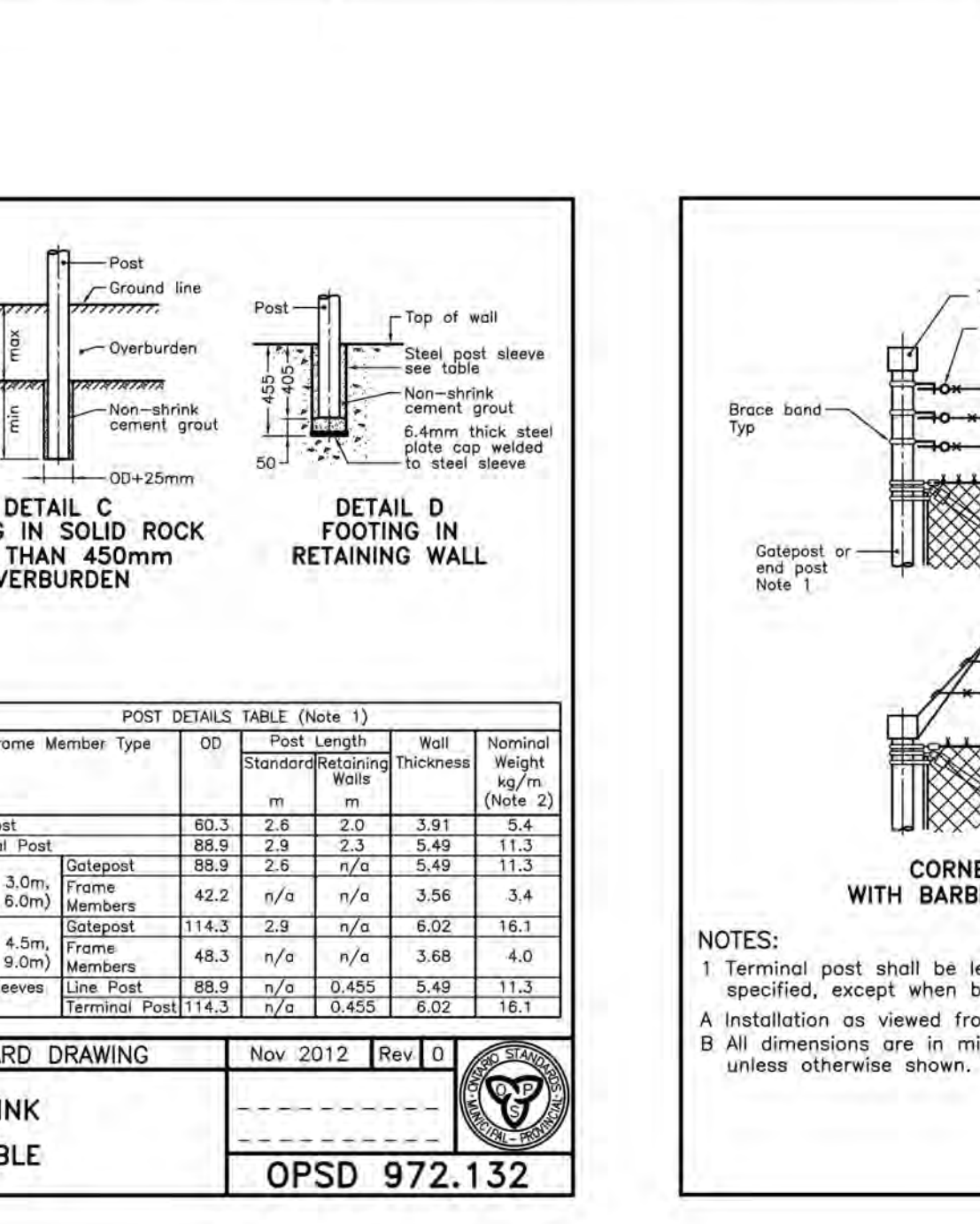
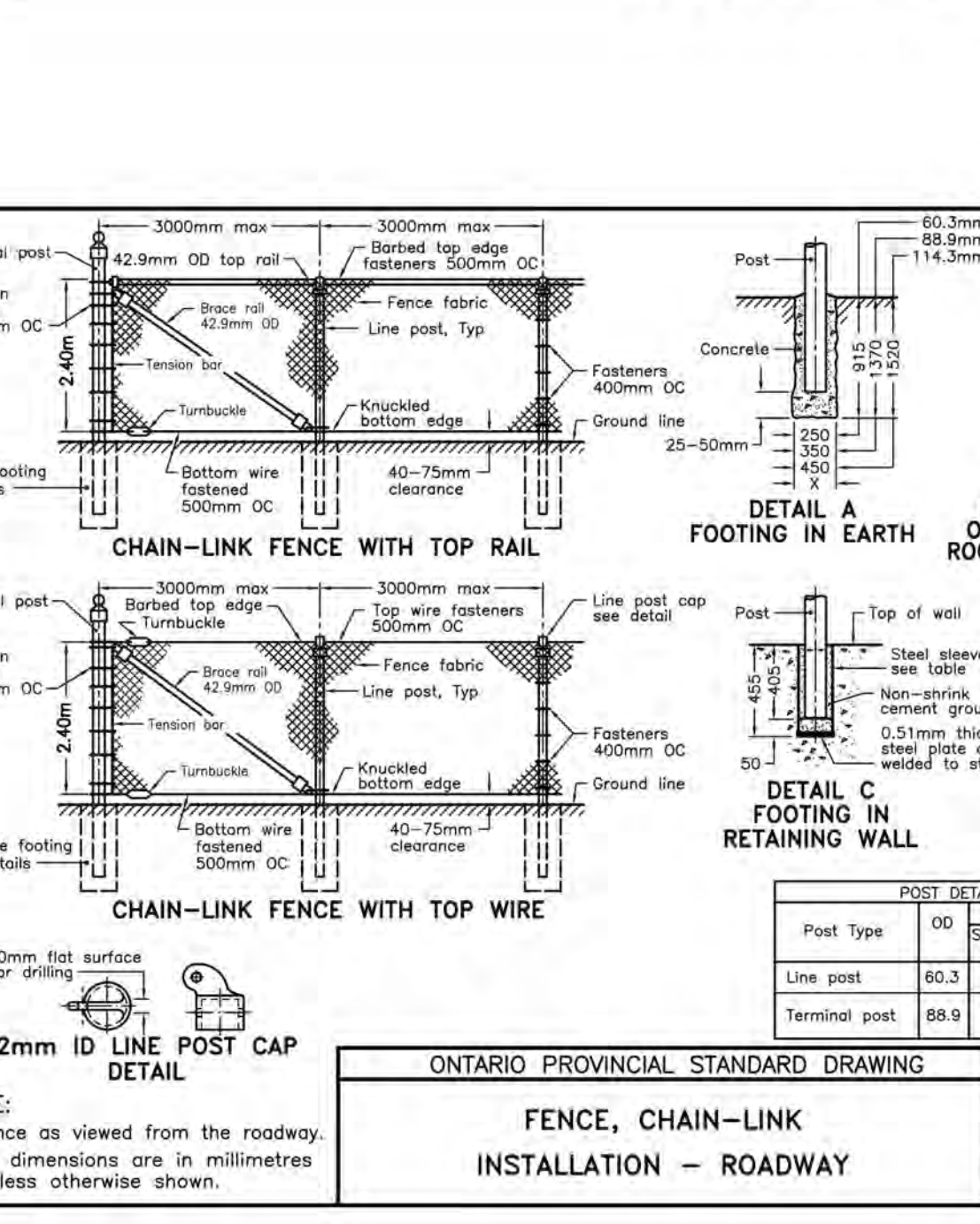
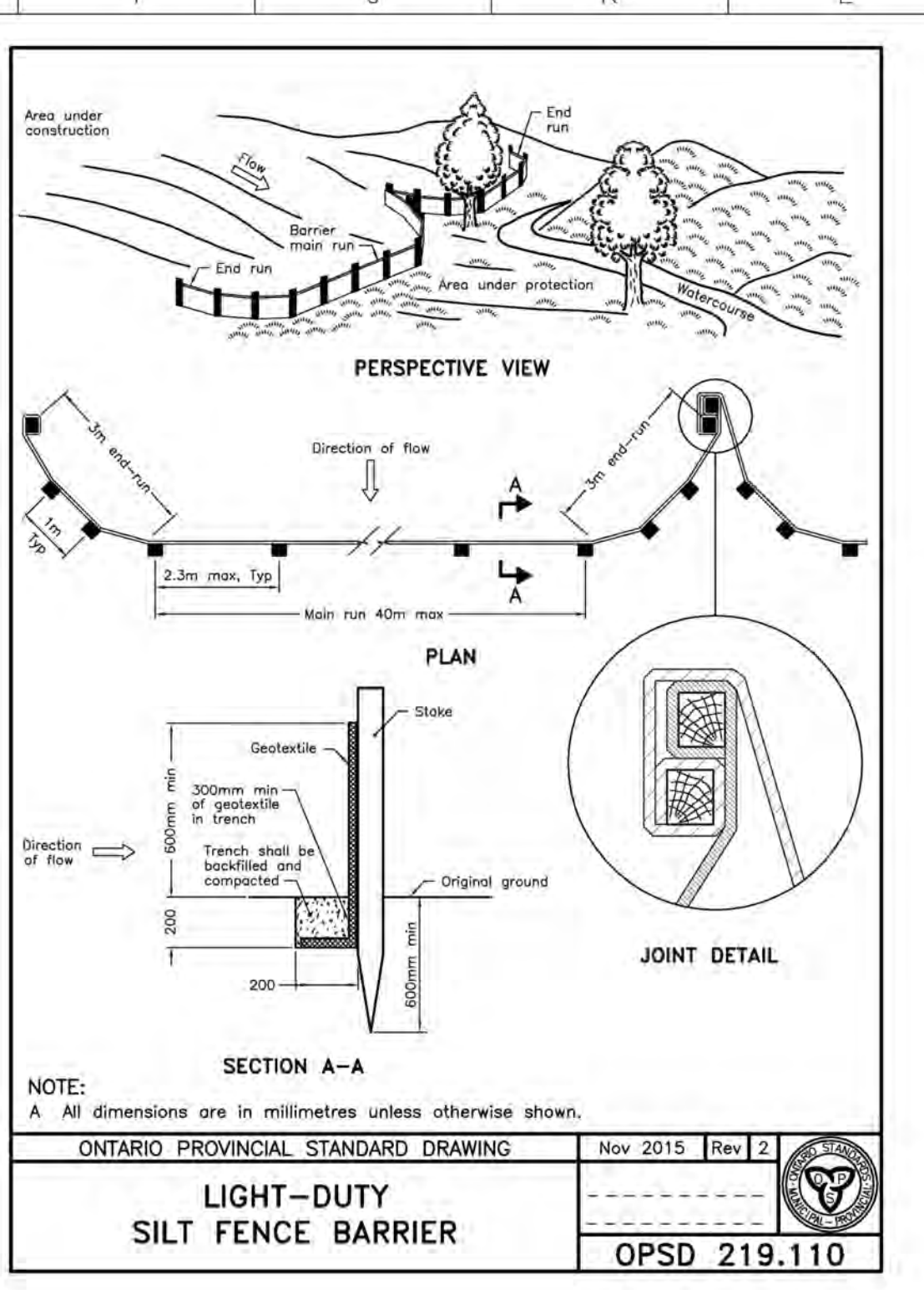
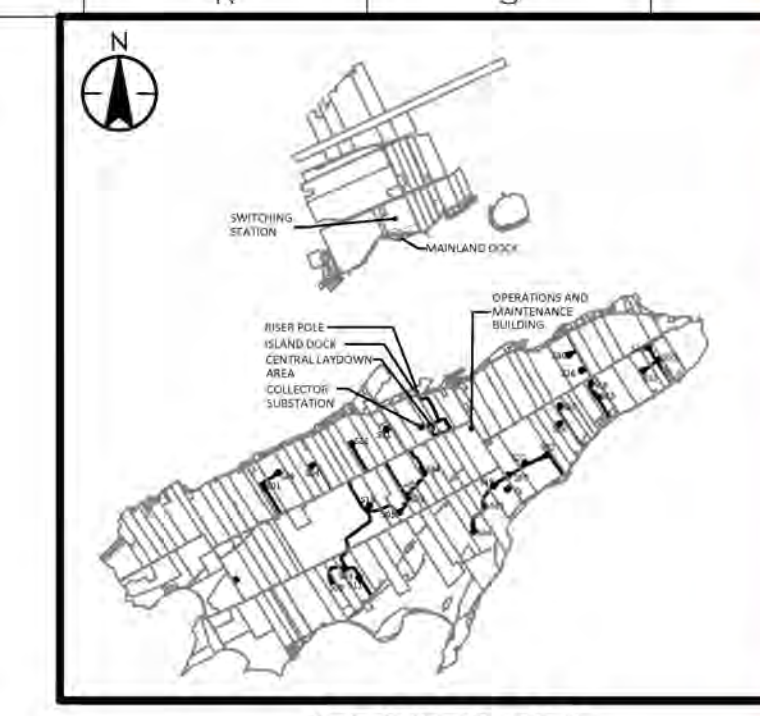
Permit-Seal



Client/Project  
**PENNECON** HEAVY CIVIL  
AMHERST ISLAND WIND PROJECT  
75MW WIND FARM  
Amherst Island, Loyalist Township, Ontario

Title  
**SITE DETAIL SHEET**

Project No.	Scale
133560100	
Drawing No.	Sheet
C303	1 of 1
	Revision
	2



V:\0161\Archive\133560100\Design\Drawings\ChainLink\Bent\133560100C-07.dwg  
2017/07/14 1:34 AM By: Robb, Brad