Municipal Roads, Geotechnical Borehole Investigation Amherst Island Wind Energy Project, Amherst Island, Ontario

Project Number: 133560104



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Sign-off Sheet

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Introduction August 29, 2017

1.0 INTRODUCTION

Pennecon Heavy Civil Limited (PHCL) commissioned Stantec Consulting Ltd. (Stantec) to carry out a geotechnical investigation of the municipal roads on Amherst Island.

The purpose of the investigation was to confirm the existing conditions (presence, thickness and condition of asphalt and/or granular materials and soil type/condition of the underlying subgrade) and subsequently assess the use of the existing municipal roads as 'heavy haul routes' during construction of the planned project.

This report provides a summary and overview of the conditions encountered in the boreholes advanced for the investigation and the results of the laboratory testing completed on samples of the granular materials and sub-grade soils collected. This report also includes an assessment of the anticipated construction traffic on the island and an assessment of the heavy haul traffic that the municipal roads can support in the present condition.

Use of this report is subject to the Statement of General Conditions provided in Appendix A.

2.0 AREA OF INVESTIGATION

Given the current proposed layout of the project and the intended locations of the wind turbines, the following municipal roads were investigated:

- Front Road
- Stella 40 Foot Road
- 2nd Concession Road
- 3rd Concession Road
- South Shore Road
- Lower 40 Foot Road
- Dump Road

For reference, the portion of Front Road in the immediate area of the town core and the initial portion of Stella 40 Foot Road from Front Road to 2nd Concession were not included in the scope of the investigation.



Field Investigation Program August 29, 2017

3.0 FIELD INVESTIGATION PROGRAM

3.1 PRE-INVESTIGATION MEASURES

The locations of the boreholes were established with a general view to obtaining information along the portion of the municipal roads of interest. The specific locations of the boreholes were constrained by the locations of residences and development and availability of access for the drilling equipment.

Prior to commencing the drilling investigation, Stantec contacted Ontario One-Call to identify and confirm the potential presence of buried utilities and services in proximity to the borehole locations. Staff from Stantec accompanied the utility locate contractor during the execution of the utility locates program.

Prior to commencing the drilling investigation, Algonquin Power (developers) forwarded letters of notification to local residents requesting that any knowledge of existing infrastructure (buried water mains or electrical cables) near the proposed borehole locations be provided. In consideration of the responses to this inquiry, the locations of several boreholes were adjusted to reflect the potential presence of private buried utilities or services that were not identified through the public utility locates program.

Algonquin Power coordinated obtaining the necessary Excavation Permits and a Temporary Road Closure Permit (specific to Dump Road) with Loyalist Township.

Use of this report is subject to the Statement of General Conditions provided in Appendix A.

3.2 BOREHOLE LOCATIONS AND NUMBERS

The number of boreholes was established to provide general coverage of the municipal roads of interest (reference the list provided in a previous section of this report) with consideration for the general characterization of the roads based on previous visual observations.

The following table provides a summary of the type of roads (or general purpose) and number of investigation holes included in the program.



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Table 1 Summary of Investigation Holes

Road Type	Number of Boreholes
Paved Roads	4
Gravel Roads	2
Poor Quality Roads	19
Proposed Road Widening	6
Existing Culverts	2 (hand dug test pits)
Proposed O/M Building	1

The road boreholes were advanced on the travelled surface of the road with due consideration for avoiding traffic disruption and consideration for appropriate traffic control and safety.

The boreholes at the locations of the two culverts were deleted from the program in lieu of hand-dug test pits to confirm the thickness of cover over the existing culverts.

The borehole for the O/M Building was included in the current municipal road investigation program for efficiency in execution. The borehole was advanced on the edge of the travelled surface of the road.

The boreholes were advanced to relatively shallow depth, consistent with penetrating the full depth of the asphalt and/or granular road structure and terminating in the underlying native soils/sub-grade. Sampling was conducted in accordance with the Standard Penetration Test as described in ASTM D1586. Samples were obtained on a continuous basis in all of the boreholes.

The locations of the boreholes are illustrated on the drawing in Appendix B.

3.3 DRILL EQUIPMENT

The boreholes were advanced with a truck mounted drill rig supplied and operated by Terex Drilling Solutions based in Concord, Ontario.

3.4 TRAFFIC CONTROL

Traffic control services were provided by On Track Safety Limited, based in Thornhill, Ontario, specialists in traffic management and control.

Traffic control was provided in accordance with the latest version of "Ontario Traffic Manual Book 7 Temporary Conditions" (OTM Book 7).

Based on the rural nature of the municipal roads on the island and the prevailing light traffic volume, Typical Layout Figure TL-19 was adopted for the traffic control program. This Layout Type applies to low volume roads, very short duration work.



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The exception to the traffic control plan described in the preceding paragraph was Dump Road. Given the extremely narrow width of this road, the Township required a temporary closure from 2nd Concession Road to the north while maintaining access from Front Road to the south.

3.5 DRILLING PROGRAM

The field drilling program was completed in accordance with the following:

- The boreholes were advanced using solid stem augers.
- Standard Penetration Testing (SPTs) was conducted on a continuous basis in each borehole.
- Soil samples were collected from the split tubes advanced for the SPTs.
- The soil samples were placed in moisture-proof containers for storage and transport.
- The presence of groundwater seepage and/or free groundwater in the open borehole was recorded (where applicable).

Coring of the underlying bedrock (known to exist at shallow depth based on the results of previous investigation drilling and test pitting on the island) was not intended or required as a component of the investigation proposed herein. In several boreholes, augering and/or sampling was terminated on presumed bedrock.

The installation of groundwater monitoring stand-pipes or monitoring wells was not included as a component of the investigation.

The boreholes were backfilled with a low-permeability mixture of the auger spoils and granular bentonite, meeting the intent of MOE Regulation 903.

A "cold-asphalt" plug was placed at the ground surface of the boreholes advanced through existing asphaltic pavements.

Consistent with the Township's request, the drilling program included consideration for barreling, testing and disposing of excess soils generated while drilling at an approved (off-island) location. However, given the limited depth of the boreholes and the volume of the samples retained for geotechnical characterization and testing, excess soils were not generated.

Stantec's Standard Operating Procedures included consideration for identification of potential environmental contamination (e.g. via olfactory or visual observation) during the investigation. If such conditions were observed, Stantec would report the conditions to Algonquin Power for discussion and further action as may be warranted.



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3.6 SURVEYING

As outlined in a previous section, the locations of the boreholes were established to provide general coverage of the municipal roads of interest (reference the list provided in a previous section of this report) with consideration for the general characterization of the roads based on previous visual observations. The specific locations of the boreholes were constrained by the locations of residences and development and availability of access for the drilling equipment.

The coordinates for the "as-drilled" locations of the boreholes were recorded in the field using hand-held GPS. The locations were referenced to the Universal Transverse Mercator (UTM) NAD 83 CSRS Zone 18N.

The ground surface elevations at the borehole locations were inferred from the available topographic information. The ground surface elevations were referenced to Canadian Geodetic Vertical Datum (CGVD) 1929/1978 adjustment.

The coordinates are shown in the table on Drawing No. 1 in **Appendix B**. The ground surface elevations are shown on the borehole (and test pit) records in **Appendix C**.

3.7 GEOTECHNICAL LABORATORY TESTING PROGRAM

The geotechnical laboratory testing program was to include the following:

- Grain size distribution tests Representative samples of the granular surfacing.
- Grain size distribution tests Representative samples of the underlying native sub-grade soils.
- Atterberg Limits tests Representative samples of the underlying native sub-grade soils.
- Moisture Content Tests Representative samples of granular surfacing and the underlying native sub-grade soils.
- Unit Weight tests Limited number of representative samples of the underlying native sub-grade soils.
- Moisture-Density Relations Two (2) representative samples of the underlying native subgrade soils.



Health and Safety August 29, 2017

4.0 HEALTH AND SAFETY

Stantec's Safe Work Practices (SWPs) are documents designed around specific tasks and are intended to help identify hazards and applicable controls necessary to reduce our employees' exposure to health and safety risks. The following SWPs apply to all drilling field investigation activities undertaken by Stantec.

Risk Management Strategy (RMS) 1 – Prepared in advance of commencement of work.

Risk Management Strategy (RMS) 2 - Prepared in the field at the time of the work.

Safe Work Practice (SWP (416) - Supervision of Contracted Drilling Activities.

The RMS1 document was prepared at commencement of the project. The document included a description of the work, recognition of applicable hazards, an assessment of the hazards, applicable and appropriate Personal Protective Equipment (PPE), and H&S contacts, documentation, and controls.

The RMS2 (Fit for Duty) is an extension of the RMS1 and was completed by the field staff on mobilization to the Island to conduct the geotechnical investigation. The RMS2 includes a field evaluation of conditions with a view to identifying potential hazards (or changed conditions) that were not identified at the time of the RMS1. It also provides for an opportunity to discuss all potential hazards and concerns with the sub-contractors present and engaged in the work, and finally includes a requirement that the field staff acknowledge they are physically capable of carrying out the required tasks.

Stantec's SWP 416 includes a comprehensive description of the responsibilities, potential hazards, and controls associated with executing field drilling activities.

Field staff (both Stantec and the drilling sub-contractor) were required to have the following personal protective equipment (PPE):

- Hearing protection;
- Eye protection;
- Head protection;
- High-visibility vests; and,
- CSA approved work boots (with a 6" steel shank and a defined heel).



Factual Results of the Investigation August 29, 2017

5.0 FACTUAL RESULTS OF THE INVESTIGATION

5.1 REFERENCE STANDARDS

The soils encountered in the boreholes were classified in accordance with the Unified Soil Classification System (USCS). Stantec adopts minor modifications to the USCS Standard consistent with the methods of the Ontario Ministry of Transportation (MTO) including the removal of the descriptions "lean" and "fat" with reference to clay soils, and including a "Medium" category with respect to plasticity.

It should be noted that the internal diameter (I.D.) of the split tube used in the Standard Penetration Test is 38 mm and hence the grain size test results and soil classifications may not reflect the entire gravel size fraction which extends to 75 mm diameter.

The presence of cobbles and/or boulders is similarly not reflected in the grain size distribution tests and typically described separately, when and where these materials are inferred to have been encountered in the boreholes.

5.2 SUBSURFACE CONDITIONS

5.2.1 Overview

The subsurface conditions encountered in the boreholes are provided in the table in **Appendix C**. The results of the geotechnical laboratory testing program are included in **Appendix D**.

In general, the subsurface stratigraphy encountered in the boreholes consisted of asphalt (on select roads), granular fill materials (travel surface or as base/sub-base under the asphalt pavement), and native sub-grade soils. Inferred bedrock was encountered in several boreholes based on the content of the split tube samples and/or on the progress or resistance/refusal to augering and/or sampling.

5.2.2 Asphalt Pavement

Front Road East was asphalt paved. The thickness of the asphalt in the two boreholes advanced on this road was approximately 1" (25 mm).

A portion of Front Road West (extending west from the intersection with Stella 40 Foot Road) was also asphalt paved. The two boreholes advanced along this portion of the road encountered two layers of asphalt; a surface layer that was approximately 1" (25 mm thick) and a second underlying layer (below a granular layer) that was also approximately 1" (25 mm) thick.



Factual Results of the Investigation August 29, 2017

A portion of Stella 40 Foot Road (from the intersection with 2nd Concession Road and extending south) was also asphalt paved. The two boreholes advanced along this portion of the road encountered asphalt that was 1.5" (37.5 mm) and 2" (50 mm) thick.

5.2.3 Granular Materials

The granular material underlying the asphalt on Front Road East was 6" (150 mm) and 9" (225 mm) thick.

The granular material underlying the surface course of asphalt on Front Road West was 3" (75 mm) and 4" (100 mm). The granular material underlying the buried asphalt layer was 4" (100 mm) and 5" (125 mm) thick.

The granular material underlying the asphalt on Stella 40 Foot Road was 13" (330 mm) and 5 $\frac{1}{2}$ " (140 mm).

The thickness of the existing granular surfacing encountered in the boreholes varied considerably. The following table provides a summary of the range in thicknesses recorded for the boreholes advanced on the respective roads (locations where asphalt was present are discussed in the preceding paragraphs and not included in the table).

	Road	Number of Boreholes	Granular Surface Thickne (Inches/mm)
ſ	Front Road East	3	7.5/190 – 10/250
ſ	Lower 40 Foot Road	3	7.5/190 – 8/200
ſ	South Shore Road	4	4/100 - 10/250
ſ	Stella 40 Foot Road	1	7/190
ſ	2 nd Concession Road	7	6/150 – 8/200
ſ	3 rd Concession Road	6	7/180 – 12/300
	Dump Road	2	No Granular Surface

Table 2 Summary of the Granular Surface Thickness

For additional reference, the hand-dug test pit at the location of the existing culvert on Stella 40 Foot Road encountered 10" (250 mm) of granular cover and the hand-dug test pit at the location of the existing culvert on Marshall 40 Foot Road encountered 7" (180 mm) of granular cover.

The existing granular surfacing consists of well-graded sand and gravel with a varying fines content.



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Moisture content tests were conducted on 17 samples of the granular surfacing material. The tests yielded results in a narrow range, from 2.1% to 3.9%.

A total of 17 grain size analysis tests were conducted on samples of the granular surfacing. The tests yielded a fines content (combined percentage of silt and clay size particles) ranging from 9% to 24% and the average of the samples tested was 18.5%. For reference, this percentage of fines exceeds the maximum fines percentage for OPSS Granular A base material (e.g. 8%).

The results of the grain size analysis tests are shown on the grain size analysis tests curves in Figures 1 to 4 in **Appendix E**.

5.2.4 Subgrade

The subgrade encountered underlying the asphalt and granular materials consisted of sandy clay, clay with sand, and silty clayey sand.

For reference, the hand-dug test pit at the location of the existing culvert on Stella 40 Foot Road encountered 5" (130 mm) of topsoil and fill material underlying the granular material noted in the preceding section; combined the granular material and fill material provided 15" (380 mm) of cover over the top of the culvert. The hand-dug test pit at the location of the existing culvert on Marshall 40 Foot Road encountered 2" (50 mm) of topsoil and fill material underlying the granular material noted in the preceding section; combined the granular material and fill material underlying the material provided 9" (230 mm) of cover over the top of the culvert.

Moisture content tests were conducted on seven samples of the native subgrade soils. The results were typically in two ranges; a lower range with two results of 6.5% and 7.5% and a higher range of 16.6% to 30%. The lower range is representative of the samples described as silty clayey sand soil and the higher range is representative of the samples described as sandy clay and clay with sand.

The results of grain size analysis tests completed on seven samples of the native subgrade soils are shown on Figures 5 and 6 in **Appendix D**.

The results of Atterberg Limits tests completed on the seven samples are illustrated on the Plasticity Chart included as Figure 7 in **Appendix D**.

The test results indicate that these soils contain varying proportions of sand, silt, and clay, with very limited gravel (e.g. typically 5% or less). The varying percentage of sand, silt and clay size particles also reflect the varying plasticity index test results; the soils range from low to high plasticity.

As indicated above and in accordance with the Unified Soil Classification System, the soil samples tested can be characterized as sandy clay (CL), clay with sand (CH) and silty clayey sand (SC-SM).



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Four samples of the native subgrade were submitted for unit weight tests. The tests yielded unit weights of 18.8 kN/m³, 17.6 kN/m³, 21.0 kN/m³ and 19.2 kN/m³.

Moisture-density relations tests were completed on 2 samples of the native sub-grade soil. The tests yielded results of 1995 kg/m³ and 1900 kg/m³ at optimum moisture contents of 10.7% and 13.0% respectively.

A single sample of the silty clayey sand (SC-SM) was selected for California Bearing Ratio (CBR) testing. The result yielded a CBR of 4.99 (un-soaked) for a penetration of 2.5 mm and a CBR of 5.39 (soaked) for a penetration of 2.5 mm. A single sample of the clay with sand (CH) was selected for CBR testing. The result yielded a CBR of 1.30 (un-soaked) for a penetration of 2.5 mm and a CBR of 1.67 (soaked) for a penetration of 2.5 mm.

5.2.5 Bedrock

The inferred depth to bedrock is indicated on the borehole summary table in **Appendix C**. The depth is indicated as "inferred" given that coring of the rock was not included as a component of the investigation. The contact surface with the bedrock was inferred based on refusal of the augers and/or sampler.

As indicated, the majority of the boreholes encountered the inferred surface of the bedrock at depths ranging from 0.33 m to 3.51 m. Several boreholes were terminated at depths of 3.66 m below grade without encountering the inferred contact with the underlying bedrock.

5.2.6 Groundwater

Free groundwater was not observed in any of the open boreholes at the time of drilling.

6.0 MUNICIPAL ROAD ASSESSMENT

6.1 ASSESSMENT METHODOLOGY

Two methods were used to assess the suitability of the existing and proposed roads to handle the anticipated heavy haul traffic.

For the majority of the roads, the 1993 AASHTO Guide of Design of Pavement Structure methodology for aggregate-surface roads was used. This approach considers two serviceability limits mechanisms as follows:

• Loss of Pavement Serviceability Index (PSI) which indicates a general decline in the road surface. For the assessment completed, an allowable decrease in serviceability of 2.0 was set as the maximum allowable.



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• Surface wheel path rutting which allows for a specific depth of ruts. For the assessment completed, a rut depth of 50 mm was permitted.

For the new road required from the new island dock to 2nd Concession Road and for Dump Road, the assessment was undertaken using a geotextile methodology by DuPont Typar titled Designing Aggregate Bases.

6.2 **EXISTING CONDITIONS**

6.2.1 Road Granular

As discussed above in Section 5.0, the existing roadway granular surfacing consists of a wellgraded sand and gravel with a percentage of silt/clay (e.g. fines) that exceeds the OPSS specification for typical granular base materials.

As a result of the high silt/clay content, the existing granular surfacing is prone to softening and rutting in wet conditions and the surface can become muddy. Under the heavy haul traffic anticipated, this condition will be compounded.

6.2.2 Subgrade

As discussed above in Section 5.0, the predominant subgrade type underlying the existing roadways (and encountered in the majority of the boreholes advanced on the island to date) consists of sandy clay, clay with sand, and silty clayey sand. For convenience, these soil strata are referred to in subsequent sections as sandy clay.

The soil types described above are generally characterized as providing poor to very poor support, impervious drainage, and a high frost potential in the context of subgrade for roads.

In consideration of the soil types described, the results of the drilling investigation, and the results of the geotechnical laboratory testing program, a subgrade modulus of 28 MPa was selected for the native sub-grade and subsequently used in this assessment.

6.2.3 Drainage

Most of the municipal roads on the island do not have adequate drainage.

The lack of drainage will result in deterioration of the existing roads under the heavy haul traffic.

6.3 FORECASTED CONSTRUCTION TRAFFIC

The loading and truck configuration for each turbine component including the transformers was reviewed, and the Equivalent Single Axle Loadings (ESALs) for construction deliveries, including concrete and aggregates, were estimated.



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The total traffic loadings were estimated and the traffic was subsequently proportioned based on the number of turbine sites accessed via the specific municipal road being assessed.

6.4 ROAD DESCRIPTION & TRAFFIC ASSESSMENT

6.4.1 Front Road

It is understood that the portion of Front Road from the new island dock to the access road for Turbine S30 will be used for the transport of turbine components for four Turbines (S13, S18, S26 and S30). It is not intended for use by other heavy vehicle loads which will use an alternative route.

The road has an asphalt surface on approximately 25% of the length, a chip seal surface on approximately 50% of the length and a gravel surface on approximately 25% of the length (this last may in fact have been a former chip seal surface that has deteriorated to the current state).

Comments regarding this road are as follows:

- Construction traffic was estimated to be 1,000 ESALs.
- The existing structure is either chip seal asphalt with 140 mm to 225 mm of granular or 180 mm to 250 mm of granular, over sandy clay subgrade.
- The assessment indicated that the existing road structure is suitable for 1,000 ESALs; and,
- Based on the results of the assessment no improvements are anticipated to be required for this road.

6.4.2 Stella 40 Foot Road

Stella 40 Foot Road was reviewed with consideration for the initial portion of the road from 2nd Concession Road to 3rd Concession Road and from just beyond 3rd Concession Road to the access entrance road to Turbine S37. Comments are as follows:

- The construction traffic on the north end of the road between 2nd Concession Road and 3rd Concession Road was estimated to be 15,000 ESALs. The construction traffic on the south end of the road from beyond 3rd Concession Road was estimated to be 13,000 ESALs.
- The existing structure has:
 - 40 mm to 50 mm of asphalt for approximately 60% of the road length (The asphalt is severely distressed, likely due to the lack of roadside drainage); and,
 - 200 mm granular over sandy clay subgrade for approximately 40% of the road length.
- The assessment indicated that the existing road structure is suitable for 2,000 ESALs based on the rutting criteria.
- Based on the results of the assessment, the improvements specified in Section 6.5.1 and Section 6.5.2 below are recommended for the respective gravel surface and asphalt surface segments of this road.



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6.4.3 2nd Concession Road

The portion of 2nd Concession Road from the intended access to the layover area extending east to the access entrance road to Turbine S01 was reviewed. Comments are as follows:

- The construction traffic at the east end of the road was estimated to be 9,000 ESALs. The construction traffic beyond the access road to Turbine S22 to the west was estimated to be 4,000 ESALs.
- The existing structure consists of 150 mm granular material over the sandy clay subgrade.
- The assessment indicated that the existing road structure is suitable for less than 1,000 ESALs based on the rutting criteria.
- Based on the results of the assessment, the improvements specified in Section 6.5.1 below are recommended for this road.

6.4.4 3rd Concession Road

The section of 3rd Concession Road from Stella 40 Foot Road to the construction access to Turbine S11 was reviewed. Comments are as follows:

- Construction traffic was estimated to be 3,500 ESALs.
- The existing structure consists of 180 mm granular material over sandy clay subgrade.
- The assessment indicated that the existing road structure is suitable for 1,000 ESALs based on the rutting criteria.
- Based on the results of the assessment, the improvements specified in Section 6.5.1 below are recommended for this road.

6.4.5 South Shore Road

This section of South Shore Road extends from the access road to Turbine S02 to the access road to Turbine S33. Comments regarding this section are as follows:

- The construction traffic at the west end of this road segment was estimated to be 8,000 ESALs. The construction traffic towards the east beyond the access road to Turbine \$14 was estimated to be 6,000 ESALs.
- The existing structure consists of 150 mm granular material over sandy clay subgrade.
- The assessment indicated that the existing road structure is suitable for less than 2,500 ESALs based on the PSI and rutting criteria.
- Based on the results of the assessment, the improvements specified in Section 6.5.1 below are recommended for this road.

6.4.6 Lower 40 Foot Road

This section of road includes the portion of South Shore Road from the access to Turbine S33 to the corner with Lower 40 Foot Road, the entire length of Lower 40 Foot Road, and the portion of Front Road from the corner with Lower 40 Foot Road to the access to Turbine S30 on Front Road. It is noted that construction traffic along this road will consist of aggregate trucks, miscellaneous



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materials/service trucks and concrete trucks but that the turbine delivery trucks will not use this route. Comments regarding this section are as follows:

- Construction traffic was estimated to be 3,500 ESALs.
- The existing pavement is 200mm granular over sandy clay subgrade.
- The assessment indicated that the existing road structure is suitable for less than 1,300 ESALs based on the rutting criteria.
- Based on the results of the assessment, the improvements specified in Section 6.5.1 below are recommended for this road.

6.5 UPGRADES TO EXISTING ROADS

6.5.1 Gravel Surface Roads

As a component of the pre-construction activity the roads with gravel surfaces will be upgraded through the following:

- Sub-excavate the upper 200 mm of existing road base materials;
- Place a Terrafix Combigrid 30/30 or equivalent; and,
- Place and compact 200 mm of OPSS Granular A.

The Combigrid will extend from one road edge to within 0.5 m of the opposite road edge. The 0.5 m gap will provide open access for the placement of the collection circuit within the road platform without the need to cut the geogrid. The side of the road accommodating the gap will vary in accordance with the collection system installation drawings, as trenching location will vary across the project.

To reiterate from a preceding section, it is understood that the portion of Front Road from the project docks to the access road for Turbine S30 will be used for the transport of turbine components for four Turbines (S13, S18, S26 and S30). It is not intended for use by other heavy vehicle loads. The assessment indicates that due to the limited traffic loading, no improvements are anticipated to be required to the gravel surface segment of this road.

As a component of the pre-construction activity, the gravel roads will be provided with a proper center crown meeting the municipal standards and a minimum functional road width of 6.0 m. Where the current granular surface is less than 6.0 m in width the existing "shoulder" material will be sub-excavated to a depth of 100 mm and replaced with compacted Granular A. The sub-excavation and replacement with 100 mm of Granular A where applied will strengthen the existing shoulder and provide for temporary passing of vehicles if and as required.

Two exceptions to the 6.0 m functional road width will occur on South Shore Road where restoration will occur within the existing widths except where temporary widening takes place in specific areas and Dump Road where the planned width is 5.0 m.

The gravel roads will be monitored and maintained/restored as necessary throughout the construction period to support the construction traffic. This approach is consistent with the current general practice for maintenance of aggregate-surface municipal roads during construction traffic loading.



Municipal Road Assessment August 29, 2017

6.5.2 Asphalt Surface Roads

As stated in a preceding section, approximately 60% of the length of Stella 40 Foot Road has a severely distressed asphalt travel-surface. The recommended treatment specific to this road segment would be either of the following:

- Undertake continual monitoring, maintenance, repairs, and upgrades, as necessary throughout the construction period to maintain the road in a suitable condition for the support of the heavy construction traffic; or,
- Upgrade by:
 - Removing the upper 200 mm of asphalt and granular materials;
 - o Placing a Terrafix Combigrid 30/30 or equivalent; and,
 - o Placing and compacting 200 mm of OPSS Granular A.

To reiterate from a preceding section, it is understood that the portion of Front Road from the project docks to the access road for Turbine S30 will be used for the transport of turbine components for four Turbines (S13, S18, S26 and S30). It is not intended for use by other heavy vehicle loads. The assessment indicates that due to the limited traffic loading, no improvements are anticipated to be required to the asphalt segment of this road.

6.5.3 Seasonal Effects of Construction Traffic

It is noted that: heavy loads hauled when the roads are frozen will have little impact on the road condition; heavy loads hauled in the spring thaw period will have a significant impact on the road condition; and, heavy loads hauled in the summer and fall period (when dryer conditions are presumed to prevail) will have less impact on the road condition but will deteriorate the road surface with cumulative passes.

6.5.4 Upgraded Road Drainage

As noted, most of the municipal roads on the island do not have adequate drainage in their current state. The predominant subgrade type underlying the existing roadways consists of sandy clay, clay with sand and silty clayey sand. These soil types are generally characterized as providing limited permeability but will permit longer-term infiltration suitable for the purposes of this project.

The provision of a defined crown or transverse slope and a properly compacted Granular A surface as a component of the upgrades to the existing roads will increase the surface runoff relative to the existing conditions, reduce percolation through the granular surface and in this respect, improve overall drainage. The provision of a crown or transverse slope at subgrade elevation will direct any percolation that does occur to the edges of the roadway, further improving overall drainage of the road system.

During pre-construction activity where the exposed subgrade and road geometry will likely limit subgrade drainage, improvements can be made by installing occasional minor drainage



Municipal Road Assessment August 29, 2017

channels to provide a positive outlet to any existing ditches. The channels would be filled with granular material as a component of the road upgrade.

6.6 CONSTRUCTION OF NEW ROADS

6.6.1 Dump Road

Based on visual observations and the conditions encountered in the boreholes, Dump Road does not have an existing granular structure or travel surface, although minor gravel was present at the intersection with 2nd Concession Road. There may also have been placement of granular material at low spots in the roadway or where standing water accumulated, though these areas were most certainly localized.

The assessment of Dump Road considered construction extending from 2nd Concession to the location of Turbine S31. Comments regarding this road are as follows:

- Construction traffic was estimated to be 1,000 ESALs.
- The existing roadway has no granular surface of any significance.
- The subgrade consists of sandy clay.

In the absence of an existing road structure, this road is not considered suitable to support heavy construction traffic. It is therefore recommended that Dump Road be upgraded as follows:

- Compact and proof-roll the exposed subgrade/road surface.
- Place Terrafix Combigrid 30/30 or approved equivalent.
- Place and compact 300 mm of OPSS Granular A.

6.6.2 Temporary Turning Alignments at Existing Intersections

It is understood that there are two locations on the municipal roads where temporary turning alignments will be required to permit turning for 'longer' delivery vehicles.

Construction of these turning alignments should be as follows. Any existing vegetation and organics (including topsoil) should be stripped and stockpiled for reinstatement on completion of the construction of the overall project. The turning alignments can be constructed by placing a Terrafix Combigrid 30/30 or equivalent and placing OPSS Granular A material to the design grades. The thickness of the required granular material will be dependent on the specific topography and grades at the turning location and the thickness of any existing vegetation and organics (including topsoil). It is recommended that the thickness of the granular be not less than 300 mm in any case. The granular material should be placed in loose lifts having a maximum thickness of 200 mm and each lift uniformly compacted to achieve 100% of the material's Standard Proctor Maximum Dry Density.



Closure August 29, 2017

7.0 CLOSURE

We trust that this is satisfactory for your present purposes. If you have any questions, please contact the undersigned at your convenience.

STANTEC CONSULTING LTD.

Original Signed by

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APPENDICES

Appendix A August 29, 2017

Appendix A

A.1 STATEMENT OF GENERAL CONDITIONS



STATEMENT OF GENERAL CONDITIONS

<u>USE OF THIS REPORT</u>: This report has been prepared for the sole benefit of the Client or its agent and may not be used by any third party without the express written consent of Stantec Consulting Ltd. and the Client. Any use which a third party makes of this report is the responsibility of such third party.

<u>BASIS OF THE REPORT</u>: The information, opinions, and/or recommendations made in this report are in accordance with Stantec Consulting Ltd.'s present understanding of the site specific project as described by the Client. The applicability of these is restricted to the site conditions encountered at the time of the investigation or study. If the proposed site specific project differs or is modified from what is described in this report or if the site conditions are altered, this report is no longer valid unless Stantec Consulting Ltd. is requested by the Client to review and revise the report to reflect the differing or modified project specifics and/or the altered site conditions.

<u>STANDARD OF CARE</u>: Preparation of this report, and all associated work, was carried out in accordance with the normally accepted standard of care in the state or province of execution for the specific professional service provided to the Client. No other warranty is made.

<u>INTERPRETATION OF SITE CONDITIONS</u>: Soil, rock, or other material descriptions, and statements regarding their condition, made in this report are based on site conditions encountered by Stantec Consulting Ltd. at the time of the work and at the specific testing and/or sampling locations. Classifications and statements of condition have been made in accordance with normally accepted practices which are judgmental in nature; no specific description should be considered exact, but rather reflective of the anticipated material behavior. Extrapolation of in situ conditions can only be made to some limited extent beyond the sampling or test points. The extent depends on variability of the soil, rock and groundwater conditions as influenced by geological processes, construction activity, and site use.

<u>VARYING OR UNEXPECTED CONDITIONS</u>: Should any site or subsurface conditions be encountered that are different from those described in this report or encountered at the test locations, Stantec Consulting Ltd. must be notified immediately to assess if the varying or unexpected conditions are substantial and if reassessments of the report conclusions or recommendations are required. Stantec Consulting Ltd. will not be responsible to any party for damages incurred as a result of failing to notify Stantec Consulting Ltd. that differing site or subsurface conditions are present upon becoming aware of such conditions.

<u>PLANNING, DESIGN, OR CONSTRUCTION</u>: Development or design plans and specifications should be reviewed by Stantec Consulting Ltd., sufficiently ahead of initiating the next project stage (property acquisition, tender, construction, etc), to confirm that this report completely addresses the elaborated project specifics and that the contents of this report have been properly interpreted. Specialty quality assurance services (field observations and testing) during construction are a necessary part of the evaluation of sub-subsurface conditions and site preparation works. Site work relating to the recommendations included in this report should only be carried out in the presence of a qualified geotechnical engineer; Stantec Consulting Ltd. cannot be responsible for site work carried out without being present.



Appendix B August 29, 2017

Appendix B

B.1 BOREHOLE LOCATION PLAN





EHIIG-17	<image/> <section-header><text><text><text><text><text><text></text></text></text></text></text></text></section-header>
EHIC-19 EHIC-19 EHIC-20 EHIC-20	Legend WTG Number Borehole Locations Paved Roads (4) [BH16-01, BH16-03 - BH16-05]
Borehole ID Easting Northing BH16-01 363584 4891992 BH16-03 364801 4890764 BH16-04 364991 4892705 BH16-05 365557 4893017	* BH16-02, BH16-09, BH16-33 and BH16-37 were deleted from the investigation program and are not shown on this plan.
BH16-06 366577 4893258 BH16-07 365275 4890012 BH16-08 366766 4893377 BH16-10 368273 4894009 BH16-11 364325 4891151 BH16-12 363380 4890714 BH16-13 364532 4890157 BH16-14 364075 4889348	Revision By Appd. YY.MM.DD.
BH16-15 363353 4888535 BH16-16 363061 4888219 BH16-17 369249 4893832 BH16-18 369591 4893250 BH16-19 369925 4892730 BH16-20 369461 4892031 BH16-21 368700 4891574 BH16-22 367572 4890726 BH16-23 362534 4890279	File Name:
BH16-24 361528 489772 BH16-25 360291 4889151 BH16-26 362718 4890675 BH16-27 362502 4891030 BH16-28 359675 4888873 BH16-29 361975 4886754 BH16-30 363194 4891040 BH16-31 364094 4891040	Client/Project Windlectric Inc. AMHERST ISLAND WIND PROJECT 75MW WIND FARM Amherst Island, Loyalist Township, Ontario
BH16-323649484890415BH16-343700254892444BH16-353654464889758BH16-363671314893279BH16-383645974891118	MUNICIPAL ROADS INVESTIGATION PROGRAM Project No. Scale 133560104 150.000 Drawing No. Sheet 1 1 of 1

Appendix C August 29, 2017

Appendix C

C.1 BOREHOLE SUMMARY



C	s	tantec	B	OR	REF N: 4	IOI 891 9	LE 92 1	RE (E: 363	C OR 584	D]	16	-01	[Sł	neet 1 of 1
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-		trace gravelmoist to wet			3 -	M		280	50/											
1 -		- moist to wet				ss	2	$\frac{380}{460}$	50/ 89											-
-			/		4 -	Π														
-			•	-																
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-		inferred bedrock approximately 1.4 m below existing grade.			5															
-		in below existing grade.																		
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-		CLAY (CH) with sand - trace gravel (decreasing with depth)	· · · · · ·		2 -								· · · · · · · · · · · · · · · · · · ·				· · · · · · · · · · · · · · · · · · ·								
- 1 -		 moist increased moisture at bottom of hole 			3 -	SS	2	$\frac{460}{610}$	12		•														
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-		BOREHOLE TERMINATED on			7																				
-		inferred bedrock approximately 2.1 m below existing grade.			8 -								· · · · · · · · · · · · · · · · · · ·				· · · · · · · · · · · · · · · · · · ·								
-		Borehole caved to 0.7 m below grade on completion of drilling.			9 -								· · · · · · · · · · · · · · · · · · ·				· · · · · · · · · · · · · · · · · · ·								
3 -		Borehole dry on completion of drilling			10-																				
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-		- trace gravel - moist			2 -			410	50/	
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2		BOREHOLE TERMINATED on inferred bedrock approximately 1.4 m below existing grade. Borehole open and dry on completion of drilling.			5 - 6 - 7 - 8 - 9 -					
4					10- 11- 12- 13- 14- 15- 16-					
										 □ Field Vane Test, kPa □ Remoulded Vane Test, kPa △ Pocket Penetrometer Test, kPa

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	LIENT _	Pennecon Heavy Civil Limite — Front Road East, Amherst Isl		ON						PROJECT No133560104 DATUM
DA	ATES: B	ORING November 17, 2016				WAT	ER I	LEVEL		TPC ELEVATION
Ê	N		-OT	VEL	ft)		SAI	MPLES		UNDRAINED SHEAR STRENGTH (kPa) 50 100 150 200
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		Paved Road						TCF	0	10 20 30 40 50 60 70 80 90 100 (%) GR SA SI C
0 -		25 mm ASPHALT 225 mm Silty SAND with gravel - geotextile at 0.01 m Stiff, brown sandy CLAY (CL) - trace gravel			-0 1 - 2 -	SS	1	<u>410</u> 610	10	
-		- moist BOREHOLE TERMINATED on								
1 -		inferred bedrock approximately 0.8 m below existing grade.			3 -					
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5 -			<u> </u>				<u> </u>			 Field Vane Test, kPa □ Remoulded Vane Test, kPa △ Pocket Penetrometer Test, kPa

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	LIENT _ DCATIO			ON						PROJECT No133560104
DA	ATES: B	ORING November 17, 2016				WAT	ER I	LEVEL		TPC ELEVATION
(۲	Z		-OT	VEL	ft)		SAI	MPLES		UNDRAINED SHEAR STRENGTH (kPa) 50 100 150 200
DEPTH (m)	ELEVATION (m)	STRATA DESCRIPTION	STRATA PLOT	WATER LEVEL	DEPTH (ft)	ТҮРЕ	NUMBER	RECOVERY (mm) TCR(%) / SCR(%)	N-VALUE OR RQD(%)	
0		Gravel Road						TCF	0	10 20 30 40 50 60 70 80 90 100 (%) (%) GR SA SI C
0		190 mm Silty SAND with gravel Dense, brown silty, clayey SAND (SC-SM) - trace gravel - moist			-0 1 - 2 -	SS	1	<u>510</u> 610	46	Ö
1 -		BOREHOLE TERMINATED on inferred bedrock approximately 0.8 m below existing grade. Borehole open and dry on completion of drilling.	<u>· / / .</u>		3 - 4 - 5 -					
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5 -					16-					 □ Field Vane Test, kPa □ Remoulded Vane Test, kPa △ Pocket Penetrometer Test, kPa

C	S	tantec	16-07	Sheet 1 of 1													
CLIENT Pennecon Heavy Civil Limited LOCATION Stella 40 Foot Road, Amherst Island, ON											PROJECT No	133560104					
		ORING <u>November 17, 2016</u>		,		WAT	ER I	LEVEL			TPC ELEVATION .						
			F				SA	MPLES		UNDRAIN	NED SHEAR STRENGTH (kP	a)					
DEPTH (m)	ELEVATION (m)	STRATA DESCRIPTION	STRATA PLOT	WATER LEVEL	DEPTH (ft)	ТҮРЕ	NUMBER	RECOVERY (mm) TCR(%) / SCR(%)	N-VALUE OR RQD(%)	DYNAMIC CON	100 150						
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-		180 mm Silty SAND with gravel Stiff to very stiff, brown CLAY (CH) with sand - trace gravel - moist			1 - 2 -	SS	1	<u>280</u> 610	13	Ó.		32 47 21					
					3 - 4 -	ss	2	<u>510</u> 610	17		фн	2 19 33 46					
- - - - - - - - - - - - - - - - - - -					5 - 6 - 7 -	SS	3	<u>610</u> 610	23	•							
		- wet 6" sand seam at 2.4 m Stiff, brown sandy CLAY (CL) - trace gravel - moist to wet			8 - 9 -	ss	4	<u>530</u> 610	20	•							
3 -		Stiff to hard, brown CLAY (CH) with sand - trace gravel - moist			10 - 11 -	ss	5	<u>380</u> 460	50/ 130								
4 -		BOREHOLE TERMINATED on inferred bedrock approximately 3.5 m below existing grade. Borehole open to 2.9 m on			12 - 13 -												
-		completion of drilling, Borehole dry on completion of drilling.			14- 15-												
5 -					16-												
										Remoul	ane Test, kPa ded Vane Test, kPa Penetrometer Test, kPa						

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(z		OT	ΈL				UN			ED S			ST	RE	NGT			200)						
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0 -		250 mm Silty SAND with gravel Dense to very dense, brown silty, clayey SAND (SC-SM) - trace gravel - dry to moist			0 1 - 2 -	ss	1	<u>530</u> 610	20	Q		•											37			
- 1 -		- light brown			3 -	ss	2	<u>610</u> 610	66	-	0 I	-1						•					5	49 32		
					4 -	X SS	3	<u>100</u> 91	<u>50/</u>													**	-			
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D	ATES: E	ORING November 17, 2016				WAT	TER I	LEVEL								TF	PC I	ELF	EVA	TIO	Ν_					
m)	NO		LOT	NEL	(ft)		SAMPLES						AINE 50	ED S		AR 100		RE	NG 15		(kPa		00			
DEPTH (m)	ELEVATION (m)	STRATA DESCRIPTION	STRATA PLOT	WATER LEVEL	DEPTH (ft)	ТҮРЕ	NUMBER	RECOVERY (mm) TCR(%) / SCR(%)	N-VALUE OR RQD(%)	DY	'nam	IIC C	ONE	PEN	ATTERBERG LIMITS H & ATTERBERG LIMITS H ENETRATION TEST, BLOWS/0.3m (RATION TEST, BLOWS/0.3m						È.	-0-	▼ REMARK & GRAIN SI			
0 -		Gravel Road			0			TCF	0		10	20	30	0 4	40	50	60	0 '	70	80	90) 1			3UTION 6) <u>SIC</u>	
U		200 mm Silty SAND with gravel Dense to very dense, light brown silty, clayey SAND (SC-SM) - trace gravel - dry				ss	1	<u>200</u> 610	24	Ö			•										I I	9 48	23	
		- increasing silt with depth			3 -	ss	2	<u>610</u> 610	42	Ō	E-I				•								5	55	26 1-	
-		BOREHOLE TERMINATED on			5 -	ss	3	<u>200</u> 200	50/ 51													>>>				
2 -		inferred bedrock approximately 1.7 m below existing grade. Borehole open and dry on			6 -																		· · · · · · · · · · · · · · · · · · ·			
		completion of drilling.			8 -																		L			
3 -					10-																					
					11 -																					
4 -					13-	-																				
					14- 15-																					
5 -					16-																					
											R	emo	Var ould et Pe	ed V	ane	Test			Pa							

C	s	tantec	B		REH N: 48	IOI 891 1	LE 51 1	RE(E: 364	C OR 325	D	16-11	Sheet 1 of 1
	LIENT _	Pennecon Heavy Civil Limit									PROJECT No.	133560104
		N <u>2nd Concession Road, Amber</u> ORING <u>November 16, 2016</u>						LEVEL			_ DATUM	
	ATES: E	ORING INOVERIDEI 10, 2010				WAI					_ TPC ELEVATION	
ε Ξ	NO		LOT	NEL	(H)		SAI	MPLES ⊺ ିଚ୍ଚ		50	100 150	200
DEPTH (m)	ELEVATION (m)	STRATA DESCRIPTION	STRATA PLOT	WATER LEVEL	DEPTH (ft)	ТҮРЕ	NUMBER	RECOVERY (mm) TCR(%) / SCR(%)	N-VALUE OR RQD(%)		TERBERG LIMITS H TRATION TEST, BLOWS/0.3m	W W _L REMARKS & GRAIN SIZE DISTRIBUTION
0		Gravel Road			0			TCF	0	10 20 30 40	50 60 70 80 9	0 100 GR SA SI CI
0 -		150 mm SAND and GRAVEL			0							
		Stiff, brown sandy CLAY (CL) - trace gravel - dry to moist			1 -	SS	1	<u>480</u> 610	15	•		
- 1 -		Compact to dense, brown clayey SAND (SC) - trace gravel			3 -	SS	2	530	15			
-		- moist to wet (increasing moisture with depth)			4 -	55		<u>530</u> 610	15			
		- gravel seam (3")			5 -	SS	3	$\frac{300}{610}$	39	•		
2 -					7 -							
					8 - 9 -	SS	4	$\frac{250}{610}$	21	•		
3 -			, , , , , , , , , , , , , , , , , , ,		10-							
			, , , , , , , , , , , , , , , , , , ,		11- - 12 -	SS	5	$\frac{410}{610}$	27			
- 4 -		BOREHOLE TERMINATED at approximately 3.7 m below grade. Borehole open and dry on			13-							
-		completion.			14-							
					15-							
5 -												
										 □ Field Vane Test □ Remoulded Van △ Pocket Penetror 	ne Test, kPa	

C	S	tantec	B	OR N	EH N: 48	OI 390 7	E 14 I	RE E: 363	C OR 380	CD 16-12 Sheet 1 of 1
	LIENT _ DCATIO	Pennecon Heavy Civil Limite 2nd Concession Road, Amhe		slanc	I, ON	[PROJECT No133560104
D	ATES: B	ORING November 16, 2016				WAT	ER I	LEVEL		TPC ELEVATION
ц)	N		-OT	VEL	ť)		SAI	MPLES		UNDRAINED SHEAR STRENGTH (kPa) 50 100 150 200
DEPTH (m)	ELEVATION (m)	STRATA DESCRIPTION	STRATA PLOT	WATER LEVEL	DEPTH (ft)	ТҮРЕ	NUMBER	RECOVERY (mm) TCR(%) / SCR(%)	N-VALUE OR RQD(%)	WP W WL WATER CONTENT & ATTERBERG LIMITS → DYNAMIC CONE PENETRATION TEST, BLOWS/0.3m STANDARD RENETRATION TEST, BLOWS/0.3m GRAIN SIZ
•		Gravel Road			•			TCR	-0	10 20 30 40 50 60 70 80 90 100 GR SA SI
0 -		150 mm Silty SAND with gravel Firm to very stiff, brown sandy CLAY (CL)			- 0 1 -	SS	1	<u>410</u> 610	10	Ø: 29 49 2 • • • • •
		- trace gravel - moist			2 -					
1 -					3 - 4 -	SS	2	<u>560</u> 610	20	
					5 -					
2 -		Compact to very dense, brown to grey clayey SAND (SC) - trace gravel - moist to wet			6 - 7 -	SS	3	<u>560</u> 610	23	
		- auger grinding			8 -	SS	4	<u>360</u> 610	64	
		- auger grinding (corresponds to rock in spoon)	· · · · ·		9 - - 10 -					
		BOREHOLE TERMINATED on inferred bedrock approximately 3.1 m below grade.			11-					
		Borehole caved to approximately 2.9 m below grade. Borehole dry on completion of drilling.			12-					
4 -					13- 14-					
					15-					
5 -					16-					
										 □ Field Vane Test, kPa □ Remoulded Vane Test, kPa △ Pocket Penetrometer Test, kPa

C	S	tantec	B		EH N: 43	IOI 890 1	LE 57 I	RE(E: 364	C OR 532	D						1	6	-13	3			Sh	eet 1 o	f 1
	LIENT _	Pennecon Heavy Civil Limite N3rd Concession Road, Amher		land													ОЛ АТЦ		No			133	35601	<u>04</u>
		BORING November 16, 2016					ER I	LEVEL											VAT	ION				
							SAI	MPLES			JND	RA	INE	DS										
DEPTH (m)	ELEVATION (m)	STRATA DESCRIPTION	STRATA PLOT	WATER LEVEL	DEPTH (ft)	түре	NUMBER	RECOVERY (mm) TCR(%) / SCR(%)	N-VALUE OR RQD(%)		TER (CON			ATTE					₩ _P		200		
			ί Ο	3			NZ	COV R(%	N-V N F	ST	ANDA	RD I	PENE	ETRA	TION	I TES	ST, B	BLOW	/S/0.3	Im		•	8 GRAIN DISTRIE	I SIZE BUTIO
0 -		Gravel Road	/ 9 - 19		0-			л П С			10 2	20	30	. 4	0	50	60	7	0 8	30	90	100	(0.	5
-		250 mm Silty SAND with gravel Dense, grey to brown silty, clayey	20		1 -	SS	1	$\frac{480}{610}$	31	a													39 39	22
-		SAND (SC-SM) - trace gravel - dry to moist		•	2 -			010																
- - 1 -		Stiff to very stiff, brown CLAY (CH) with sand - trace gravel	· / ·		3 -			460																
-		- moist	, , , , , , , , , , , , , , , , , , ,		4 -	SS	2	<u>460</u> 610	13															
-					5 -																			
- - 2 -		Dense, grey to brown silty, clayey	· · · ·	•	6 -	ss	3	<u>530</u> 610	18															
-		SAND (SC-SM) - trace gravel - moist		•	7 -																			
-		- auger grinding (minimal recovery in spoon)			8 -	SS	4	$\frac{51}{610}$	50/ 51												>	, l		
-		Dense, grey clayey SAND (SC)			9 -																			
3 -		- trace gravel - wet		•	10-			5.00																
-		Dense, grey to brown silty, clayey SAND (SC-SM) - trace gravel				SS	5	$\frac{560}{610}$	47															
-		- dry - possible bedrock fragment BOREHOLE TERMINATED at			12																			
4 -		approximately 3.7 m below existing grade.			13-																			
-		Borehole open and dry on completion of drilling.			14																			
-					16-																			
5 -					1						i:::: Fie	eld '	∷∐ Vane	e Te	st, k	Pa	::E			1:::	:1:::	::!		
											Re	mo	ulde	d V	ane	Test								
										Δ	Ро	cke	t Pe	netr	omet	ter T	[est	, kPa	a					

C	s	tantec	B	OR	EH N: 48	OI 389 3	LE 48 1	RE E: 364	C OR 075	RD 16-14 Sheet 1 of 1
-	LIENT _ CATIO	Pennecon Heavy Civil Limite N3rd Concession Road, Amhe		sland	. ON					PROJECT No133560104
		ORING November 16, 2016						LEVEL		TPC ELEVATION
							SA	MPLES		UNDRAINED SHEAR STRENGTH (kPa)
DEPTH (m)	EVATION (m)	STRATA DESCRIPTION	STRATA PLOT	WATER LEVEL	DEPTH (ft)					- 50 100 150 200 $+ + + + + + + + + + + + + + + + + + +$
DE	ELE		STRA	WATE	DE	ТҮРЕ	NUMBER	RECOVERY (mm) TCR(%) / SCR(%)	N-VALUE OR RQD(%)	DYNAMIC CONE PENETRATION TEST, BLOWS/0.3m V STANDARD PENETRATION TEST, BLOWS/0.3m O GRAIN SIZ DISTRIBUTION
0 -		Gravel Road			_0_			Ч Ц С Ц С		10 20 30 40 50 60 70 80 90 100 ^(%) GR SA SI
-		280 mm Silty SAND with gravel Stiff to hard, brown CLAY (CH) with sand - trace gravel			1 - 2 -	SS	1	<u>430</u> 610	46	
		- moist to wet (increasing moisture with depth)			3 - 4 -	SS	2	<u>410</u> 610	14	
					5 - 6 -	SS	3	<u>510</u> 610	10	
		- grey Very dense, brown to grey clayey SAND (SC) - trace to some gravel			7 - 8 -	SS	4	<u>560</u> 610	89	
3 -		- dry to slightly moist			9 - 10-			610		
-		BOREHOLE TERMINATED on	//		-11-	ss	5	$\frac{230}{300}$	50/ 130	
-		inferred bedrock at approximately 3.4 m below existing grade. Borehole open and dry on			12-					
4 -		completion of drilling.			13 - 14 -					
5 -					15- 16-					
5 -										 □ Field Vane Test, kPa ■ Remoulded Vane Test, kPa △ Pocket Penetrometer Test, kPa

C	s	tantec	B	OR N	EH N: 48	IOI 888 5	LE 35 I	RE E: 363	C OR 353	CD 16-15 Sheet 1 of 5
-	LIENT _ DCATIO	Pennecon Heavy Civil Limit		sland	, ON					PROJECT No133560104
		BORING November 16, 2016					TER I	LEVEL		TPC ELEVATION
			F				SAI	MPLES		UNDRAINED SHEAR STRENGTH (kPa)
DEPTH (m)	ELEVATION (m)	STRATA DESCRIPTION	STRATA PLOT	WATER LEVEL	DEPTH (ft)	ТҮРЕ	NUMBER	RECOVERY (mm) TCR(%) / SCR(%)	N-VALUE OR RQD(%)	- 50 100 150 200 WATER CONTENT & ATTERBERG LIMITS → H DYNAMIC CONE PENETRATION TEST, BLOWS/0.3m → REMARK STANDARD PENETRATION TEST, BLOWS/0.3m → GRAIN SI
				-			ž	CR(9	Υ ^N	DISTRIBUT
0 -		Gravel Road 250 mm SAND and GRAVEL			0					10 20 30 40 50 60 70 80 90 100 GR SA SI
		Stiff to hard, brown to grey CLAY (CH) with sand - trace gravel - moist to wet			1 - 2 -	ss	1	<u>250</u> 610	20	
1 -					3 -	SS	2	<u>510</u> 610	13	
					4 -			610		
		 300 m wet layer 25 mm gravel seam			5 - 6 -	SS	3	$\frac{460}{610}$	26	
2 -			, , , , , , ,		7 -					
		Very dense, grey silty, clayey SAND (SC-SM) - trace to some gravel - dry to slightly moist		• < • • < •	8 - 9 -	SS	4	<u>560</u> 610	73	
3 -					10 - 11 -	ss	5	$\frac{430}{460}$	50/ 150	
		BOREHOLE TERMINATED on inferred bedrock at approximately 3.5 m below existing grade.			12-					
4 -		Borehole open and dry on completion of drilling.			13 - 14 -					
					15- 16-	,				
5 -				<u> </u>	10-					□ Field Vane Test, kPa
										 Remoulded Vane Test, kPa Pocket Penetrometer Test, kPa

\overline{C}	S	tantec	B	OR	EH N: 48	IOI 888 2	LE 19 I	RE(E: 363	COR 061	D 16-16 Sheet 1 of 1
-	LIENT _	Pennecon Heavy Civil Limite 3rd Concession Road, Amher	ed							PROJECT No133560104 DATUM
		ORING November 16, 2016					TER I	LEVEL		DATOM TPC ELEVATION
							SAI	MPLES		UNDRAINED SHEAR STRENGTH (kPa)
DEPTH (m)	ELEVATION (m)	STRATA DESCRIPTION	STRATA PLOT	WATER LEVEL	DEPTH (ft)	ТҮРЕ	NUMBER	RECOVERY (mm) TCR(%) / SCR(%)	N-VALUE OR RQD(%)	50 100 150 200 WATER CONTENT & ATTERBERG LIMITS Wp W WL DYNAMIC CONE PENETRATION TEST, BLOWS/0.3m ▼ REMARKS STANDARD PENETRATION TEST, BLOWS/0.3m ● GRAIN SIZ
		Gravel Road						REC(R	29	10 20 30 40 50 60 70 80 90 100 (%) GR SA SI
0 -		300 mm Silty SAND with gravel Compact, bown silty, clayey SAND			- 0 - 1 -	SS	1	<u>360</u> 610	25	Q
-		(SC) - trace gravel - dry		•	2 -					
1 -		Stiff to very stiff, brown CLAY (CH) with sand - trace gravel - moist to wet		•	3 -	SS	2	<u>510</u> 610	20	• 0 2 26 38
-				•	- 5 -					
2 -		- 50 mm - 75 mm sand seam			6 -	SS	3	<u>480</u> 610	13	
-					7 -					
-		- grey			o - 9 -	SS	4	$\frac{610}{610}$	14	
3 -		Compact, brown to grey clayey SAND (SC)			10-					
-		- trace gravel - moist to wet				ss	5	$\frac{610}{610}$	12	•
- - 4 -		BOREHOLE TERMINATED at approximately 3.7 m below existing grade.			-12 - 13-					
-		Borehole open and dry on completion of drilling.			14-					
-					15- 16-					
5 -					10-					
										 Field Vane Test, kPa Remoulded Vane Test, kPa
										 △ Pocket Penetrometer Test, kPa

C	s	tantec	B	OR	REH N: 43	IOI 893 8	LE 32 B	RE(E: 369	C OR 249	D	16-17	Sheet 1 of 1
	LIENT _ DCATIO	Pennecon Heavy Civil Limite Lower 40 Foot Road, Amher		land,	, ON							133560104
DA	ATES: B	ORING November 17, 2016				WAT	TER I	LEVEL			_ TPC ELEVATION _	
(m	NO		LOT	:VEL	(#)		SAI	MPLES । ଚିତି		UNDRAINED SI	IEAR STRENGTH (kPa 100 150	a) 200
DEPTH (m)	ELEVATION (m)	STRATA DESCRIPTION	STRATA PLOT	WATER LEVEL	DEPTH (ft)	ТҮРЕ	NUMBER	RECOVERY (mm) TCR(%) / SCR(%)	N-VALUE OR RQD(%)		Wp	W W _L REMARKS & GRAIN SIZE GRAIN SIZE
•		Gravel Road				1		TCF	0	10 20 30 40	50 60 70 80 90	DISTRIBUTION (%) GR SA SI CL
0		200 mm Silty SAND with gravel Compact, brown clayey SAND (SC) - trace gravel - moist to dry			0 1 - 2 -	ss	1	<u>250</u> 610	12	•		
- - 1 -		BOREHOLE TERMINATED on inferred bedrock approximately 0.8 m below existing grade.			3 -							
-		Borehole caved to 0.7 m below grade on completion of drilling. Borehole dry on completion of drilling			4 -							
2 -					6 -							
-					8 - 9 -							
3 -					10-							
-					12-							
4 -					13 - 14 -							
-					15-							
5 -										 □ Field Vane Tes □ Remoulded Van △ Pocket Penetron 	ne Test, kPa	

C	S	tantec	B	OR	REF N: 4	IOI 893 2	LE 50 I	RE(E: 369	C OR 591	RD 16-18 Sheet 1 of 1
	LIENT _ CATIO	Pennecon Heavy Civil Limite Lower 40 Foot Road, Amher		land	, ON					PROJECT No133560104 DATUM
		ORING November 17, 2016					FER I	LEVEL		TPC ELEVATION
			F				SA	MPLES		UNDRAINED SHEAR STRENGTH (kPa)
DEPTH (m)	ELEVATION (m)	STRATA DESCRIPTION	STRATA PLOT	WATER LEVEL	DEPTH (ft)	ТҮРЕ	NUMBER	RECOVERY (mm) TCR(%) / SCR(%)	N-VALUE OR RQD(%)	→ 50 100 150 200 WP W WL WATER CONTENT & ATTERBERG LIMITS → T DYNAMIC CONE PENETRATION TEST, BLOWS/0.3m ▼ REMARKS & GRAIN SIZE DYNAMIC PENETRATION TEST, BLOWS/0.3m ▼ REMARKS
		Gravel Road						REC	20	10 20 30 40 50 60 70 80 90 100 (%) GR SA SI C
0		190 mm Silty SAND with gravel Compact to very dense, brown to grey clayey SAND (SC) - trace gravel - moist			0 1 - 2 -	ss	1	<u>380</u> 610	10	•
-		noist								
		DODELIOI E TEDL (B. 1 TED	<u> ^ · ·</u>		3	<u>ss</u>	2	$\frac{130}{200}$	50/ 51	
1		BOREHOLE TERMINATED on inferred bedrock approximately 0.9 m below existing grade. Borehole caved to 0.7 m below grade on completion of drilling. Borehole dry on completion of drilling			4 - 5 - 6 -					
- - - - - - -					7 - 8 - 9 -					
3 -					10 - 11 - 12 -					
- - 4 -					13-					
					14- 15- 16-					
5 -										 □ Field Vane Test, kPa □ Remoulded Vane Test, kPa △ Pocket Penetrometer Test, kPa

		tantec	B		EH N: 48	IOI 892 7	LE 30 I	RE(E: 369	C OR 925	D 16-19 Sheet 1 of 1
	LIENT	Pennecon Heavy Civil Limite Lower 40 Foot Road, Amher		land	ON					PROJECT No133560104
		ORING November 17, 2016					FER I	LEVEL		DATUM TPC ELEVATION
	TLS. L							MPLES		UNDRAINED SHEAR STRENGTH (kPa)
Ê	NO		2	NEI	(ft)					50 100 150 200
Ξ	EVATION (m)	STRATA DESCRIPTION	∠	S LE	TH		6	(mn (%)		Wp W WL
DEPTH (m)) EV		STRATA PLOT	WATER LEVEL	DEPTH (ft)	ТҮРЕ	BEI	/SC	ALUI 2D(WATER CONTENT & ATTERBERG LIMITS
	ELI		ST	M		≿	NUMBER	RECOVERY (mm) TCR(%) / SCR(%)	N-VALUE OR RQD(%)	STANDARD PENETRATION TEST BLOWS/0.3m
		Gravel Road						LCR CR CR	20	10 20 30 40 50 60 70 80 90 100 GR SA SI
0 -		190 mm Silty SAND with gravel	914		-0-					Ö
-			ЪЫ			N				
-		Compact, brown clayey SAND (SC) - trace gravel (decreasing content]	1 -	SS	1	$\frac{250}{610}$	11	
_		with depth)	·]		N				
-		- moist		1	2 -					
-				1		$\left \right $				
			.,/		3 -	M				
1 -						SS	2	$\frac{510}{610}$	23	
-					4 -	$\langle \rangle$		010		
						}				
-		BOREHOLE TERMINATED on	<u>.</u> /.		-5					
_		inferred bedrock approximately 1.5								
-		m below existing grade.			6 -					
2										
		Borehole open and dry on completion of drilling.			7 -					
		completion of arming.								
-					8 -					
_					Ū					
-					9 -					
-										
3 -					10					
-					10-					
-					11					
-					11-					
-										
-					12-					
4 -					13-					
-					14-					
_										
-					15-					
-										
-					16-					
5 -										□ Field Vane Test, kPa
										 Remoulded Vane Test, kPa Remoulded Vane Test, kPa
										$\triangle \text{Pocket Penetrometer Test, kPa}$

C	s	tantec	B		EH N: 43	IOI 892 0	LE 31 I	RE(E: 369	C OR 461	D					16	5-2	0		S	heet 1 of 1
LO	LIENT _ DCATIO			d, O											DAT	TUM				33560104
D	ATES: E	ORING November 17, 2016	1			WAT	ER I	LEVEL		í								ΓΙΟΝ		
(m)			PLOT	LEVEL	H (ft)			VPLES		U		RAIN 50	IED S		NR S 00	TRE	NG 15	ΓΗ (k 0	Pa) 	
DEPTH (m)	ELEVATION (m)	STRATA DESCRIPTION	STRATA PLOT	WATER LEVEL	DEPTH (ft)	ТҮРЕ	NUMBER	RECOVERY (mm) TCR(%) / SCR(%)	N-VALUE OR RQD(%)	DYN	IAMIC	CON	ENT & / E PEN NETR/	ETRAT	TION T	EST,	BLOV	₩ _P ⊢ VS/0.3i .3m	w m ▼	W _L REMARKS & GRAIN SIZE DISTRIBUTION
0 -		Gravel Road	-//• .14		0			RE(TCI	0	1	0 2	20	30 4	0 5	0 6	50	70	80	90 10	0 (%) GR SA SI CL
-		150 mm Silty SAND with gravel	<u>N</u> K		Ŭ	M														
-		Hard, brown CLAY (CH) with sand - trace gravel - slightly moist to moist			1 -	ss	1	$\frac{430}{610}$	49											
-		BOREHOLE TERMINATED on	//.		-2															
- - 1 -		inferred bedrock approximately 0.6 m below existing grade.			3 -															
1 -		Borehole caved to 0.5 m below																		
-		grade on completion of drilling. Borehole dry upon completion of			4 -															
-		drilling			5 -															
-					5															
-					6 -															
2 -																				-
-					7 -															
-					0															
-					8 -															_
-					9 -															
3 -					10-													<u>.</u>		-
-					10-															
-					11-															
-																				-
-					12-															
-																				
4 -					13-															_
-					14-															
-					1-1															
-					15-															-
					16-															
5 -				•	-								ine Te							
													ded V Penetr				Pa			
											r0	unce I	eneur	omete	лте	3ι, Κ	a			

C	s	tantec	B	OR	EH N: 48	IOI 891 5	JE 74 1	RE E: 368	C OR 700	D 16-21 Sheet 1 of 1
LC	LIENT _ DCATIO	N South Shore Road, Amherst I	Islan	,						PROJECT No133560104 DATUM
D	ATES: E	ORING November 17, 2016				WAT	ER I	LEVEL		TPC ELEVATION
m)	NO		LOT	VEL	(ft)		SAI	MPLES	;	UNDRAINED SHEAR STRENGTH (kPa) 50 100 150 200
DEPTH (m)	ELEVATION (m)	STRATA DESCRIPTION	STRATA PLOT	WATER LEVEL	DEPTH (ft)	ТҮРЕ	NUMBER	RECOVERY (mm) TCR(%) / SCR(%)	N-VALUE OR RQD(%)	WP W WL WATER CONTENT & ATTERBERG LIMITS → H DYNAMIC CONE PENETRATION TEST, BLOWS/0.3m STANDARD PENETRATION TEST, BLOWS/0.3m GRAIN SIZE DISTRIBUTION
0		Gravel Road						TCF	0	10 20 30 40 50 60 70 80 90 100 (%) (%) GR SA SI CL
0		250 mm Silty SAND with gravel Very stiff to hard, brown clayey SAND (SC) - trace gravel - moist to wet (increasing moisture			0 1 - 2 -	SS	1	<u>360</u> 610	19	Ö. 0.1 OA OF OL Homoson 46 41 13
- - 1 -		content with depth)			3 -	ss	2	$\frac{180}{460}$	50/ 150	2 53 21 24
2		BOREHOLE TERMINATED on inferred bedrock approximately 1.2 m below existing grade. Borehole caved to 0.8 m below grade on completion of drilling. Borehole dry on completion of drilling			5 - 6 - 7 - 8 - 9 -					
3					10 - 11 - 12 -					
4 -					13 - 14 - 15 -					
5 -					16-					 □ Field Vane Test, kPa □ Remoulded Vane Test, kPa △ Pocket Penetrometer Test, kPa

C	s	tantec	B	OR	EH N: 43	IOI 890 7	LE 26 I	RE(E: 367	C OR 572	D					16	5-2	2		Sh	eet 1 of 1
	LIENT _ DCATIO	Pennecon Heavy Civil Limite N South Shore Road, Amherst 1		d, 0											PRO DAT		T No		13	3560104
D	ATES: E	BORING November 16, 2016				WAT	TER I	LEVEL							TPC	ELE	EVAT	ION		
H (m)	TION (A PLOT	LEVEL	H (ft)			VPLES (%)		10	NDR +	50	ED S		NR S ⁻ 00	TRE	NGT 150	+	200	
DEPTH (m)	ELEVATION (m)	STRATA DESCRIPTION	STRATA PLOT	WATER LEVEL	DEPTH (ft)	ТҮРЕ	NUMBER	RECOVERY (mm) TCR(%) / SCR(%	N-VALUE OR RQD(%)	DYN/	AMIC	CONE		ETRAT	TION T	EST,	TS BLOW NS/0.3		W → n ▼	W _L
0 -		Gravel Road			0	1		TCR	-0										0 10	(0/)
- 0		100 mm SAND and GRAVEL			0	\mathbf{V}				0										32 45 23
		Very stiff, brown CLAY (CH) with sand - trace gravel - dry to moist			1 -	ss	1	<u>380</u> 610	16		•	· · · · · · · · · · · · · · · · · · ·								
-		- rock fragments at 0.5 m	//		2	\square						<u></u>								
- - 1 -		BOREHOLE TERMINATED on inferred bedrock approximately 0.6 m below existing grade.			3 -															-
		Borehole caved to 0.5 m below grade on completion of drilling. Borehole dry upon completion of drilling			4 - 5 -															
2 -					6 -														 	-
-					7 -															
					8 -															-
3 -					9 - 10-															
-					11-															
-					12 -															-
- - 4 -					13-															
-					14-															
					15-															
5 -					16-															
													ine Te ied V			Pa				
													enetr				Pa			
										I	5.5					.,				

C	s	tantec	B	OR I	REH N: 48	IOI 890 2	JE 79 I	RE (E: 362	C OR 534	RD 16-23 Sheet 1	of 1
	LIENT _	Pennecon Heavy Civil Limite 2nd Concession Road, Amhe		sland	1. ON					PROJECT No133560	0104
		ORING November 16, 2016			· ·		ER I	LEVEL		TPC ELEVATION	
			F	<u>ب</u> ـ			SAI	MPLES	;	UNDRAINED SHEAR STRENGTH (kPa)	
DEPTH (m)	ELEVATION (m)	STRATA DESCRIPTION	STRATA PLOT	WATER LEVEL	DEPTH (ft)	ТҮРЕ	NUMBER	RECOVERY (mm) TCR(%) / SCR(%)	N-VALUE OR RQD(%)	→ 50 100 150 200 WATER CONTENT & ATTERBERG LIMITS → WP W WL DYNAMIC CONE PENETRATION TEST, BLOWS/0.3m ▼ REI STANDARD PENETRATION TEST, BLOWS/0.3m ● GR/ DIST	MARKS & IN SIZE RIBUTION
0 -		Gravel Road			0			A T C T		10 20 30 40 50 60 70 80 90 100 _{GR S}	(%) A SI CL
-		190 mm SAND and GRAVEL Firm to very stiff, brown sandy CLAY (CL) - trace gravel - dry to moist			Ŭ	SS	1	<u>380</u> 610	8		
-					3 -	ss	2	$\frac{130}{240}$	50/ 100		
1		BOREHOLE TERMINATED on inferred bedrock approximately 1.0 m below grade. Borehole open and dry on completion of drilling.			4 -						
2 -					6 -						
-					8 -						
3 -					10 - 11 -						
-					12 -						
4 -					13-						
-					15-						
5 -										 □ Field Vane Test, kPa □ Remoulded Vane Test, kPa △ Pocket Penetrometer Test, kPa 	

C	S	tantec	B	OR I	REH N: 43	IOI 889 7	E 72 I	RE (E: 361	C OR 528	D 16-24 Sheet 1 of 1
	LIENT _	Pennecon Heavy Civil Limit		1	1.01					PROJECT No. 133560104
		N <u>2nd Concession Road, Amhe</u> ORING <u>November 16, 2016</u>					TED I	LEVEL		DATUM
	ATES: B	ORING <u>INOVEILIDEI 10, 2010</u>				WAI				
(u	NO		LOT	EVEL	(#)		SAI	MPLES ୮ ନିଛି		UNDRAINED SHEAR STRENGTH (kPa) 50 100 150 200
DEPTH (m)	ELEVATION (m)	STRATA DESCRIPTION	STRATA PLOT	WATER LEVEL	DEPTH (ft)	ТҮРЕ	NUMBER	RECOVERY (mm) TCR(%) / SCR(%)	N-VALUE OR RQD(%)	WP W WL WATER CONTENT & ATTERBERG LIMITS FOR TREMARKS DYNAMIC CONE PENETRATION TEST, BLOWS/0.3m REMARKS STANDARD PENETRATION TEST, BLOWS/0.3m GRAIN SIZE
		Gravel Road					2	LCR(EC)	2 Q	STANDARD PENETRATION TEST, BLOWS/0.3m GRAIN SIZE DISTRIBUTION 10 20 30 40 50 60 70 80 90 100 (%) GR SA SI C (%) GR SA SI C
0 -		180 mm Silty SAND with gravel	of H		0-					10 20 30 40 30 00 70 00 70 10 <u>GR SA SI C</u>
-		Stiff, brown to black sandy CLAY (CL) - trace gravel - moist			1 -	ss	1	<u>410</u> 610	10	
1-		light brown to greymoist to wet			3 -	ss	2	$\frac{280}{460}$	10	
-		BOREHOLE TERMINATED on inferred bedrock approximately 1.2 m below grade. Borehole open and dry on completion of drilling.			- 5 - 6 -					
2 -					7 -					
					9 -					
-					10-					
-					12-					
4 -					14-					
-					15-					
5 -					16-					
-										 □ Field Vane Test, kPa □ Remoulded Vane Test, kPa △ Pocket Penetrometer Test, kPa

C	s	tantec	B		XEH N: 48	IOI 889 1	E 51 I	RE (E: 360	C OR 291	D 16-25 Sheet 1 of
	LIENT _ DCATIO	Pennecon Heavy Civil Limite 2nd Concession Road, Amhe		alan	1.01					PROJECT No13356010
		ORING November 16, 2016			,		ER I	LEVEL		DATUM TPC ELEVATION
	AILS. E									UNDRAINED SHEAR STRENGTH (kPa)
(m) H	(TION		A PLOT	LEVEL	(ff) H			MPLES		50 100 150 200
DEPTH (m)	ELEVATION (m)	STRATA DESCRIPTION	STRATA PLOT	WATER LEVEL	DEPTH (ft)	ТҮРЕ	NUMBER	RECOVERY (mm) TCR(%) / SCR(%)	N-VALUE OR RQD(%)	WATER CONTENT & ATTERBERG LIMITS W W DYNAMIC CONE PENETRATION TEST, BLOWS/0.3m ▼ REMAI STANDARD PENETRATION TEST, BLOWS/0.3m ● GRAIN DISTRIBUTE ■ ■
0 -		Gravel Road			0	_		TCF	0	10 20 30 40 50 60 70 80 90 100 (%) GR SA
U -		200 mm Silty SAND with gravel			Ŭ			200		
		Compact, brown silty, clayey SAND (SC-SM) - trace gravel			1 -	SS	1	$\frac{380}{610}$	15	
-		- moist Stiff, brown sandy CLAY (CL)			2 -					
1 -		- trace gravel - moist			3 -	SS	2	$\frac{480}{610}$	13	
-					4 -					
		BOREHOLE TERMINATED on inferred bedrock approximately 1.4	<u></u>		5 -					
-		m below grade.			6 -					
2 -		Borehole caved to approximately 1.2 m below grade on completion. Borehole dry on completion.			7 -					
-					8 -					
-					0					
-					9 -					
3 -					10-					
					11-					
-					12 -					
4 -					13-					
-					14-					
-					15-					
-					16-					
5 -					10-					
										Field Vane Test, kPa Remoulded Vane Test, kPa
										 Remoulded Vane Test, kPa Pocket Penetrometer Test, kPa

C	s	tantec	B	OR	REH N: 43	IOI 890 6	LE 75 1	RE(E: 362	C OR 718	D						16	5-20	6		SI	heet 1 of 1
	LIENT _		ed)JEC]	Г No		13	3560104
		N Dump Road, Amherst Island ORING November 15, 2016	<u>, ON</u>			WAT	ER I	LEVEL									ΓUM	- VAT	ION		
	AIE3. E	OKING <u>10000110,2010</u>						MPLES													
DEPTH (m)	ELEVATION (m)	STRATA DESCRIPTION	STRATA PLOT	WATER LEVEL	DEPTH (ft)	ТҮРЕ	NUMBER	(mr (%)	N-VALUE OR RQD(%)	w	ATE	RCC	50 		1 ATTER		G LIMIT	150 	W _P	20 	W _L
			0,	>			z	CR(%	ν-Ν NOR								, BLOV			•	& GRAIN SIZE DISTRIBUTION
0 -		Gravel Road Compact to very dense, brown sandy CLAY (CL) - trace gravel - gravel content increases below 0.8 m			0 - 1 -	ss	1	<u>410</u> 610	13			20) 3)	0 4	0	50	60 7	70 8	30 9	20 10	0 GR SA SI CI
-		- dry to moist			2 -	Xss	2	<u>_100</u> 	50/ 130												
		BOREHOLE TERMINATED on inferred bedrock approximately 0.9 m below existing grade. Borehole open and dry on completion of drilling.			-3 4 - 5 - 6 - 7 - 8 - 9 - 10 - 11 - 11 - 12 - 13 - 14 - 15 -																
5 -					16-									ne Te							
																Гest, er Te	kPa st, kP	a			

C	s	tantec	B	OR	REH N: 43	IO 891 0	LE 30 I	RE E: 362	C OR 502	D 16-27 Sheet 1 of 1
	LIENT _ DCATIO	Pennecon Heavy Civil Limit		1						PROJECT No133560104
		BORING November 15, 2016				WAT	TER I	LEVEL		TPC ELEVATION
u)	N		LOT	VEL	ft)		SAI	MPLES		UNDRAINED SHEAR STRENGTH (kPa) 50 100 150 200
DEPTH (m)	ELEVATION (m)	STRATA DESCRIPTION	STRATA PLOT	WATER LEVEL	DEPTH (ft)	ТҮРЕ	NUMBER	RECOVERY (mm) TCR(%) / SCR(%)	N-VALUE OR RQD(%)	WP W WL WATER CONTENT & ATTERBERG LIMITS H O H DYNAMIC CONE PENETRATION TEST, BLOWS/0.3m ▼ REMARKS & STANDARD PENETRATION TEST, BLOWS/0.3m ● GRAIN SIZ DISTRIBUTION
0 -		Gravel Road			0			TCF	0	10 20 30 40 50 60 70 80 90 100 (%) (%) GR SA SI
-		150 mm Silty SAND with gravel Compact to very dense, brown sandy CLAY (CL) - trace gravel			1 -	SS	1	<u>330</u> 610	13	Q 42 41 1
		- moist			2 -	×ss	2	25	<u>50/</u> 25	
1 -		BOREHOLE TERMINATED on inferred bedrock at approximately 0.8 m below existing grade.			3 -			30	25	
-		Borehole open and dry on completion of drilling.			4 -					
-					6 -					
2 -					7 -					
					8 -					
3 -					9 - 10-					
-					11-					
-					12 -					
4 -					13-					
-					14-					
-					16-					
5 -				<u>.</u>				1		 □ Field Vane Test, kPa □ Remoulded Vane Test, kPa △ Pocket Penetrometer Test, kPa

C	s	tantec	B	OR	REH N: 48	IOI 888 8	СЕ 73 І	RE(E: 359	C OR 675	RD 16-28 Sheet 1 of 1
	LIENT _	Pennecon Heavy Civil Limite <u>2nd Concession Road, Amhe</u>		sland	1 01	1				PROJECT No133560104
		BORING November 16, 2016					ER I	LEVEL		TPC ELEVATION
							SAI	MPLES		UNDRAINED SHEAR STRENGTH (kPa)
DEPTH (m)	ELEVATION (m)	STRATA DESCRIPTION	STRATA PLOT	WATER LEVEL	DEPTH (ft)	ТҮРЕ	NUMBER	(%) (%)	N-VALUE OR RQD(%)	→ 50 100 150 200 → → → → → → → → → → → → → → → → → → →
0 -		Gravel Road			0-			TCI		10 20 30 40 50 60 70 80 90 100 GR SA SI 0
-		200 mm Silty SAND with gravel Firm to stiff, brown sandy CLAY (CL) - trace gravel - moist to wet			1 - 2 -	SS	1	<u>380</u> 610	17	Ö
		- 300 m wet layer			3 -	ss	2	<u>460</u> 610	8	
2 -		- 100 mm gravel seam			5 -	ss	3	<u>510</u> 610	17	
-		Very dense, brown silty, clayey SAND (SC-SM) - trace gravel			7 -	ss	4	<u>380</u> 380	50/ 76	
3 -		- dry to moist BOREHOLE TERMINATED on inferred bedrock approximately 2.6 m below existing grade. Borehole open and dry on			9 - 10-					
		completion of drilling.			11 - 12 -					
- 4 -					13-					
-					14- 15-					
5 -					16-					□ Field Vane Test, kPa
										 □ Remoulded Vane Test, kPa △ Pocket Penetrometer Test, kPa

Q	s	tantec	B	OR	EH N: 48	[O] 886 7	LE 54 B	RE E: 361	C OR 975	D 16-29 Sheet 1 of 1
	LIENT	Pennecon Heavy Civil Limite N 3rd Concession Road, Amher		land	ON					PROJECT No DATUM
		ORING November 15, 2016			· · · · ·		ER I	LEVEL		DATOM TPC ELEVATION
								MPLES		UNDRAINED SHEAR STRENGTH (kPa)
DEPTH (m)	EVATION (m)	STRATA DESCRIPTION	STRATA PLOT	WATER LEVEL	DEPTH (ft)	ш		RECOVERY (mm) TCR(%) / SCR(%)		$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
ä	ELI		STR	MA		ТҮРЕ	NUMBER	COVEF (%)/	N-VALUE OR RQD(%)	DYNAMIC CONE PENETRATION TEST, BLOWS/0.3m V STANDARD PENETRATION TEST, BLOWS/0.3m GRAIN SIZE DISTRIBUTION
0 -		Gravel Road	701		-0			Ш Ш С		10 20 30 40 50 60 70 80 90 100 GR SA SI
-		180 mm Silty SAND with gravel Stiff to hard, brown to grey CLAY (CH) with sand - trace gravel - moist				SS	1	$\frac{410}{610}$	14	
		 possible fill to 0.8 m decreasing clay content with depth below 2.7 m 			2 - 3 -			510		
-		- auger grinding			4 -	SS	2	<u>510</u> 610	24	
					5 -	SS	3	<u>610</u> 610	22	
2 -					7 - 8 -					
-					9 -	SS	4	<u>610</u> 610	45	
3 -		Very dense, grey silty, clayey SAND (SC-SM) - trace gravel - dry to slightly moist			10- - 11-	ss	5	$\frac{280}{300}$	50/ 130	*
-		BOREHOLE TERMINATED on inferred bedrock at approximately 3.4 m below existing grade.			11					
4 -		Borehole open and dry on completion of drilling.			13 - 14 -					
-					15-					
					16-					
5 -			_1	1			1			 Field Vane Test, kPa Remoulded Vane Test, kPa Pocket Penetrometer Test, kPa

C	s	tantec	B		N: 4	IOI 891 9	LE 08 1	RE E: 363	C OR 194	CD 16-30 Sheet 1 of 1
LO	LIENT _ DCATIO			l, O1						PROJECT No133560104 DATUM
D.	ATES: E	ORING November 15, 2016		1		WAT	ER I	LEVEL		TPC ELEVATION
DEPTH (m)	ELEVATION (m)	STRATA DESCRIPTION	STRATA PLOT	WATER LEVEL	DEPTH (ft)	ТҮРЕ	NUMBER	RECOVERY (mm) A TCR(%) / SCR(%) B	N-VALUE OR RQD(%)	UNDRAINED SHEAR STRENGTH (kPa) 50 100 150 200 + + + + + + + + + + + + + + + + + + +
	ш		<u>ہ</u>	Š		ļ Ĥ	N N N	COV R(%)	2-2 2-2 2-2	STANDARD PENETRATION TEST, BLOWS/0.3m
0 -		Paved Road			0			ЩЦ Ц Ц Ц Ц Ц		10 20 30 40 50 60 70 80 90 100 (%) GR SA SI CI
-		25 mm ASPHALT 75 mm SAND and GRAVEL 25 mm ASPHALT 100 mm SAND and GRAVEL Stiff, brown sandy CLAY (CL)			1 -	ss	1	<u>360</u> 610	8	
- 1- -		- trace gravel - moist			3 -	ss	2	<u>300</u> 610	9	
-		BOREHOLE TERMINATED on			5 -	X ss	3	$\frac{130}{150}$	50/ 1300	
2		inferred bedrock approximately 1.7 m below existing grade. Borehole open and dry on completion of drilling.			6 - 7 - 8 -	-				
- - 3 - - -					9 - 10- 11-	-				
- - - - 4 -					12 - 13 -					
					14- 15-					
5 -					16-					 □ Field Vane Test, kPa □ Remoulded Vane Test, kPa △ Pocket Penetrometer Test, kPa

C	s	tantec	B	OR	REH N: 43	IOI 891 0	LE 40 I	RE(E: 364	COR 094	D	16-31	Sheet 1 of 1
	LIENT _ DCATIO	Pennecon Heavy Civil Limite 2nd Concession Road, Amhe		sland	d, ON	1						133560104
		ORING November 16, 2016					TER I	LEVEL			TPC ELEVATION	
							SAI	MPLES			SHEAR STRENGTH (kPa	a) 200
DEPTH (m)	ELEVATION (m)	STRATA DESCRIPTION	STRATA PLOT	WATER LEVEL	DEPTH (ft)	ТҮРЕ	NUMBER	RECOVERY (mm) TCR(%) / SCR(%)	N-VALUE OR RQD(%)		100 150 WP ATTERBERG LIMITS VETRATION TEST, BLOWS/0.3m ATION TEST, BLOWS/0.3m	W W _L ▼ REMARKS GRAIN SIZE DISTRIBUTION
0 -		Gravel Road			0-			RE(TCI)	10 20 30	40 50 60 70 80 90	
• • • •		180 mm Silty SAND with gravel Stiff to very stiff, brown sandy CLAY (CL) - trace gravel - moist			1 -	ss	1	<u>280</u> 610	13	δ 		28 51 21
1 -					3 -	ss	2	<u>360</u> 610	13			
					5 -	ss	3	<u>510</u> 610	26	•		
		Very dense, brown clayey SAND			7 - 8 -	ss	4	$\frac{\underline{230}}{\underline{230}}$	50/ 76			- - -
3 -		(SC) - trace gravel - moist to wet BOREHOLE TERMINATED on inferred bedrock approximately 2.6 m below grade.			9 - 10-							
		Borehole open and dry upon completion.			11-							
4 -					13- 14-							
-					15- 16-							
5 -				1	1		1	I			est, kPa /ane Test, kPa rometer Test, kPa	

C	s	tantec	B		XEH N: 48	[O] 390 4	LE 15 I	RE(E: 364	C OR 948	RD 16-32 Sheet 1 of
	LIENT _	Pennecon Heavy Civil Limite 3rd Concession Road, Amher		land	LON					PROJECT No133560104
		ORING <u>November 15, 2016</u>			,		ER I	LEVEL		TPC ELEVATION
			1				SAI	MPLES		UNDRAINED SHEAR STRENGTH (kPa)
DEPTH (m)	ELEVATION (m)	STRATA DESCRIPTION	STRATA PLOT	WATER LEVEL	DEPTH (ft)	ТҮРЕ	NUMBER	RECOVERY (mm) TCR(%) / SCR(%)	N-VALUE OR RQD(%)	→ 50 100 150 200 WP W WL WATER CONTENT & ATTERBERG LIMITS → 1 DYNAMIC CONE PENETRATION TEST, BLOWS/0.3m ▼ REMARK & GRAIN SI DISTRIBUT
		Orrevel Deed					z	ECC CR(ЧÖ	STANDARD PENETRATION TEST, BLOWS/0.3m GRAIN SI DISTRIBUT 10 20 30 40 50 60 70 80 90 100 (%)
0 -		Gravel Road 270 mm SAND and GRAVEL Stiff to very stiff, brown CLAY (CH) with sand - trace gravel			-0 1 - 2 -	SS	1	<u>460</u> 610	31	10 20 30 40 30 00 70 80 90 100 <u>GR SA SI</u>
1 -					3 - 4 -	SS	2	<u>250</u> 610	10	
2 -					5 - 6 - 7 -	SS	3	<u>610</u> 610	20	
		Compact to very dense silty, clayey SAND (SC-SM) - trace gravel			8 - 9 -	SS	4	<u>330</u> 610	20	
3						SS	5	<u>580</u> 610	67	
4 -		BOREHOLE TERMINATED at approximately 3.7 m below existing grade. Borehole open and dry on completion of drilling.			- 12 13 - 14 -					
		completion of drinning.			15-					
5 -			<u> </u>							 □ Field Vane Test, kPa □ Remoulded Vane Test, kPa △ Pocket Penetrometer Test, kPa

C	s	tantec	B		EH N: 48	IOI 892 4	СЕ 44 і	RE(E: 370	C OR 025	D					1	6	-34	4		SI	neet 1 of 1
LO	LIENT _ DCATIO	N South Shore Road, Amherst I		d <u>, O</u>											PR D/			Г No	Э.	13	3560104
D.	ATES: E	ORING November 17, 2016		1		WAT	ER I	LEVEL		i									TION		
(m)	NOIL		PLOT	EVEL	H (ft)		SAI	MPLES			אר −+	IDRAIN 50	IED		EAR 100	ST	RE +	NGT 150		°a) 	0
DEPTH (m)	ELEVATION (m)	STRATA DESCRIPTION	STRATA PLOT	WATER LEVEL	DEPTH (ft)	ТҮРЕ	NUMBER	RECOVERY (mm) TCR(%) / SCR(%	N-VALUE OR RQD(%)	DY	NA	ER CONTE MIC CON DARD PE	E PEI	NETR	ATION	N TE	ST, I	BLOW		W O I V	W _L REMARKS & GRAIN SIZE DISTRIBUTION
0 -		Gravel Road			0-	_		TCI	0	1	10	20	30	40	50	60) 7	70	80	0 10	0 GR SA SI CL
-		240 mm SAND and GRAVEL			Ū	ss	1	$\frac{200}{340}$	50/ 51												
-		Very dense, grey weathered bedrock			1 -																
-		BOREHOLE TERMINATED on									E										-
-		inferred bedrock approximately 0.3 m below existing grade.			2 -					· · · · · · · · · · · · · · · · · · ·											
- 1		Borehole open and dry on			3 -																-
-		completion of drilling.			4 -																
_					5 -					· · · · · · · · · · · · · · · · · · ·											-
-					6 -					· · · · · · · · · · · · · · · · · · ·											
2 -					7																_
-					7 -					· · · · · · · · · · · · · · · · · · ·											
-					8 -					· · · · · · · · · · · · · · · · · · ·											_
-					9 -																
3 -					10-																-
-					11 -																
-					12-																-
-					13-					· · · · · · · · · · · · · · · · · · ·											
4 -										· · · · · · · · · · · · · · · · · · ·											-
-					14-																
-					15-																
5 -					16-																
												Field Va									
												Remoul Pocket I						09			
										Δ		rocket l	renet	rome	er I	est	, кр	a			

C	s	tantec	B	OR	REH N: 43	IOI 891 1	LE 18 I	RE(E: 364	C OR 597	D						10	6-3	8			S	heet 1	of 1
		Pennecon Heavy Civil Limite N Stella 40 Foot Road, Amhers		and	ON												DJEC		ю.			33560	<u>104</u>
		NI 1 15 0016	51 151			WAT	ER I	LEVEL									TUM						
	AIES. E			1							JND												
DEPTH (m)	.EVATION (m)	STRATA DESCRIPTION	STRATA PLOT	WATER LEVEL	DEPTH (ft)			VPLES				5	0	-+	10	00	-+	15	0	,iki →⊢ ₩p	20 W	00 <i>W</i> L	
DEP) ELEV		STRA ⁻	WATE	DEP	ТҮРЕ	NUMBER	RECOVERY (mm) TCR(%) / SCR(%)	N-VALUE OR RQD(%)	DY	ater ('Namic Andai	c cc	NE P	PENE	TRAT	FION "	TEST,	BLO				GRA	IARKS & IN SIZE IBUTION
0		Paved Road						TCF	0		10 2	20	30	40	5	0	60	70	80	9) 10	0 GR SA	%) \ <u>SICL</u>
0 -		38 mm ASPHALT	/		0																	-	
-		330 mm SAND and GRAVEL Firm to very stiff, grey to brown			1 -	SS	1	$\frac{460}{610}$	28	Ō			•									- 43 41 - -	16
-		CLAY (CH) with sand - trace gravel			2 -																	-	
- 1 -		- moist			3 -																	-	
-					4 -	SS	2	$\frac{300}{610}$	7													-	
		BOREHOLE TERMINATED on inferred bedrock approximately 1.4 m below existing grade.			5 -																	-	
2 -		Borehole open and dry on completion of drilling.			7 -																	-	
-					8 -																	-	
-					9 -																	-	
3 -					10-																	-	
-					11-																	-	
-					12 -																	-	
4 -					13-																	-	
-					14-																	- - -	
-					15-																	-	
5 -					16-																	-	
											Re	moi	/ane uldec Pen	l Va	ne T	est,	kPa est, kl	Pa					

C	s	tantec	r	ΓE	ST N: 4	PI 889 7	Г Р /58 н	EC E: 365	ORD 446)	Sheet 1 of 1 16-35
	IENT _ CATION	Pennecon Heavy Civil Limite Stella 40 Foot Road, Amhers		and,	ON						PROJECT No133560104 DATUM
EX							FER I	EVEL			TPC ELEVATION
	_		Ц				SAM	MPLES		ι	UNDRAINED SHEAR STRENGTH (kPa)
DEPTH (m)	ELEVATION (m)	STRATA DESCRIPTION	STRATA PLOT	WATER LEVEL	DEPTH (ft)	TYPE NUMBER		RECOVERY (mm) TCR(%) / SCR(%)	N-VALUE OR RQD(%)	DY	50 100 150 200 WP W WL VATER CONTENT & ATTERBERG LIMITS H H H YNAMIC CONE PENETRATION TEST, BLOWS/0.3m REMARKS TANDARD PENETRATION TEST, BLOWS/0.3m GRAIN SIZE DISTRIBUTIO
		Gravel Road				1		REC	20		10 20 30 40 50 60 70 80 90 100 GR SA SI C
0 -		250 mm SAND and GRAVEL - some organic inclusions (at road edge)			-0-						
_		Brown CLAY (CL) with sand - topsoil inclusions - moist			1 -						
-		TEST HOLE TERMINATED on existing CSP culvert at approximately 0.4 m below existing grade. Note: Test hole was excavated by hand.			2 -						
- 1 -					3 -						
					4 -	-					
					5 -	-					
- - 2 _					6 -						
2 -					•		•				
											 Remoulded Vane Test, kPa Pocket Penetrometer Test, kPa

LOCATION	C	S	tantec	r	ΓE	ST N: 4	PI' 893 2	Г Р 79 е	ECC 2: 367	ORD 131	Sheet 1 of 1 16-36
E 3 -			•		Isla	nd, C	N				
Image: Strata DESCRIPTION Image:	EX									TPC ELEVATION	
0 Gravel Road 0 180 nm Silty SAND with gravel - some organic inclusions (at road edge) 0 10 20 30 40 50 60 70 80 90 100 (or. sh 1 Brown CLAY (CL) with sand - topsoil inclusions - moist 1 1 1 1 1 1 TEST HOLE TERMINATED on existing CSP culvert at approximately 0.2 m below existing grade. 1 1 1 1 Note: Test hole was excavated by hand. 2 - 3 - 4 - - - - - - 6 - - - - - -	<u>(</u>	z		OT	WATER LEVEL	t)	SAMPLES				
180 rm Silvy SAND with gravel edge)	DEPTH (n	ELEVATIO (m)		STRATA PL		DEPTH (ft	ТҮРЕ	NUMBER	JVERY (mm (%) / SCR(% 4-VALUE 7 RQD(%)	N-VALUE R RQD(%)	WP W WL WATER CONTENT & ATTERBERG LIMITS DYNAMIC CONE PENETRATION TEST, BLOWS/0.3m ▼ REMARKS & STANDARD PENETRATION TEST, BLOWS/0.3m ● GRAIN SIZE
180 rm Silvy SAND with gravel edge)			Gravel Road						REC	20	DISTRIBUTIO
1 - topsol inclusions - moist - TEST HOLE TERMINATED on - existing CSP culvert at - approximately 0.2 m below existing grade. Note: Test hole was excavated by - and <td>0 -</td> <td></td> <td>180 mm Silty SAND with gravel - some organic inclusions (at road edge)</td> <td></td> <td></td> <td>-0-</td> <td></td> <td></td> <td></td> <td></td> <td></td>	0 -		180 mm Silty SAND with gravel - some organic inclusions (at road edge)			-0-					
			 topsoil inclusions moist TEST HOLE TERMINATED on existing CSP culvert at approximately 0.2 m below existing grade. Note: Test hole was excavated by 			2 3 4 5					
 Field Vane Test, kPa Remoulded Vane Test, kPa 	2 -			<u> </u>	<u> </u>	<u> </u>	1	<u> </u>			 Field Vane Test, kPa Remoulded Vane Test, kPa

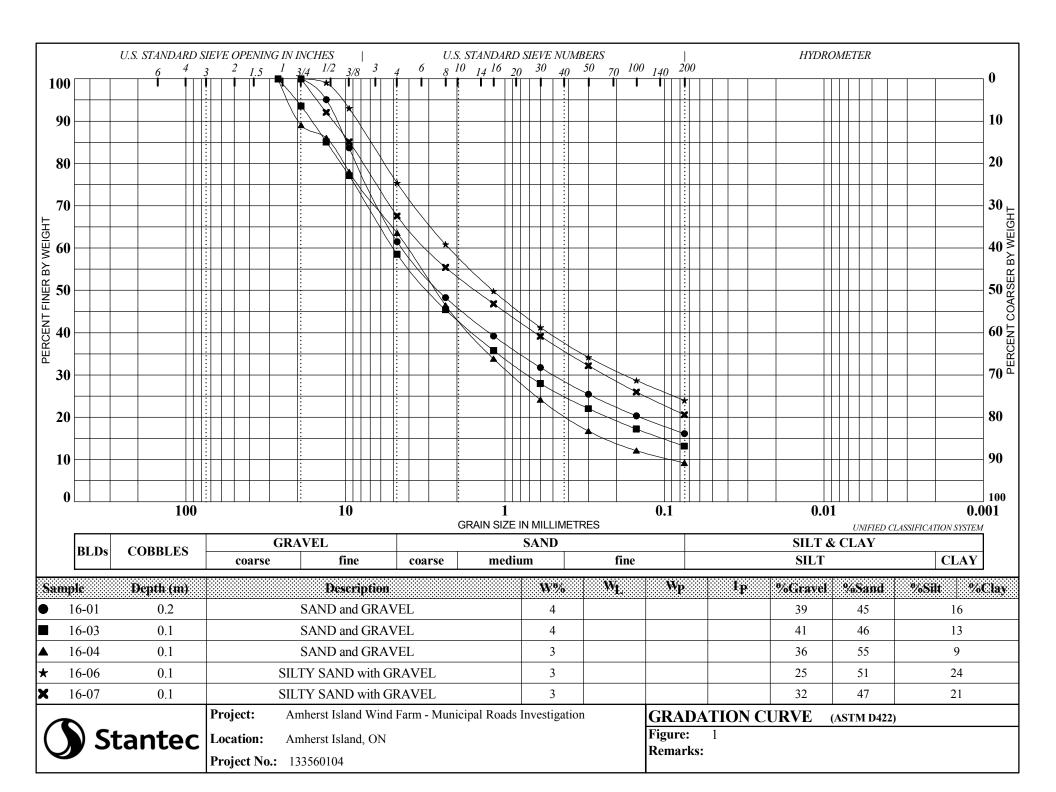
MUNICIPAL ROADS, GEOTECHNICAL BOREHOLE INVESTIGATION AMHERST ISLAND WIND ENERGY PROJECT, AMHERST ISLAND, ONTARIO

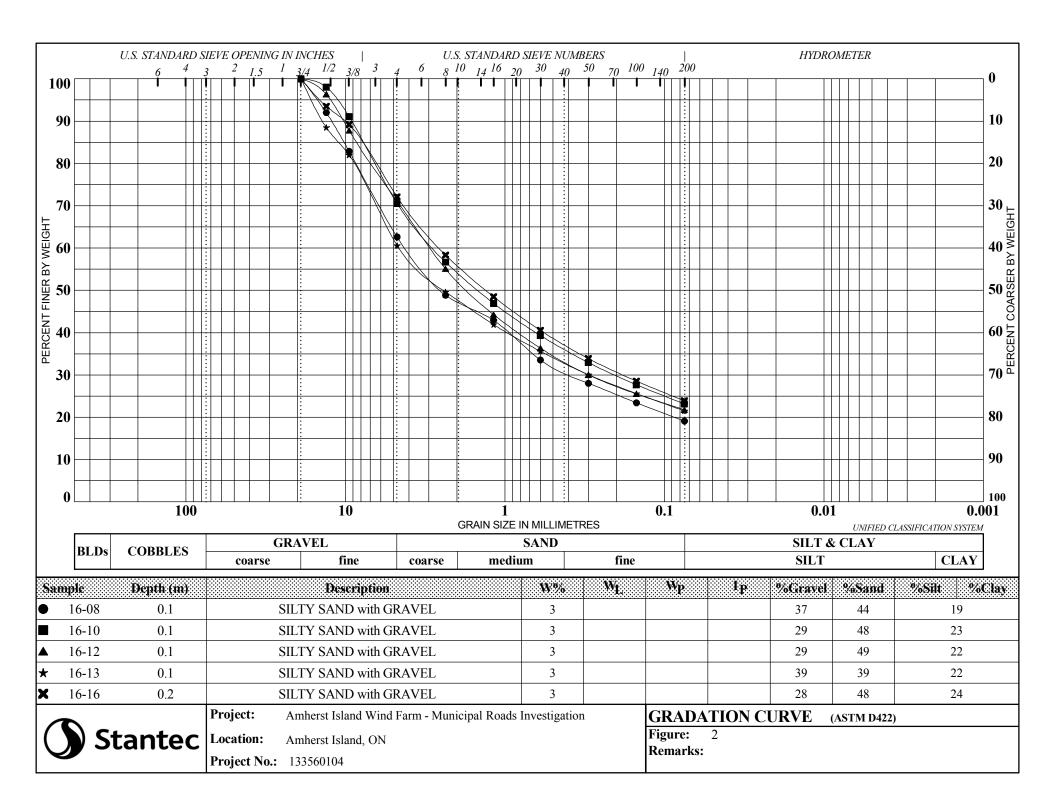
Appendix D August 29, 2017

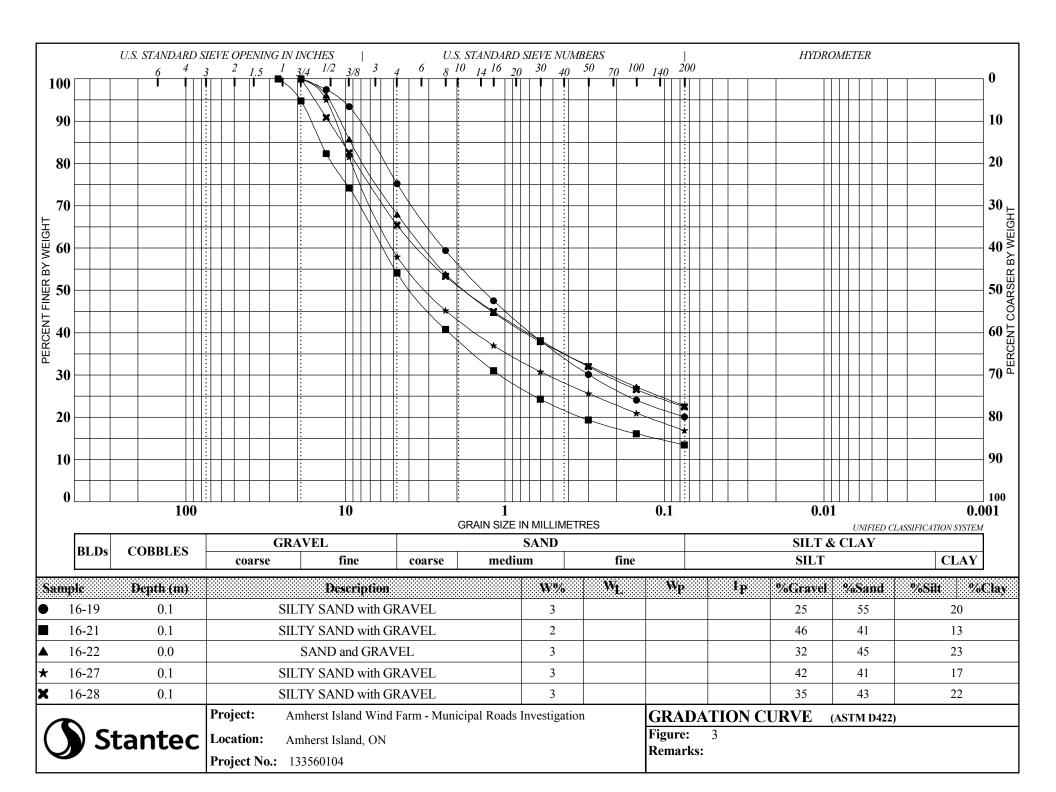
Appendix D

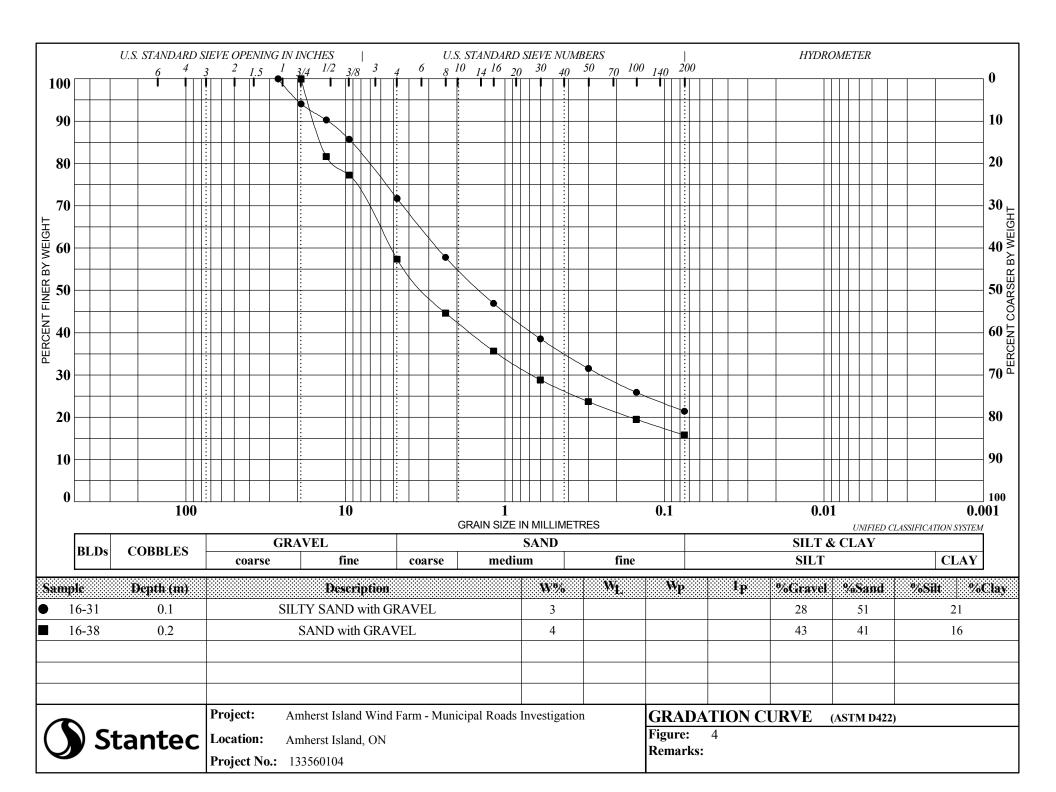
D.1 GEOTECHNICAL LABORATORY TESTING RESULTS

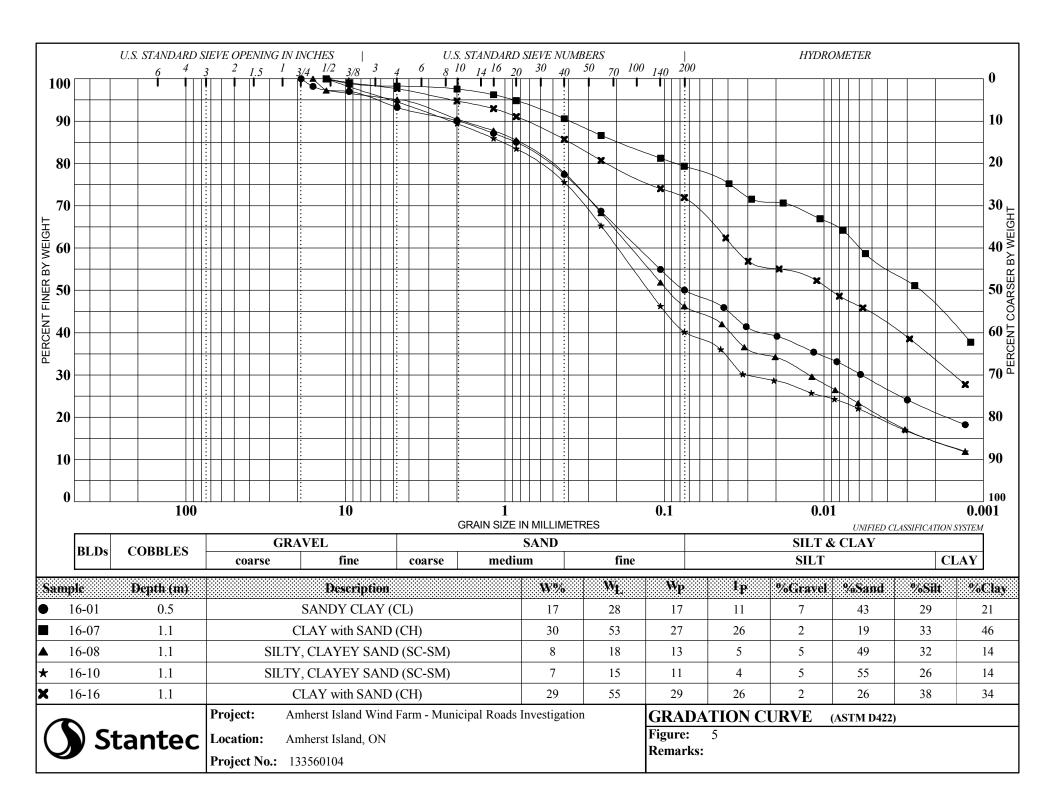


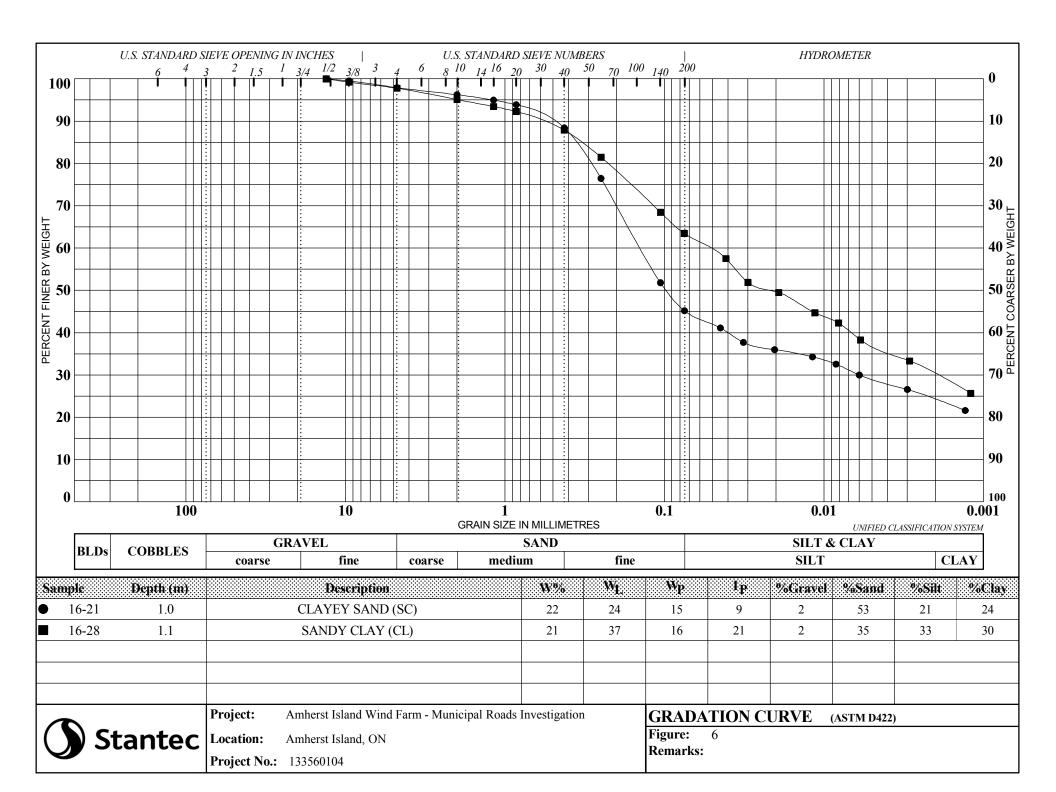




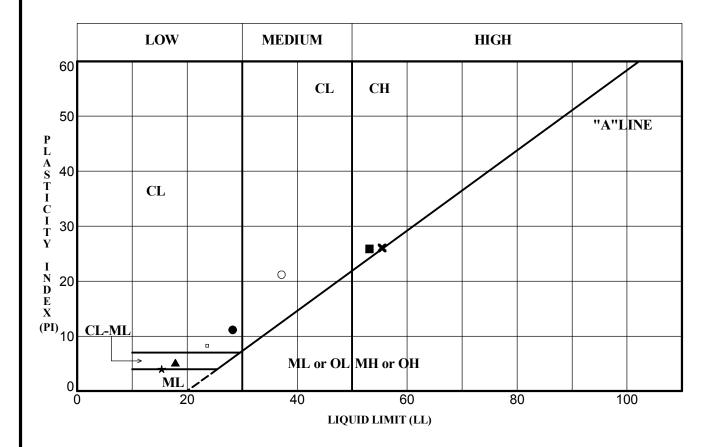








PLASTICITY CHART



	Specimen	Depth (m)	LL	PL	PI	Fines	W%	Classification
•	16-01	0.5	28	17	11	50	17	SANDY CLAY (CL)
	16-07	1.1	53	27	26	79	30	CLAY with SAND (CH)
	16-08	1.1	18	13	5	46	8	SILTY, CLAYEY SAND (SC-SM)
*	16-10	1.1	15	11	4	40	7	SILTY, CLAYEY SAND (SC-SM)
X	16-16	1.1	55	29	26	72	29	CLAY with SAND (CH)
	16-21	1.0	24	15	9	45	22	CLAYEY SAND (SC)
0	16-28	1.1	37	16	21	63	21	SANDY CLAY (CL)

~	Project:	Amherst Island Wind Farm - Municipal Roads Investigation	ATTERBERG LIMITS (ASTM D4318)
Stantec	Location:	Amherst Island, ON	Figure: 7
	Project No.:	133560104	Remarks: